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NUMBERS, FRACTIONS, AND DECIMALS
Mathematical Signs and Commonly Used Abbreviations

| $+$ | Plus (sign of addition) | $\pi$ | $\mathrm{Pi}(3.1416)$ |
| :---: | :---: | :---: | :---: |
| $+$ | Positive | $\Sigma$ | Sigma (sign of summation) |
| - | Minus (sign of subtraction) | $\omega$ | Omega (angles measured in radians) |
| - | Negative | $g$ | Acceleration due to gravity ( 32.16 ft . per sec. per sec.) |
| $\pm(\mp)$ | Plus or minus (minus or plus) | $i$ (or $j$ ) | Imaginary quantity $(\sqrt{-1})$ |
| $\times$ | Multiplied by (multiplication sign) | $\sin$ | Sine |
| . | Multiplied by (multiplication sign) | cos | Cosine |
| $\div$ | Divided by (division sign) | $\tan$ | Tangent |
| 1 | Divided by (division sign) | $\cot$ | Cotangent |
| : | Is to (in proportion) | sec | Secant |
| $=$ | Equals | csc | Cosecant |
| $\neq$ | Is not equal to | vers | Versed sine |
| 三 | Is identical to | covers | Coversed sine |
| : | Equals (in proportion) | $\sin ^{-1} a$ <br> $\arcsin a$ | Arc the sine of which is $a$ |
| $\cong$ | Approximately equals | $(\sin a)^{-1}$ | Reciprocal of $\sin a(1 \div \sin a)$ |
| $\approx$ |  | $\sin ^{n} x$ | $n$th power of $\sin x$ |
| $>$ | Greater than | $\sinh x$ | Hyperbolic sine of $x$ |
| $<$ | Less than | $\cosh x$ | Hyperbolic cosine of $x$ |
| $\geq$ | Greater than or equal to | $\Delta$ | Delta (increment of) |
| $\leq$ | Less than or equal to | $\delta$ | Delta (variation of) |
| $\rightarrow$ | Approaches as a limit | d | Differential (in calculus) |
| $\propto$ | Varies directly as | $\partial$ | Partial differentiation (in calculus) |
| $\therefore$ | Therefore | ¢ | Integral (in calculus) |
| $\sqrt{ }$ | Square root | $\int_{b}^{a}$ | Integral between the limits $a$ and $b$ |
| $\sqrt[3]{ }$ | Cube root | ! | $5!=1 \times 2 \times 3 \times 4 \times 5$ (Factorial) |
| $\sqrt[4]{ }$ | 4th root | $\angle$ | Angle |
| $\sqrt[n]{ }$ | $n$th root $1 / 2$ | L | Right angle |
| $a^{2}$ | $a$ squared (2nd power of $a$ ) | $\perp$ | Perpendicular to |
| $a^{3}$ | $a$ cubed (3rd power of $a$ ) | $\triangle$ | Triangle |
| $a^{4}$ | 4 th power of $a$ | $\bigcirc$ | Circle |
| $a^{n}$ | $n$th power of $a$ | $\square$ | Parallelogram |
| $a^{-n}$ | $1 \div a^{n}$ | - | Degree (circular arc or temperature) |
| $\frac{1}{n}$ | Reciprocal value of $n$ | , | Minutes or feet |
| $\log$ | Logarithm | " | Seconds or inches |
| $\log _{e}$ | Natural or Napierian logarithm | $a^{\prime}$ | $a$ prime |
| $\ln$ |  | $a^{\prime \prime}$ | $a$ double prime |
| $e$ | Base of natural logarithms (2.71828) | $a_{1}$ | $a$ sub one |
| $\lim$ | Limit value (of an expression) | $a_{2}$ | $a$ sub two |
| $\infty$ | Infinity | $a_{n}$ | $a \operatorname{sub} n$ |
| $\alpha$ | Alpha | ( ) | Parentheses |
| $\beta$ | Beta commonly used to | [] | Brackets |
| $\gamma$ | Gamma denote angles | \{ \} | Braces |
| $\theta$ | Theta |  |  |
| $\phi$ | Phi |  |  |
| $\mu$ | Mu (coefficient of friction) |  |  |

## Prime Numbers and Factors of Numbers

The factors of a given number are those numbers which when multiplied together give a product equal to that number; thus, 2 and 3 are factors of 6 ; and 5 and 7 are factors of 35 .

A prime number is one which has no factors except itself and 1 . Thus, $3,5,7,11$, etc., are prime numbers. A factor which is a prime number is called a prime factor.

The accompanying "Prime Number and Factor Tables" give the smallest prime factor of all odd numbers from 1 to 9600 , and can be used for finding all the factors for numbers up to this limit. For example, find the factors of 931 . In the column headed " 900 " and in the line indicated by " 31 " in the left-hand column, the smallest prime factor is found to be 7 . As this leaves another factor 133 (since $931 \div 7=133$ ), find the smallest prime factor of this number. In the column headed " 100 " and in the line " 33 ", this is found to be 7 , leaving a factor 19. This latter is a prime number; hence, the factors of 931 are $7 \times 7 \times 19$. Where no factor is given for a number in the factor table, it indicates that the number is a prime number.

The last page of the tables lists all prime numbers from 9551 through 18691; and can be used to identify quickly all unfactorable numbers in that range.

For factoring, the following general rules will be found useful:
2 is a factor of any number the right-hand figure of which is an even number or 0 . Thus, $28=2 \times 14$, and $210=2 \times 105$.

3 is a factor of any number the sum of the figures of which is evenly divisible by 3 . Thus, 3 is a factor of 1869 , because $1+8+6+9=24 \div 3=8$.

4 is a factor of any number the two right-hand figures of which, considered as one number, are evenly divisible by 4 . Thus, 1844 has a factor 4 , because $44 \div 4=11$.

5 is a factor of any number the right-hand figure of which is 0 or 5 . Thus, $85=5 \times 17 ; 70$ $=5 \times 14$.

Tables of prime numbers and factors of numbers are particularly useful for calculations involving change-gear ratios for compound gearing, dividing heads, gear-generating machines, and mechanical designs having gear trains.

Example 1: A set of four gears is required in a mechanical design to provide an overall gear ratio of $4104 \div 1200$. Furthermore, no gear in the set is to have more than 120 teeth or less than 24 teeth. Determine the tooth numbers.

First, as explained previously, the factors of 4104 are determined to be: $2 \times 2 \times 2 \times 3 \times 3$ $\times 57=4104$. Next, the factors of 1200 are determined: $2 \times 2 \times 2 \times 2 \times 5 \times 5 \times 3=1200$. Therefore $\frac{4104}{1200}=\frac{2 \times 2 \times 2 \times 3 \times 3 \times 57}{2 \times 2 \times 2 \times 2 \times 5 \times 5 \times 3}=\frac{72 \times 57}{24 \times 50}$. If the factors had been combined differently, say, to give $\frac{72 \times 57}{16 \times 75}$, then the 16 -tooth gear in the denominator would not satisfy the requirement of no less than 24 teeth.

Example 2: Factor the number 25078 into two numbers neither of which is larger than 200.

The first factor of 25078 is obviously 2 , leaving $25078 \div 2=12539$ to be factored further. However, from the last table, Prime Numbers from 9551 to 18691, it is seen that 12539 is a prime number; therefore, no solution exists.

Prime Number and Factor Table for 1 to 1199

| From To | $\begin{gathered} 0 \\ 100 \end{gathered}$ | 100 200 | 200 300 | 300 400 | 400 500 | 500 600 | 600 700 | 700 800 | 800 900 | 900 1000 | 1000 1100 | $\begin{aligned} & 1100 \\ & 1200 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | P | P | 3 | 7 | P | 3 | P | P | 3 | 17 | 7 | 3 |
| 3 | P | P | 7 | 3 | 13 | P | 3 | 19 | 11 | 3 | 17 | P |
| 5 | P | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 7 | P | P | 3 | P | 11 | 3 | P | 7 | 3 | P | 19 | 3 |
| 9 | 3 | P | 11 | 3 | P | P | 3 | P | P | 3 | P | P |
| 11 | P | 3 | P | P | 3 | 7 | 13 | 3 | P | P | 3 | 11 |
| 13 | P | P | 3 | P | 7 | 3 | P | 23 | 3 | 11 | P | 3 |
| 15 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 17 | P | 3 | 7 | P | 3 | 11 | P | 3 | 19 | 7 | 3 | P |
| 19 | P | 7 | 3 | 11 | P | 3 | P | P | 3 | P | P | 3 |
| 21 | 3 | 11 | 13 | 3 | P | P | 3 | 7 | P | 3 | P | 19 |
| 23 | P | 3 | P | 17 | 3 | P | 7 | 3 | P | 13 | 3 | P |
| 25 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 27 | 3 | P | P | 3 | 7 | 17 | 3 | P | P | 3 | 13 | 7 |
| 29 | P | 3 | P | 7 | 3 | 23 | 17 | 3 | P | P | 3 | P |
| 31 | P | P | 3 | P | P | 3 | P | 17 | 3 | 7 | P | 3 |
| 33 | 3 | 7 | P | 3 | P | 13 | 3 | P | 7 | 3 | P | 11 |
| 35 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 37 | P | P | 3 | P | 19 | 3 | 7 | 11 | 3 | P | 17 | 3 |
| 39 | 3 | P | P | 3 | P | 7 | 3 | P | P | 3 | P | 17 |
| 41 | P | 3 | P | 11 | 3 | P | P | 3 | 29 | P | 3 | 7 |
| 43 | P | 11 | 3 | 7 | P | 3 | P | P | 3 | 23 | 7 | 3 |
| 45 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 47 | P | 3 | 13 | P | 3 | P | P | 3 | 7 | P | 3 | 31 |
| 49 | 7 | P | 3 | P | P | 3 | 11 | 7 | 3 | 13 | P | 3 |
| 51 | 3 | P | P | 3 | 11 | 19 | 3 | P | 23 | 3 | P | P |
| 53 | P | 3 | 11 | P | 3 | 7 | P | 3 | P | P | 3 | P |
| 55 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 57 | 3 | P | P | 3 | P | P | 3 | P | P | 3 | 7 | 13 |
| 59 | P | 3 | 7 | P | 3 | 13 | P | 3 | P | 7 | 3 | 19 |
| 61 | P | 7 | 3 | 19 | P | 3 | P | P | 3 | 31 | P | 3 |
| 63 | 3 | P | P | 3 | P | P | 3 | 7 | P | 3 | P | P |
| 65 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 67 | P | P | 3 | P | P | 3 | 23 | 13 | 3 | P | 11 | 3 |
| 69 | 3 | 13 | P | 3 | 7 | P | 3 | P | 11 | 3 | P | 7 |
| 71 | P | 3 | P | 7 | 3 | P | 11 | 3 | 13 | P | 3 | P |
| 73 | P | P | 3 | P | 11 | 3 | P | P | 3 | 7 | 29 | 3 |
| 75 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 77 | 7 | 3 | P | 13 | 3 | P | P | 3 | P | P | 3 | 11 |
| 79 | P | P | 3 | P | P | 3 | 7 | 19 | 3 | 11 | 13 | 3 |
| 81 | 3 | P | P | 3 | 13 | 7 | 3 | 11 | P | 3 | 23 | P |
| 83 | P | 3 | P | P | 3 | 11 | P | 3 | P | P | 3 | 7 |
| 85 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 87 | 3 | 11 | 7 | 3 | P | P | 3 | P | P | 3 | P | P |
| 89 | P | 3 | 17 | P | 3 | 19 | 13 | 3 | 7 | 23 | 3 | 29 |
| 91 | 7 | P | 3 | 17 | P | 3 | P | 7 | 3 | P | P | 3 |
| 93 | 3 | P | P | 3 | 17 | P | 3 | 13 | 19 | 3 | P | P |
| 95 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 97 | P | P | 3 | P | 7 | 3 | 17 | P | 3 | P | P | 3 |
| 99 | 3 | P | 13 | 3 | P | P | 3 | 17 | 29 | 3 | 7 | 11 |

Prime Number and Factor Table for 1201 to 2399

| From To | 1200 1300 | 1300 1400 | 1400 1500 | 1500 1600 | 1600 1700 | 1700 1800 | 1800 1900 | 1900 | 2000 2100 | 2100 2200 | 2200 2300 | 2300 2400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | P | P | 3 | 19 | P | 3 | P | P | 3 | 11 | 31 | 3 |
| 3 | 3 | P | 23 | 3 | 7 | 13 | 3 | 11 | P | 3 | P | 7 |
| 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 7 | 17 | P | 3 | 11 | P | 3 | 13 | P | 3 | 7 | P | 3 |
| 9 | 3 | 7 | P | 3 | P | P | 3 | 23 | 7 | 3 | 47 | P |
| 11 | 7 | 3 | 17 | P | 3 | 29 | P | 3 | P | P | 3 | P |
| 13 | P | 13 | 3 | 17 | P | 3 | 7 | P | 3 | P | P | 3 |
| 15 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 17 | P | 3 | 13 | 37 | 3 | 17 | 23 | 3 | P | 29 | 3 | 7 |
| 19 | 23 | P | 3 | 7 | P | 3 | 17 | 19 | 3 | 13 | 7 | 3 |
| 21 | 3 | P | 7 | 3 | P | P | 3 | 17 | 43 | 3 | P | 11 |
| 23 | P | 3 | P | P | 3 | P | P | 3 | 7 | 11 | 3 | 23 |
| 25 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 27 | 3 | P | P | 3 | P | 11 | 3 | 41 | P | 3 | 17 | 13 |
| 29 | P | 3 | P | 11 | 3 | 7 | 31 | 3 | P | P | 3 | 17 |
| 31 | P | 11 | 3 | P | 7 | 3 | P | P | 3 | P | 23 | 3 |
| 33 | 3 | 31 | P | 3 | 23 | P | 3 | P | 19 | 3 | 7 | P |
| 35 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 37 | P | 7 | 3 | 29 | P | 3 | 11 | 13 | 3 | P | P | 3 |
| 39 | 3 | 13 | P | 3 | 11 | 37 | 3 | 7 | P | 3 | P | P |
| 41 | 17 | 3 | 11 | 23 | 3 | P | 7 | 3 | 13 | P | 3 | P |
| 43 | 11 | 17 | 3 | P | 31 | 3 | 19 | 29 | 3 | P | P | 3 |
| 45 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 47 | 29 | 3 | P | 7 | 3 | P | P | 3 | 23 | 19 | 3 | P |
| 49 | P | 19 | 3 | P | 17 | 3 | 43 | P | 3 | 7 | 13 | 3 |
| 51 | 3 | 7 | P | 3 | 13 | 17 | 3 | P | 7 | 3 | P | P |
| 53 | 7 | 3 | P | P | 3 | P | 17 | 3 | P | P | 3 | 13 |
| 55 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 57 | 3 | 23 | 31 | 3 | P | 7 | 3 | 19 | 11 | 3 | 37 | P |
| 59 | P | 3 | P | P | 3 | P | 11 | 3 | 29 | 17 | 3 | 7 |
| 61 | 13 | P | 3 | 7 | 11 | 3 | P | 37 | 3 | P | 7 | 3 |
| 63 | 3 | 29 | 7 | 3 | P | 41 | 3 | 13 | P | 3 | 31 | 17 |
| 65 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 67 | 7 | P | 3 | P | P | 3 | P | 7 | 3 | 11 | P | 3 |
| 69 | 3 | 37 | 13 | 3 | P | 29 | 3 | 11 | P | 3 | P | 23 |
| 71 | 31 | 3 | P | P | 3 | 7 | P | 3 | 19 | 13 | 3 | P |
| 73 | 19 | P | 3 | 11 | 7 | 3 | P | P | 3 | 41 | P | 3 |
| 75 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 77 | P | 3 | 7 | 19 | 3 | P | P | 3 | 31 | 7 | 3 | P |
| 79 | P | 7 | 3 | P | 23 | 3 | P | P | 3 | P | 43 | 3 |
| 81 | 3 | P | P | 3 | 41 | 13 | 3 | 7 | P | 3 | P | P |
| 83 | P | 3 | P | P | 3 | P | 7 | 3 | P | 37 | 3 | P |
| 85 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 87 | 3 | 19 | P | 3 | 7 | P | 3 | P | P | 3 | P | 7 |
| 89 | P | 3 | P | 7 | 3 | P | P | 3 | P | 11 | 3 | P |
| 91 | P | 13 | 3 | 37 | 19 | 3 | 31 | 11 | 3 | 7 | 29 | 3 |
| 93 | 3 | 7 | P | 3 | P | 11 | 3 | P | 7 | 3 | P | P |
| 95 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 97 | P | 11 | 3 | P | P | 3 | 7 | P | 3 | 13 | P | 3 |
| 99 | 3 | P | P | 3 | P | 7 | 3 | P | P | 3 | 11 | P |

Prime Number and Factor Table for 2401 to 3599

| $\begin{gathered} \text { From } \\ \text { To } \end{gathered}$ | 2400 2500 | 2500 2600 | 2600 2700 | 2700 2800 | 2800 2900 | 2900 3000 | 3000 3100 | 3100 3200 | 3200 3300 | 3300 3400 | 3400 3500 | 3500 3600 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 7 | 41 | 3 | 37 | P | 3 | P | 7 | 3 | P | 19 | 3 |
| 3 | 3 | P | 19 | 3 | P | P | 3 | 29 | P | 3 | 41 | 31 |
| 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 7 | 29 | 23 | 3 | P | 7 | 3 | 31 | 13 | 3 | P | P | 3 |
| 9 | 3 | 13 | P | 3 | 53 | P | 3 | P | P | 3 | 7 | 11 |
| 11 | P | 3 | 7 | P | 3 | 41 | P | 3 | 13 | 7 | 3 | P |
| 13 | 19 | 7 | 3 | P | 29 | 3 | 23 | 11 | 3 | P | P | 3 |
| 15 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 17 | P | 3 | P | 11 | 3 | P | 7 | 3 | P | 31 | 3 | P |
| 19 | 41 | 11 | 3 | P | P | 3 | P | P | 3 | P | 13 | 3 |
| 21 | 3 | P | P | 3 | 7 | 23 | 3 | P | P | 3 | 11 | 7 |
| 23 | P | 3 | 43 | 7 | 3 | 37 | P | 3 | 11 | P | 3 | 13 |
| 25 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 27 | 3 | 7 | 37 | 3 | 11 | P | 3 | 53 | 7 | 3 | 23 | P |
| 29 | 7 | 3 | 11 | P | 3 | 29 | 13 | 3 | P | P | 3 | P |
| 31 | 11 | P | 3 | P | 19 | 3 | 7 | 31 | 3 | P | 47 | 3 |
| 33 | 3 | 17 | P | 3 | P | 7 | 3 | 13 | 53 | 3 | P | P |
| 35 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 37 | P | 43 | 3 | 7 | P | 3 | P | P | 3 | 47 | 7 | 3 |
| 39 | 3 | P | 7 | 3 | 17 | P | 3 | 43 | 41 | 3 | 19 | P |
| 41 | P | 3 | 19 | P | 3 | 17 | P | 3 | 7 | 13 | 3 | P |
| 43 | 7 | P | 3 | 13 | P | 3 | 17 | 7 | 3 | P | 11 | 3 |
| 45 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 47 | P | 3 | P | 41 | 3 | 7 | 11 | 3 | 17 | P | 3 | P |
| 49 | 31 | P | 3 | P | 7 | 3 | P | 47 | 3 | 17 | P | 3 |
| 51 | 3 | P | 11 | 3 | P | 13 | 3 | 23 | P | 3 | 7 | 53 |
| 53 | 11 | 3 | 7 | P | 3 | P | 43 | 3 | P | 7 | 3 | 11 |
| 55 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 57 | 3 | P | P | 3 | P | P | 3 | 7 | P | 3 | P | P |
| 59 | P | 3 | P | 31 | 3 | 11 | 7 | 3 | P | P | 3 | P |
| 61 | 23 | 13 | 3 | 11 | P | 3 | P | 29 | 3 | P | P | 3 |
| 63 | 3 | 11 | P | 3 | 7 | P | 3 | P | 13 | 3 | P | 7 |
| 65 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 67 | P | 17 | 3 | P | 47 | 3 | P | P | 3 | 7 | P | 3 |
| 69 | 3 | 7 | 17 | 3 | 19 | P | 3 | P | 7 | 3 | P | 43 |
| 71 | 7 | 3 | P | 17 | 3 | P | 37 | 3 | P | P | 3 | P |
| 73 | P | 31 | 3 | 47 | 13 | 3 | 7 | 19 | 3 | P | 23 | 3 |
| 75 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 77 | P | 3 | P | P | 3 | 13 | 17 | 3 | 29 | 11 | 3 | 7 |
| 79 | 37 | P | 3 | 7 | P | 3 | P | 11 | 3 | 31 | 7 | 3 |
| 81 | 3 | 29 | 7 | 3 | 43 | 11 | 3 | P | 17 | 3 | 59 | P |
| 83 | 13 | 3 | P | 11 | 3 | 19 | P | 3 | 7 | 17 | 3 | P |
| 85 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 87 | 3 | 13 | P | 3 | P | 29 | 3 | P | 19 | 3 | 11 | 17 |
| 89 | 19 | 3 | P | P | 3 | 7 | P | 3 | 11 | P | 3 | 37 |
| 91 | 47 | P | 3 | P | 7 | 3 | 11 | P | 3 | P | P | 3 |
| 93 | 3 | P | P | 3 | 11 | 41 | 3 | 31 | 37 | 3 | 7 | P |
| 95 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 97 | 11 | 7 | 3 | P | P | 3 | 19 | 23 | 3 | 43 | 13 | 3 |
| 99 | 3 | 23 | P | 3 | 13 | P | 3 | 7 | P | 3 | P | 59 |

Prime Number and Factor Table for 3601 to 4799

| From To | 3600 3700 | 3700 3800 | 3800 3900 | 3900 4000 | 4000 4100 | 4100 4200 | 4200 4300 | 4300 4400 | 4400 4500 | 4500 4600 | 4600 4700 | 4700 4800 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 13 | P | 3 | 47 | P | 3 | P | 11 | 3 | 7 | 43 | 3 |
| 3 | 3 | 7 | P | 3 | P | 11 | 3 | 13 | 7 | 3 | P | P |
| 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 7 | P | 11 | 3 | P | P | 3 | 7 | 59 | 3 | P | 17 | 3 |
| 9 | 3 | P | 13 | 3 | 19 | 7 | 3 | 31 | P | 3 | 11 | 17 |
| 11 | 23 | 3 | 37 | P | 3 | P | P | 3 | 11 | 13 | 3 | 7 |
| 13 | P | 47 | 3 | 7 | P | 3 | 11 | 19 | 3 | P | 7 | 3 |
| 15 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 17 | P | 3 | 11 | P | 3 | 23 | P | 3 | 7 | P | 3 | 53 |
| 19 | 7 | P | 3 | P | P | 3 | P | 7 | 3 | P | 31 | 3 |
| 21 | 3 | 61 | P | 3 | P | 13 | 3 | 29 | P | 3 | P | P |
| 23 | P | 3 | P | P | 3 | 7 | 41 | 3 | P | P | 3 | P |
| 25 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 27 | 3 | P | 43 | 3 | P | P | 3 | P | 19 | 3 | 7 | 29 |
| 29 | 19 | 3 | 7 | P | 3 | P | P | 3 | 43 | 7 | 3 | P |
| 31 | P | 7 | 3 | P | 29 | 3 | P | 61 | 3 | 23 | 11 | 3 |
| 33 | 3 | P | P | 3 | 37 | P | 3 | 7 | 11 | 3 | 41 | P |
| 35 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 37 | P | 37 | 3 | 31 | 11 | 3 | 19 | P | 3 | 13 | P | 3 |
| 39 | 3 | P | 11 | 3 | 7 | P | 3 | P | 23 | 3 | P | 7 |
| 41 | 11 | 3 | 23 | 7 | 3 | 41 | P | 3 | P | 19 | 3 | 11 |
| 43 | P | 19 | 3 | P | 13 | 3 | P | 43 | 3 | 7 | P | 3 |
| 45 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 47 | 7 | 3 | P | P | 3 | 11 | 31 | 3 | P | P | 3 | 47 |
| 49 | 41 | 23 | 3 | 11 | P | 3 | 7 | P | 3 | P | P | 3 |
| 51 | 3 | 11 | P | 3 | P | 7 | 3 | 19 | P | 3 | P | P |
| 53 | 13 | 3 | P | 59 | 3 | P | P | 3 | 61 | 29 | 3 | 7 |
| 55 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 57 | 3 | 13 | 7 | 3 | P | P | 3 | P | P | 3 | P | 67 |
| 59 | P | 3 | 17 | 37 | 3 | P | P | 3 | 7 | 47 | 3 | P |
| 61 | 7 | P | 3 | 17 | 31 | 3 | P | 7 | 3 | P | 59 | 3 |
| 63 | 3 | 53 | P | 3 | 17 | 23 | 3 | P | P | 3 | P | 11 |
| 65 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 67 | 19 | P | 3 | P | 7 | 3 | 17 | 11 | 3 | P | 13 | 3 |
| 69 | 3 | P | 53 | 3 | 13 | 11 | 3 | 17 | 41 | 3 | 7 | 19 |
| 71 | P | 3 | 7 | 11 | 3 | 43 | P | 3 | 17 | 7 | 3 | 13 |
| 73 | P | 7 | 3 | 29 | P | 3 | P | P | 3 | 17 | P | 3 |
| 75 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 77 | P | 3 | P | 41 | 3 | P | 7 | 3 | 11 | 23 | 3 | 17 |
| 79 | 13 | P | 3 | 23 | P | 3 | 11 | 29 | 3 | 19 | P | 3 |
| 81 | 3 | 19 | P | 3 | 7 | 37 | 3 | 13 | P | 3 | 31 | 7 |
| 83 | 29 | 3 | 11 | 7 | 3 | 47 | P | 3 | P | P | 3 | P |
| 85 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 87 | 3 | 7 | 13 | 3 | 61 | 53 | 3 | 41 | 7 | 3 | 43 | P |
| 89 | 7 | 3 | P | P | 3 | 59 | P | 3 | 67 | 13 | 3 | P |
| 91 | P | 17 | 3 | 13 | P | 3 | 7 | P | 3 | P | P | 3 |
| 93 | 3 | P | 17 | 3 | P | 7 | 3 | 23 | P | 3 | 13 | P |
| 95 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 97 | P | P | 3 | 7 | 17 | 3 | P | P | 3 | P | 7 | 3 |
| 99 | 3 | 29 | 7 | 3 | P | 13 | 3 | 53 | 11 | 3 | 37 | P |

Prime Number and Factor Table for 4801 to 5999

| $\begin{gathered} \text { From } \\ \text { To } \end{gathered}$ | 4800 4900 | 4900 5000 | 5000 5100 | 5100 5200 | 5200 5300 | $\begin{aligned} & \hline 5300 \\ & 5400 \end{aligned}$ | 5400 5500 | 5500 5600 | 5600 5700 | 5700 5800 | 5800 5900 | $\begin{aligned} & 5900 \\ & 6000 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | P | 13 | 3 | P | 7 | 3 | 11 | P | 3 | P | P | 3 |
| 3 | 3 | P | P | 3 | 11 | P | 3 | P | 13 | 3 | 7 | P |
| 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 7 | 11 | 7 | 3 | P | 41 | 3 | P | P | 3 | 13 | P | 3 |
| 9 | 3 | P | P | 3 | P | P | 3 | 7 | 71 | 3 | 37 | 19 |
| 11 | 17 | 3 | P | 19 | 3 | 47 | 7 | 3 | 31 | P | 3 | 23 |
| 13 | P | 17 | 3 | P | 13 | 3 | P | 37 | 3 | 29 | P | 3 |
| 15 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 17 | P | 3 | 29 | 7 | 3 | 13 | P | 3 | 41 | P | 3 | 61 |
| 19 | 61 | P | 3 | P | 17 | 3 | P | P | 3 | 7 | 11 | 3 |
| 21 | 3 | 7 | P | 3 | 23 | 17 | 3 | P | 7 | 3 | P | 31 |
| 23 | 7 | 3 | P | 47 | 3 | P | 11 | 3 | P | 59 | 3 | P |
| 25 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 27 | 3 | 13 | 11 | 3 | P | 7 | 3 | P | 17 | 3 | P | P |
| 29 | 11 | 3 | 47 | 23 | 3 | 73 | 61 | 3 | 13 | 17 | 3 | 7 |
| 31 | P | P | 3 | 7 | P | 3 | P | P | 3 | 11 | 7 | 3 |
| 33 | 3 | P | 7 | 3 | P | P | 3 | 11 | 43 | 3 | 19 | 17 |
| 35 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 37 | 7 | P | 3 | 11 | P | 3 | P | 7 | 3 | P | 13 | 3 |
| 39 | 3 | 11 | P | 3 | 13 | 19 | 3 | 29 | P | 3 | P | P |
| 41 | 47 | 3 | 71 | 53 | 3 | 7 | P | 3 | P | P | 3 | 13 |
| 43 | 29 | P | 3 | 37 | 7 | 3 | P | 23 | 3 | P | P | 3 |
| 45 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 47 | 37 | 3 | 7 | P | 3 | P | 13 | 3 | P | 7 | 3 | 19 |
| 49 | 13 | 7 | 3 | 19 | 29 | 3 | P | 31 | 3 | P | P | 3 |
| 51 | 3 | P | P | 3 | 59 | P | 3 | 7 | P | 3 | P | 11 |
| 53 | 23 | 3 | 31 | P | 3 | 53 | 7 | 3 | P | 11 | 3 | P |
| 55 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 57 | 3 | P | 13 | 3 | 7 | 11 | 3 | P | P | 3 | P | 7 |
| 59 | 43 | 3 | P | 7 | 3 | 23 | 53 | 3 | P | 13 | 3 | 59 |
| 61 | P | 11 | 3 | 13 | P | 3 | 43 | 67 | 3 | 7 | P | 3 |
| 63 | 3 | 7 | 61 | 3 | 19 | 31 | 3 | P | 7 | 3 | 11 | 67 |
| 65 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 67 | 31 | P | 3 | P | 23 | 3 | 7 | 19 | 3 | 73 | P | 3 |
| 69 | 3 | P | 37 | 3 | 11 | 7 | 3 | P | P | 3 | P | 47 |
| 71 | P | 3 | 11 | P | 3 | 41 | P | 3 | 53 | 29 | 3 | 7 |
| 73 | 11 | P | 3 | 7 | P | 3 | 13 | P | 3 | 23 | 7 | 3 |
| 75 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 77 | P | 3 | P | 31 | 3 | 19 | P | 3 | 7 | 53 | 3 | 43 |
| 79 | 7 | 13 | 3 | P | P | 3 | P | 7 | 3 | P | P | 3 |
| 81 | 3 | 17 | P | 3 | P | P | 3 | P | 13 | 3 | P | P |
| 83 | 19 | 3 | 13 | 71 | 3 | 7 | P | 3 | P | P | 3 | 31 |
| 85 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 87 | 3 | P | P | 3 | 17 | P | 3 | 37 | 11 | 3 | 7 | P |
| 89 | P | 3 | 7 | P | 3 | 17 | 11 | 3 | P | 7 | 3 | 53 |
| 91 | 67 | 7 | 3 | 29 | 11 | 3 | 17 | P | 3 | P | 43 | 3 |
| 93 | 3 | P | 11 | 3 | 67 | P | 3 | 7 | P | 3 | 71 | 13 |
| 95 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 97 | 59 | 19 | 3 | P | P | 3 | 23 | 29 | 3 | 11 | P | 3 |
| 99 | 3 | P | P | 3 | 7 | P | 3 | 11 | 41 | 3 | 17 | 7 |

Prime Number and Factor Table for 6001 to 7199

| From To | 6000 6100 | 6100 6200 | 6200 6300 | $\begin{aligned} & 6300 \\ & 6400 \end{aligned}$ | 6400 6500 | 6500 6600 | 6600 6700 | 6700 6800 | 6800 6900 | 6900 7000 | 7000 7100 | 7100 7200 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 17 | P | 3 | P | 37 | 3 | 7 | P | 3 | 67 | P | 3 |
| 3 | 3 | 17 | P | 3 | 19 | 7 | 3 | P | P | 3 | 47 | P |
| 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 7 | P | 31 | 3 | 7 | 43 | 3 | P | 19 | 3 | P | 7 | 3 |
| 9 | 3 | 41 | 7 | 3 | 13 | 23 | 3 | P | 11 | 3 | 43 | P |
| 11 | P | 3 | P | P | 3 | 17 | 11 | 3 | 7 | P | 3 | 13 |
| 13 | 7 | P | 3 | 59 | 11 | 3 | 17 | 7 | 3 | 31 | P | 3 |
| 15 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 17 | 11 | 3 | P | P | 3 | 7 | 13 | 3 | 17 | P | 3 | 11 |
| 19 | 13 | 29 | 3 | 71 | 7 | 3 | P | P | 3 | 11 | P | 3 |
| 21 | 3 | P | P | 3 | P | P | 3 | 11 | 19 | 3 | 7 | P |
| 23 | 19 | 3 | 7 | P | 3 | 11 | 37 | 3 | P | 7 | 3 | 17 |
| 25 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 27 | 3 | 11 | 13 | 3 | P | 61 | 3 | 7 | P | 3 | P | P |
| 29 | P | 3 | P | P | 3 | P | 7 | 3 | P | 13 | 3 | P |
| 31 | 37 | P | 3 | 13 | 59 | 3 | 19 | 53 | 3 | 29 | 79 | 3 |
| 33 | 3 | P | 23 | 3 | 7 | 47 | 3 | P | P | 3 | 13 | 7 |
| 35 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 37 | P | 17 | 3 | P | 41 | 3 | P | P | 3 | 7 | 31 | 3 |
| 39 | 3 | 7 | 17 | 3 | 47 | 13 | 3 | 23 | 7 | 3 | P | 11 |
| 41 | 7 | 3 | 79 | 17 | 3 | 31 | 29 | 3 | P | 11 | 3 | 37 |
| 43 | P | P | 3 | P | 17 | 3 | 7 | 11 | 3 | 53 | P | 3 |
| 45 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 47 | P | 3 | P | 11 | 3 | P | 17 | 3 | 41 | P | 3 | 7 |
| 49 | 23 | 11 | 3 | 7 | P | 3 | 61 | 17 | 3 | P | 7 | 3 |
| 51 | 3 | P | 7 | 3 | P | P | 3 | 43 | 13 | 3 | 11 | P |
| 53 | P | 3 | 13 | P | 3 | P | P | 3 | 7 | 17 | 3 | 23 |
| 55 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 57 | 3 | 47 | P | 3 | 11 | 79 | 3 | 29 | P | 3 | P | 17 |
| 59 | 73 | 3 | 11 | P | 3 | 7 | P | 3 | 19 | P | 3 | P |
| 61 | 11 | 61 | 3 | P | 7 | 3 | P | P | 3 | P | 23 | 3 |
| 63 | 3 | P | P | 3 | 23 | P | 3 | P | P | 3 | 7 | 13 |
| 65 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 67 | P | 7 | 3 | P | 29 | 3 | 59 | 67 | 3 | P | 37 | 3 |
| 69 | 3 | 31 | P | 3 | P | P | 3 | 7 | P | 3 | P | 67 |
| 71 | 13 | 3 | P | 23 | 3 | P | 7 | 3 | P | P | 3 | 71 |
| 73 | P | P | 3 | P | P | 3 | P | 13 | 3 | 19 | 11 | 3 |
| 75 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 77 | 59 | 3 | P | 7 | 3 | P | 11 | 3 | 13 | P | 3 | P |
| 79 | P | 37 | 3 | P | 11 | 3 | P | P | 3 | 7 | P | 3 |
| 81 | 3 | 7 | 11 | 3 | P | P | 3 | P | 7 | 3 | 73 | 43 |
| 83 | 7 | 3 | 61 | 13 | 3 | 29 | 41 | 3 | P | P | 3 | 11 |
| 85 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 87 | 3 | 23 | P | 3 | 13 | 7 | 3 | 11 | 71 | 3 | 19 | P |
| 89 | P | 3 | 19 | P | 3 | 11 | P | 3 | 83 | 29 | 3 | 7 |
| 91 | P | 41 | 3 | 7 | P | 3 | P | P | 3 | P | 7 | 3 |
| 93 | 3 | 11 | 7 | 3 | 43 | 19 | 3 | P | 61 | 3 | 41 | P |
| 95 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 97 | 7 | P | 3 | P | 73 | 3 | 37 | 7 | 3 | P | 47 | 3 |
| 99 | 3 | P | P | 3 | 67 | P | 3 | 13 | P | 3 | 31 | 23 |

Prime Number and Factor Table for 7201 to 8399

| $\begin{aligned} & \text { From } \\ & \text { To } \end{aligned}$ | 7200 7300 | 7300 7400 | 7400 7500 | 7500 7600 | 7600 7700 | 7700 7800 | 7800 7900 | 7900 8000 | 8000 8100 | 8100 8200 | 8200 8300 | 8300 8400 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 19 | 7 | 3 | 13 | 11 | 3 | 29 | P | 3 | P | 59 | 3 |
| 3 | 3 | 67 | 11 | 3 | P | P | 3 | 7 | 53 | 3 | 13 | 19 |
| 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 7 | P | P | 3 | P | P | 3 | 37 | P | 3 | 11 | 29 | 3 |
| 9 | 3 | P | 31 | 3 | 7 | 13 | 3 | 11 | P | 3 | P | 7 |
| 11 | P | 3 | P | 7 | 3 | 11 | 73 | 3 | P | P | 3 | P |
| 13 | P | 71 | 3 | 11 | 23 | 3 | 13 | 41 | 3 | 7 | 43 | 3 |
| 15 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 17 | 7 | 3 | P | P | 3 | P | P | 3 | P | P | 3 | P |
| 19 | P | 13 | 3 | 73 | 19 | 3 | 7 | P | 3 | 23 | P | 3 |
| 21 | 3 | P | 41 | 3 | P | 7 | 3 | 89 | 13 | 3 | P | 53 |
| 23 | 31 | 3 | 13 | P | 3 | P | P | 3 | 71 | P | 3 | 7 |
| 25 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 27 | 3 | 17 | 7 | 3 | 29 | P | 3 | P | 23 | 3 | 19 | 11 |
| 29 | P | 3 | 17 | P | 3 | 59 | P | 3 | 7 | 11 | 3 | P |
| 31 | 7 | P | 3 | 17 | 13 | 3 | 41 | 7 | 3 | 47 | P | 3 |
| 33 | 3 | P | P | 3 | 17 | 11 | 3 | P | 29 | 3 | P | 13 |
| 35 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 37 | P | 11 | 3 | P | 7 | 3 | 17 | P | 3 | 79 | P | 3 |
| 39 | 3 | 41 | 43 | 3 | P | 71 | 3 | 17 | P | 3 | 7 | 31 |
| 41 | 13 | 3 | 7 | P | 3 | P | P | 3 | 11 | 7 | 3 | 19 |
| 43 | P | 7 | 3 | 19 | P | 3 | 11 | 13 | 3 | 17 | P | 3 |
| 45 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 47 | P | 3 | 11 | P | 3 | 61 | 7 | 3 | 13 | P | 3 | 17 |
| 49 | 11 | P | 3 | P | P | 3 | 47 | P | 3 | 29 | 73 | 3 |
| 51 | 3 | P | P | 3 | 7 | 23 | 3 | P | 83 | 3 | 37 | 7 |
| 53 | P | 3 | 29 | 7 | 3 | P | P | 3 | P | 31 | 3 | P |
| 55 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 57 | 3 | 7 | P | 3 | 13 | P | 3 | 73 | 7 | 3 | 23 | 61 |
| 59 | 7 | 3 | P | P | 3 | P | 29 | 3 | P | 41 | 3 | 13 |
| 61 | 53 | 17 | 3 | P | 47 | 3 | 7 | 19 | 3 | P | 11 | 3 |
| 63 | 3 | 37 | 17 | 3 | 79 | 7 | 3 | P | 11 | 3 | P | P |
| 65 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 67 | 13 | 53 | 3 | 7 | 11 | 3 | P | 31 | 3 | P | 7 | 3 |
| 69 | 3 | P | 7 | 3 | P | 17 | 3 | 13 | P | 3 | P | P |
| 71 | 11 | 3 | 31 | 67 | 3 | 19 | 17 | 3 | 7 | P | 3 | 11 |
| 73 | 7 | 73 | 3 | P | P | 3 | P | 7 | 3 | 11 | P | 3 |
| 75 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 77 | 19 | 3 | P | P | 3 | 7 | P | 3 | 41 | 13 | 3 | P |
| 79 | 29 | 47 | 3 | 11 | 7 | 3 | P | 79 | 3 | P | 17 | 3 |
| 81 | 3 | 11 | P | 3 | P | 31 | 3 | 23 | P | 3 | 7 | 17 |
| 83 | P | 3 | 7 | P | 3 | 43 | P | 3 | 59 | 7 | 3 | 83 |
| 85 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 87 | 3 | 83 | P | 3 | P | 13 | 3 | 7 | P | 3 | P | P |
| 89 | 37 | 3 | P | P | 3 | P | 7 | 3 | P | 19 | 3 | P |
| 91 | 23 | 19 | 3 | P | P | 3 | 13 | 61 | 3 | P | P | 3 |
| 93 | 3 | P | 59 | 3 | 7 | P | 3 | P | P | 3 | P | 7 |
| 95 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 97 | P | 13 | 3 | 71 | 43 | 3 | 53 | 11 | 3 | 7 | P | 3 |
| 99 | 3 | 7 | P | 3 | P | 11 | 3 | 19 | 7 | 3 | 43 | 37 |

Prime Number and Factor Table for 8401 to 9599

| From To | $\begin{aligned} & 8400 \\ & 8500 \end{aligned}$ | 8500 8600 | $\begin{aligned} & 8600 \\ & 8700 \end{aligned}$ | $\begin{aligned} & 8700 \\ & 8800 \end{aligned}$ | $\begin{aligned} & 8800 \\ & 8900 \end{aligned}$ | $\begin{aligned} & 8900 \\ & 9000 \end{aligned}$ | $\begin{aligned} & 9000 \\ & 9100 \end{aligned}$ | $\begin{aligned} & 9100 \\ & 9200 \end{aligned}$ | 9200 9300 | 9300 9400 | $\begin{aligned} & 9400 \\ & 9500 \end{aligned}$ | $\begin{aligned} & 9500 \\ & 9600 \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 31 | P | 3 | 7 | 13 | 3 | P | 19 | 3 | 71 | 7 | 3 |
| 3 | 3 | 11 | 7 | 3 | P | 29 | 3 | P | P | 3 | P | 13 |
| 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 7 | 7 | 47 | 3 | P | P | 3 | P | 7 | 3 | 41 | 23 | 3 |
| 9 | 3 | 67 | P | 3 | 23 | 59 | 3 | P | P | 3 | 97 | 37 |
| 11 | 13 | 3 | 79 | 31 | 3 | 7 | P | 3 | 61 | P | 3 | P |
| 13 | 47 | P | 3 | P | 7 | 3 | P | 13 | 3 | 67 | P | 3 |
| 15 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 17 | 19 | 3 | 7 | 23 | 3 | 37 | 71 | 3 | 13 | 7 | 3 | 31 |
| 19 | P | 7 | 3 | P | P | 3 | 29 | 11 | 3 | P | P | 3 |
| 21 | 3 | P | 37 | 3 | P | 11 | 3 | 7 | P | 3 | P | P |
| 23 | P | 3 | P | 11 | 3 | P | 7 | 3 | 23 | P | 3 | 89 |
| 25 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 27 | 3 | P | P | 3 | 7 | 79 | 3 | P | P | 3 | 11 | 7 |
| 29 | P | 3 | P | 7 | 3 | P | P | 3 | 11 | 19 | 3 | 13 |
| 31 | P | 19 | 3 | P | P | 3 | 11 | 23 | 3 | 7 | P | 3 |
| 33 | 3 | 7 | 89 | 3 | 11 | P | 3 | P | 7 | 3 | P | P |
| 35 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 37 | 11 | P | 3 | P | P | 3 | 7 | P | 3 | P | P | 3 |
| 39 | 3 | P | 53 | 3 | P | 7 | 3 | 13 | P | 3 | P | P |
| 41 | 23 | 3 | P | P | 3 | P | P | 3 | P | P | 3 | 7 |
| 43 | P | P | 3 | 7 | 37 | 3 | P | 41 | 3 | P | 7 | 3 |
| 45 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 47 | P | 3 | P | P | 3 | 23 | 83 | 3 | 7 | 13 | 3 | P |
| 49 | 7 | 83 | 3 | 13 | P | 3 | P | 7 | 3 | P | 11 | 3 |
| 51 | 3 | 17 | 41 | 3 | 53 | P | 3 | P | 11 | 3 | 13 | P |
| 53 | 79 | 3 | 17 | P | 3 | 7 | 11 | 3 | 19 | 47 | 3 | 41 |
| 55 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 57 | 3 | 43 | 11 | 3 | 17 | 13 | 3 | P | P | 3 | 7 | 19 |
| 59 | 11 | 3 | 7 | 19 | 3 | 17 | P | 3 | 47 | 7 | 3 | 11 |
| 61 | P | 7 | 3 | P | P | 3 | 13 | P | 3 | 11 | P | 3 |
| 63 | 3 | P | P | 3 | P | P | 3 | 7 | 59 | 3 | P | 73 |
| 65 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 67 | P | 13 | 3 | 11 | P | 3 | P | 89 | 3 | 17 | P | 3 |
| 69 | 3 | 11 | P | 3 | 7 | P | 3 | 53 | 13 | 3 | 17 | 7 |
| 71 | 43 | 3 | 13 | 7 | 3 | P | 47 | 3 | 73 | P | 3 | 17 |
| 73 | 37 | P | 3 | 31 | 19 | 3 | 43 | P | 3 | 7 | P | 3 |
| 75 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 |
| 77 | 7 | 3 | P | 67 | 3 | 47 | 29 | 3 | P | P | 3 | 61 |
| 79 | 61 | 23 | 3 | P | 13 | 3 | 7 | 67 | 3 | 83 | P | 3 |
| 81 | 3 | P | P | 3 | 83 | 7 | 3 | P | P | 3 | 19 | 11 |
| 83 | 17 | 3 | 19 | P | 3 | 13 | 31 | 3 | P | 11 | 3 | 7 |
| 85 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 |
| 87 | 3 | 31 | 7 | 3 | P | 11 | 3 | P | 37 | 3 | 53 | P |
| 89 | 13 | 3 | P | 11 | 3 | 89 | 61 | 3 | 7 | 41 | 3 | 43 |
| 91 | 7 | 11 | 3 | 59 | 17 | 3 | P | 7 | 3 | P | P | 3 |
| 93 | 3 | 13 | P | 3 | P | 17 | 3 | 29 | P | 3 | 11 | 53 |
| 95 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 | 5 | 3 | 5 |
| 97 | 29 | P | 3 | 19 | 7 | 3 | 11 | 17 | 3 | P | P | 3 |
| 99 | 3 | P | P | 3 | 11 | P | 3 | P | 17 | 3 | 7 | 29 |

Prime Numbers from 9551 to 18691

| 9551 | 10181 | 10853 | 11497 | 12157 | 12763 | 13417 | 14071 | 14747 | 15361 | 16001 | 16693 | 17387 | 18043 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 9587 | 10193 | 10859 | 11503 | 12161 | 12781 | 13421 | 14081 | 14753 | 15373 | 16007 | 16699 | 17389 | 18047 |
| 9601 | 10211 | 10861 | 11519 | 12163 | 12791 | 13441 | 14083 | 14759 | 15377 | 16033 | 16703 | 17393 | 18049 |
| 9613 | 10223 | 10867 | 11527 | 12197 | 12799 | 13451 | 14087 | 14767 | 15383 | 16057 | 16729 | 17401 | 18059 |
| 9619 | 10243 | 10883 | 11549 | 12203 | 12809 | 13457 | 14107 | 14771 | 15391 | 16061 | 16741 | 17417 | 18061 |
| 9623 | 10247 | 10889 | 11551 | 12211 | 12821 | 13463 | 14143 | 14779 | 15401 | 16063 | 16747 | 17419 | 18077 |
| 9629 | 10253 | 10891 | 11579 | 12227 | 12823 | 13469 | 14149 | 14783 | 15413 | 16067 | 16759 | 17431 | 18089 |
| 9631 | 10259 | 10903 | 11587 | 12239 | 12829 | 13477 | 14153 | 14797 | 15427 | 16069 | 16763 | 17443 | 18097 |
| 9643 | 10267 | 10909 | 11593 | 12241 | 12841 | 13487 | 14159 | 14813 | 15439 | 16073 | 16787 | 17449 | 18119 |
| 9649 | 10271 | 10937 | 11597 | 12251 | 12853 | 13499 | 14173 | 14821 | 15443 | 16087 | 16811 | 17467 | 18121 |
| 9661 | 10273 | 10939 | 11617 | 12253 | 12889 | 13513 | 14177 | 14827 | 15451 | 16091 | 16823 | 17471 | 18127 |
| 9677 | 10289 | 10949 | 11621 | 12263 | 12893 | 13523 | 14197 | 14831 | 15461 | 16097 | 16829 | 17477 | 18131 |
| 9679 | 10301 | 10957 | 11633 | 12269 | 12899 | 13537 | 14207 | 14843 | 15467 | 16103 | 16831 | 17483 | 18133 |
| 9689 | 10303 | 10973 | 11657 | 12277 | 12907 | 13553 | 14221 | 14851 | 15473 | 16111 | 16843 | 17489 | 18143 |
| 9697 | 10313 | 10979 | 11677 | 12281 | 12911 | 13567 | 14243 | 14867 | 15493 | 16127 | 16871 | 17491 | 18149 |
| 9719 | 10321 | 10987 | 11681 | 12289 | 12917 | 13577 | 14249 | 14869 | 15497 | 16139 | 16879 | 17497 | 18169 |
| 9721 | 10331 | 10993 | 11689 | 12301 | 12919 | 13591 | 14251 | 14879 | 15511 | 16141 | 16883 | 17509 | 18181 |
| 9733 | 10333 | 11003 | 11699 | 12323 | 12923 | 13597 | 14281 | 14887 | 15527 | 16183 | 16889 | 17519 | 18191 |
| 9739 | 10337 | 11027 | 11701 | 12329 | 12941 | 13613 | 14293 | 14891 | 15541 | 16187 | 16901 | 17539 | 18199 |
| 9743 | 10343 | 11047 | 11717 | 12343 | 12953 | 13619 | 14303 | 14897 | 15551 | 16189 | 16903 | 17551 | 18211 |
| 9749 | 10357 | 11057 | 11719 | 12347 | 12959 | 13627 | 14321 | 14923 | 15559 | 16193 | 16921 | 17569 | 18217 |
| 9767 | 10369 | 11059 | 11731 | 12373 | 12967 | 13633 | 14323 | 14929 | 15569 | 16217 | 16927 | 17573 | 18223 |
| 9769 | 10391 | 11069 | 11743 | 12377 | 12973 | 13649 | 14327 | 14939 | 15581 | 16223 | 16931 | 17579 | 18229 |
| 9781 | 10399 | 11071 | 11777 | 12379 | 12979 | 13669 | 14341 | 14947 | 15583 | 16229 | 16937 | 17581 | 18233 |
| 9787 | 10427 | 11083 | 11779 | 12391 | 12983 | 13679 | 14347 | 14951 | 15601 | 16231 | 16943 | 17597 | 18251 |
| 9791 | 10429 | 11087 | 11783 | 12401 | 13001 | 13681 | 14369 | 14957 | 15607 | 16249 | 16963 | 17599 | 18253 |
| 9803 | 10433 | 11093 | 11789 | 12409 | 13003 | 13687 | 14387 | 14969 | 15619 | 16253 | 16979 | 17609 | 18257 |
| 9811 | 10453 | 11113 | 11801 | 12413 | 13007 | 13691 | 14389 | 14983 | 15629 | 16267 | 16981 | 17623 | 18269 |
| 9817 | 10457 | 11117 | 11807 | 12421 | 13009 | 13693 | 14401 | 15013 | 15641 | 16273 | 16987 | 17627 | 18287 |
| 9829 | 10459 | 11119 | 11813 | 12433 | 13033 | 13697 | 14407 | 15017 | 15643 | 16301 | 16993 | 17657 | 18289 |
| 9833 | 10463 | 11131 | 11821 | 12437 | 13037 | 13709 | 14411 | 15031 | 15647 | 16319 | 17011 | 17659 | 18301 |
| 9839 | 10477 | 11149 | 11827 | 12451 | 13043 | 13711 | 14419 | 15053 | 15649 | 16333 | 17021 | 17669 | 18307 |
| 9851 | 10487 | 11159 | 11831 | 12457 | 13049 | 13721 | 14423 | 15061 | 15661 | 16339 | 17027 | 17681 | 18311 |
| 9857 | 10499 | 11161 | 11833 | 12473 | 13063 | 13723 | 14431 | 15073 | 15667 | 16349 | 17029 | 17683 | 18313 |
| 9859 | 10501 | 11171 | 11839 | 12479 | 13093 | 13729 | 14437 | 15077 | 15671 | 16361 | 17033 | 17707 | 18329 |
| 9871 | 10513 | 11173 | 11863 | 12487 | 13099 | 13751 | 14447 | 15083 | 15679 | 16363 | 17041 | 17713 | 18341 |
| 9883 | 10529 | 11177 | 11867 | 12491 | 13103 | 13757 | 14449 | 15091 | 15683 | 16369 | 17047 | 17729 | 18353 |
| 9887 | 10531 | 11197 | 11887 | 12497 | 13109 | 13759 | 14461 | 15101 | 15727 | 16381 | 17053 | 17737 | 18367 |
| 9901 | 10559 | 11213 | 11897 | 12503 | 13121 | 13763 | 14479 | 15107 | 15731 | 16411 | 17077 | 17747 | 18371 |
| 9907 | 10567 | 11239 | 11903 | 12511 | 13127 | 13781 | 14489 | 15121 | 15733 | 16417 | 17093 | 17749 | 18379 |
| 9923 | 10589 | 11243 | 11909 | 12517 | 13147 | 13789 | 14503 | 15131 | 15737 | 16421 | 17099 | 17761 | 18397 |
| 9929 | 10597 | 11251 | 11923 | 12527 | 13151 | 13799 | 14519 | 15137 | 15739 | 16427 | 17107 | 17783 | 18401 |
| 9931 | 10601 | 11257 | 11927 | 12539 | 13159 | 13807 | 14533 | 15139 | 15749 | 16433 | 17117 | 17789 | 18413 |
| 9941 | 10607 | 11261 | 11933 | 12541 | 13163 | 13829 | 14537 | 15149 | 15761 | 16447 | 17123 | 17791 | 18427 |
| 9949 | 10613 | 11273 | 11939 | 12547 | 13171 | 13831 | 14543 | 15161 | 15767 | 16451 | 17137 | 17807 | 18433 |
| 9967 | 10627 | 11279 | 11941 | 12553 | 13177 | 13841 | 14549 | 15173 | 15773 | 16453 | 17159 | 17827 | 18439 |
| 9973 | 10631 | 11287 | 11953 | 12569 | 13183 | 13859 | 14551 | 15187 | 15787 | 16477 | 17167 | 17837 | 18443 |
| 10007 | 10639 | 11299 | 11959 | 12577 | 13187 | 13873 | 14557 | 15193 | 15791 | 16481 | 17183 | 17839 | 18451 |
| 10009 | 10651 | 11311 | 11969 | 12583 | 13217 | 13877 | 14561 | 15199 | 15797 | 16487 | 17189 | 17851 | 18457 |
| 10037 | 10657 | 11317 | 11971 | 12589 | 13219 | 13879 | 14563 | 15217 | 15803 | 16493 | 17191 | 17863 | 18461 |
| 10039 | 10663 | 11321 | 11981 | 12601 | 13229 | 13883 | 14591 | 15227 | 15809 | 16519 | 17203 | 17881 | 18481 |
| 10061 | 10667 | 11329 | 11987 | 12611 | 13241 | 13901 | 14593 | 15233 | 15817 | 16529 | 17207 | 17891 | 18493 |
| 10067 | 10687 | 11351 | 12007 | 12613 | 13249 | 13903 | 14621 | 15241 | 15823 | 16547 | 17209 | 17903 | 18503 |
| 10069 | 10691 | 11353 | 12011 | 12619 | 13259 | 13907 | 14627 | 15259 | 15859 | 16553 | 17231 | 17909 | 18517 |
| 10079 | 10709 | 11369 | 12037 | 12637 | 13267 | 13913 | 14629 | 15263 | 15877 | 16561 | 17239 | 17911 | 18521 |
| 10091 | 10711 | 11383 | 12041 | 12641 | 13291 | 13921 | 14633 | 15269 | 15881 | 16567 | 17257 | 17921 | 18523 |
| 10093 | 10723 | 11393 | 12043 | 12647 | 13297 | 13931 | 14639 | 15271 | 15887 | 16573 | 17291 | 17923 | 18539 |
| 10099 | 10729 | 11399 | 12049 | 12653 | 13309 | 13933 | 14653 | 15277 | 15889 | 16603 | 17293 | 17929 | 18541 |
| 10103 | 10733 | 11411 | 12071 | 12659 | 13313 | 13963 | 14657 | 15287 | 15901 | 16607 | 17299 | 17939 | 18553 |
| 10111 | 10739 | 11423 | 12073 | 12671 | 13327 | 13967 | 14669 | 15289 | 15907 | 16619 | 17317 | 17957 | 18583 |
| 10133 | 10753 | 11437 | 12097 | 12689 | 13331 | 13997 | 14683 | 15299 | 15913 | 16631 | 17321 | 17959 | 18587 |
| 10139 | 10771 | 11443 | 12101 | 12697 | 13337 | 13999 | 14699 | 15307 | 15919 | 16633 | 17327 | 17971 | 18593 |
| 10141 | 10781 | 11447 | 12107 | 12703 | 13339 | 14009 | 14713 | 15313 | 15923 | 16649 | 17333 | 17977 | 18617 |
| 10151 | 10789 | 11467 | 12109 | 12713 | 13367 | 14011 | 14717 | 15319 | 15937 | 16651 | 17341 | 17981 | 18637 |
| 10159 | 10799 | 11471 | 12113 | 12721 | 13381 | 14029 | 14723 | 15329 | 15959 | 16657 | 17351 | 17987 | 18661 |
| 10163 | 10831 | 11483 | 12119 | 12739 | 13397 | 14033 | 14731 | 15331 | 15971 | 16661 | 17359 | 17989 | 18671 |
| 10169 | 10837 | 11489 | 12143 | 12743 | 13399 | 14051 | 14737 | 15349 | 15973 | 16673 | 17377 | 18013 | 18679 |
| 10177 | 10847 | 11491 | 12149 | 12757 | 13411 | 14057 | 14741 | 15359 | 15991 | 16691 | 17383 | 18041 | 18691 |

## Continued and Conjugate Fractions

Continued Fractions.-In dealing with a cumbersome fraction, or one which does not have satisfactory factors, it may be possible to substitute some other, approximately equal, fraction which is simpler or which can be factored satisfactorily. Continued fractions provide a means of computing a series of fractions each of which is a closer approximation to the original fraction than the one preceding it in the series.
A continued fraction is a proper fraction (one whose numerator is smaller than its denominator) expressed in the form

$$
\frac{N}{D}=\frac{1}{D_{1}+\frac{1}{D_{2}+\frac{1}{D_{3}+\ldots}}}
$$

It is convenient to write the above expression as

$$
\frac{N}{D}=\frac{1}{D_{1}}+\frac{1}{D_{2}}+\frac{1}{D_{3}}+\frac{1}{D_{4}}+\cdots
$$

The continued fraction is produced from a proper fraction $N / D$ by dividing the numerator $N$ both into itself and into the denominator $D$. Dividing the numerator into itself gives a result of 1 ; dividing the numerator into the denominator gives a whole number $D_{1}$ plus a remainder fraction $R_{1}$. The process is then repeated on the remainder fraction $R_{1}$ to obtain $D_{2}$ and $R_{2}$; then $D_{3}, R_{3}$, etc., until a remainder of zero results. As an example, using $N / D=$ 2153/9277,

$$
\begin{gathered}
\frac{2153}{9277}=\frac{2153 \div 2153}{9277 \div 2153}=\frac{1}{4+\frac{665}{2153}}=\frac{1}{D_{1}+R_{1}} \\
R_{1}=\frac{665}{2153}=\frac{1}{3+\frac{158}{665}}=\frac{1}{D_{2}+R_{2}} \text { etc. }
\end{gathered}
$$

from which it may be seen that $D_{1}=4, R_{1}=665 / 2153 ; D_{2}=3, R_{2}=158 / 665$; and, continuing as was explained previously, it would be found that: $D_{3}=4, R_{3}=33 / 158 ; \ldots ; D_{9}=2, R_{9}$ $=0$. The complete set of continued fraction elements representing 2153/9277 may then be written as

$$
\begin{aligned}
\frac{2153}{9277}= & \frac{1}{4}+\frac{1}{3}+\frac{1}{4}+\frac{1}{4}+\frac{1}{1}+\frac{1}{3}+\frac{1}{1}+\frac{1}{2}+\frac{1}{2} \\
& D_{1} \ldots \ldots \ldots \ldots D_{5} \ldots \ldots \ldots \ldots D_{9}
\end{aligned}
$$

By following a simple procedure, together with a table organized similar to the one below for the fraction 2153/9277, the denominators $D_{1}, D_{2}, \ldots$ of the elements of a continued fraction may be used to calculate a series of fractions, each of which is a successively closer approximation, called a convergent, to the original fraction $N / D$.

1) The first row of the table contains column numbers numbered from 1 through 2 plus the number of elements, $2+9=11$ in this example.
2) The second row contains the denominators of the continued fraction elements in sequence but beginning in column 3 instead of column 1 because columns 1 and 2 must be blank in this procedure.
3) The third row contains the convergents to the original fraction as they are calculated and entered. Note that the fractions $1 / 0$ and $0 / 1$ have been inserted into columns 1 and 2 . These are two arbitrary convergents, the first equal to infinity, the second to zero, which are used to facilitate the calculations.
4) The convergent in column 3 is now calculated. To find the numerator, multiply the denominator in column 3 by the numerator of the convergent in column 2 and add the numerator of the convergent in column 1 . Thus, $4 \times 0+1=1$.
5) The denominator of the convergent in column 3 is found by multiplying the denominator in column 3 by the denominator of the convergent in column 2 and adding the denominator of the convergent in column 1 . Thus, $4 \times 1+0=4$, and the convergent in column 3 is then $1 / 4$ as shown in the table.
6) Finding the remaining successive convergents can be reduced to using the simple equation

$$
\operatorname{CONVERGENT}_{n}=\frac{\left(D_{n}\right)\left(\mathrm{NUM}_{n-1}\right)+\mathrm{NUM}_{n-2}}{\left(D_{n}\right)\left(\mathrm{DEN}_{n-1}\right)+\mathrm{DEN}_{n-2}}
$$

in which $n=$ column number in the table; $D_{n}=$ denominator in column $n ; \mathrm{NUM}_{n-1}$ and $\mathrm{NUM}_{n-2}$ are numerators and $\mathrm{DEN}_{n-1}$ and $\mathrm{DEN}_{n-2}$ are denominators of the convergents in the columns indicated by their subscripts; and CONVERGENT ${ }_{n}$ is the convergent in column $n$.

Convergents of the Continued Fraction for 2153/9277

| Column <br> Number, $n$ | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Denominator, <br> $D_{n}$ | - | - | 4 | 3 | 4 | 4 | 1 | 3 | 1 | 2 | 2 |
| Convergent $_{n}$ | $\frac{1}{0}$ | $\frac{0}{1}$ | $\frac{1}{4}$ | $\frac{3}{13}$ | $\frac{13}{56}$ | $\frac{55}{237}$ | $\frac{68}{293}$ | $\frac{259}{1116}$ | $\frac{327}{1409}$ | $\frac{913}{3934}$ | $\frac{2153}{9277}$ |

Notes: The decimal values of the successive convergents in the table are alternately larger and smaller than the value of the original fraction 2153/9277. If the last convergent in the table has the same value as the original fraction 2153/9277, then all of the other calculated convergents are correct.
Conjugate Fractions.-In addition to finding approximate ratios by the use of continued fractions and logarithms of ratios, conjugate fractions may be used for the same purpose, independently, or in combination with the other methods.
Two fractions $a / b$ and $c / d$ are said to be conjugate if $a d-b c= \pm 1$. Examples of such pairs are: $0 / 1$ and $1 / 1 ; 1 / 2$ and $1 / 1 ;$ and $9 / 10$ and $8 / 9$. Also, every successive pair of the convergents of a continued fraction are conjugate. Conjugate fractions have certain properties that are useful for solving ratio problems:

1) No fraction between two conjugate fractions $a / b$ and $c / d$ can have a denominator smaller than either $b$ or $d$.
2) A new fraction, $e l f$, conjugate to both fractions of a given pair of conjugate fractions, $a / b$ and $c / d$, and lying between them, may be created by adding respective numerators, $a+$ $c$, and denominators, $b+d$, so that $e l f=(a+c) /(b+d)$.
3) The denominator $f=b+d$ of the new fraction $e l f$ is the smallest of any possible fraction lying between $a / b$ and $c / d$. Thus, 17/19 is conjugate to both $8 / 9$ and $9 / 10$ and no fraction with denominator smaller than 19 lies between them. This property is important if it is desired to minimize the size of the factors of the ratio to be found.
The following example shows the steps to approximate a ratio for a set of gears to any desired degree of accuracy within the limits established for the allowable size of the factors in the ratio.
Example: Find a set of four change gears, $a b / c d$, to approximate the ratio 2.105399 accurate to within $\pm 0.0001$; no gear is to have more than 120 teeth.
Step 1. Convert the given ratio $R$ to a number $r$ between 0 and 1 by taking its reciprocal: $1 / R=1 / 2.105399=0.4749693=r$.
Step 2. Select a pair of conjugate fractions $a / b$ and $c / d$ that bracket $r$. The pair $a / b=0 / 1$ and $c / d=1 / 1$, for example, will bracket 0.4749693 .

Step 3. Add the respective numerators and denominators of the conjugates $0 / 1$ and $1 / 1$ to create a new conjugate $e / f$ between 0 and 1 : $e / f=(a+c) /(b+d)=(0+1) /(1+1)=1 / 2$.
Step 4. Since 0.4749693 lies between $0 / 1$ and $1 / 2$, elf must also be between $0 / 1$ and $1 / 2$ : $e l f=(0+1) /(1+2)=1 / 3$.
Step 5. Since 0.4749693 now lies between $1 / 3$ and $1 / 2$, elf must also be between $1 / 3$ and $1 / 2$ : $e / f=(1+1) /(3+2)=2 / 5$.
Step 6. Continuing as above to obtain successively closer approximations of elf to 0.4749693 , and using a handheld calculator and a scratch pad to facilitate the process, the fractions below, each of which has factors less than 120, were determined:

| Fraction | Numerator Factors | Denominator Factors | Error |
| :--- | :--- | :--- | :--- |
| $19 / 40$ | 19 | $2 \times 2 \times 2 \times 5$ | +.000031 |
| $28 / 59$ | $2 \times 2 \times 7$ | 59 | -.00039 |
| $47 / 99$ | 47 | $3 \times 3 \times 11$ | -.00022 |
| $104 / 219$ | $3 \times 41$ | $7 \times 37$ | -.000066 |
| $142 / 299$ | $2 \times 71$ | $13 \times 23$ | -.000053 |
| $161 / 339$ | $7 \times 23$ | $3 \times 113$ | -.000043 |
| $218 / 459$ | $2 \times 109$ | $3 \times 3 \times 3 \times 17$ | -.000024 |
| $256 / 539$ | $2 \times 2 \times 2 \times 2 \times 2 \times 2 \times 2 \times 2$ | $7 \times 7 \times 11$ | -.000016 |
| $370 / 779$ | $2 \times 5 \times 37$ | $19 \times 41$ | -.0000014 |
| $759 / 1598$ | $3 \times 11 \times 23$ | $2 \times 17 \times 47$ | -.00000059 |

Factors for the numerators and denominators of the fractions shown above were found with the aid of the Prime Numbers and Factors tables beginning on page 4. Since in Step 1 the desired ratio of 2.105399 was converted to its reciprocal 0.4749693 , all of the above fractions should be inverted. Note also that the last fraction, $759 / 1598$, when inverted to become $1598 / 759$, is in error from the desired value by approximately one-half the amount obtained by trial and error using earlier methods.

Using Continued Fraction Convergents as Conjugates.-Since successive convergents of a continued fraction are also conjugate, they may be used to find a series of additional fractions in between themselves. As an example, the successive convergents 55/237 and $68 / 293$ from the table of convergents for 2153/9277 on page 14 will be used to demonstrate the process for finding the first few in-between ratios.

$$
\text { Desired Fraction } N / D=2153 / 9277=0.2320793
$$

| $a / b$ | elf | $c / d$ |  |
| :---: | ---: | ---: | ---: |
| $(1)$ | $55 / 237=.2320675$ | $123 / 530=.2320755$ error $=-.00000039$ | $68 / 293=.2320819$ |
| $(2)$ | $123 / 530=.2320755$ | $191 / 823=.2320778$ error $=-.0000016$ | $68 / 293=.2320819$ |
| $(3)$ | $191 / 823=.2320778$ | ${ }^{a} 259 / 1116=.2320789$ error $=-.0000005$ | $68 / 293=.2320819$ |
| $(4)$ | $259 / 1116=.2320789$ | $327 / 1409=.2320795$ error $=+.0000002$ | $68 / 293=.2320819$ |
| $(5)$ | $259 / 1116=.2320789$ | $586 / 2525=.2320792$ error $=-.0000001$ | $327 / 1409=.2320795$ |
| $(6)$ | $586 / 2525=.2320792$ | $913 / 3934=.2320793$ error $=-.0000000$ | $327 / 1409=.2320795$ |

${ }^{\text {a }}$ Only these ratios had suitable factors below 120.
Step 1. Check the convergents for conjugateness: $55 \times 293-237 \times 68=16115-16116=$ -1 proving the pair to be conjugate.
Step 2. Set up a table as shown on the next page. The leftmost column of line (1) contains the convergent of lowest value, $a / b$; the rightmost the higher value, $c / d$; and the center column the derived value $e / f$ found by adding the respective numerators and denominators of $a / b$ and $c / d$. The error or difference between $e l f$ and the desired value $N / D$, error $=N / D-e / f$, is also shown.
Step 3. On line (2), the process used on line (1) is repeated with the elf value from line (1) becoming the new value of $a / b$ while the $c / d$ value remains unchanged. Had the error in elf
been + instead of - , then $e l f$ would have been the new $c / d$ value and $a / b$ would be unchanged.
Step 4. The process is continued until, as seen on line (4), the error changes sign to + from the previous -. When this occurs, the $e / f$ value becomes the $c / d$ value on the next line instead of $a / b$ as previously and the $a / b$ value remains unchanged.

## Positive and Negative Numbers

The degrees on a thermometer scale extending upward from the zero point may be called positive and may be preceded by a plus sign; thus +5 degrees means 5 degrees above zero. The degrees below zero may be called negative and may be preceded by a minus sign; thus -5 degrees means 5 degrees below zero. In the same way, the ordinary numbers $1,2,3$, etc., which are larger than 0 , are called positive numbers; but numbers can be conceived of as extending in the other direction from 0 , numbers that, in fact, are less than 0 , and these are called negative. As these numbers must be expressed by the same figures as the positive numbers they are designated by a minus sign placed before them, thus: ( -3 ). A negative number should always be enclosed within parentheses whenever it is written in line with other numbers; for example: $17+(-13)-3 \times(-0.76)$.
Negative numbers are most commonly met with in the use of logarithms and natural trigonometric functions. The following rules govern calculations with negative numbers.
A negative number can be added to a positive number by subtracting its numerical value from the positive number.
Example: $4+(-3)=4-3=1$.
A negative number can be subtracted from a positive number by adding its numerical value to the positive number.
Example: $4-(-3)=4+3=7$.
A negative number can be added to a negative number by adding the numerical values and making the sum negative.

## Example: $(-4)+(-3)=-7$.

A negative number can be subtracted from a larger negative number by subtracting the numerical values and making the difference negative.
Example: $(-4)-(-3)=-1$.
A negative number can be subtracted from a smaller negative number by subtracting the numerical values and making the difference positive.
Example: $(-3)-(-4)=1$.
If in a subtraction the number to be subtracted is larger than the number from which it is to be subtracted, the calculation can be carried out by subtracting the smaller number from the larger, and indicating that the remainder is negative.

## Example: $3-5=-(5-3)=-2$.

When a positive number is to be multiplied or divided by a negative numbers, multiply or divide the numerical values as usual; the product or quotient, respectively, is negative. The same rule is true if a negative number is multiplied or divided by a positive number.

$$
\text { Examples: } \begin{array}{rlrl}
4 \times(-3) & =-12 & & (-4) \times 3=-12 \\
15 \div(-3) & =-5 & (-15) \div 3=-5
\end{array}
$$

When two negative numbers are to be multiplied by each other, the product is positive. When a negative number is divided by a negative number, the quotient is positive.
Examples: $(-4) \times(-3)=12 ;(-4) \div(-3)=1.333$.
The two last rules are often expressed for memorizing as follows: "Equal signs make plus, unequal signs make minus."

## Powers, Roots, and Reciprocals

The square of a number (or quantity) is the product of that number multiplied by itself. Thus, the square of 9 is $9 \times 9=81$. The square of a number is indicated by the exponent $\left({ }^{2}\right)$, thus: $9^{2}=9 \times 9=81$.
The cube or third power of a number is the product obtained by using that number as a factor three times. Thus, the cube of 4 is $4 \times 4 \times 4=64$, and is written $4^{3}$.
If a number is used as a factor four or five times, respectively, the product is the fourth or fifth power. Thus, $3^{4}=3 \times 3 \times 3 \times 3=81$, and $2^{5}=2 \times 2 \times 2 \times 2 \times 2=32$. A number can be raised to any power by using it as a factor the required number of times.
The square root of a given number is that number which, when multiplied by itself, will give a product equal to the given number. The square root of 16 (written $\sqrt{16}$ ) equals 4 , because $4 \times 4=16$.
The cube root of a given number is that number which, when used as a factor three times, will give a product equal to the given number. Thus, the cube root of 64 (written $\sqrt[3]{64}$ ) equals 4 , because $4 \times 4 \times 4=64$.
The fourth, fifth, etc., roots of a given number are those numbers which when used as factors four, five, etc., times, will give as a product the given number. Thus, $\sqrt[4]{16}=2$, because $2 \times 2 \times 2 \times 2=16$.
In some formulas, there may be such expressions as $\left(a^{2}\right)^{3}$ and $a^{3 / 2}$. The first of these, $\left(a^{2}\right)^{3}$, means that the number $a$ is first to be squared, $a^{2}$, and the result then cubed to give $a^{6}$. Thus, $\left(a^{2}\right)^{3}$ is equivalent to $a^{6}$ which is obtained by multiplying the exponents 2 and 3. Similarly, $a^{3 / 2}$ may be interpreted as the cube of the square root of $a$, $(\sqrt{a})^{3}$, or $\left(a^{1 / 2}\right)^{3}$, so that, for example, $16^{3 / 2}=(\sqrt{16})^{3}=64$.
The multiplications required for raising numbers to powers and the extracting of roots are greatly facilitated by the use of logarithms. Extracting the square root and cube root by the regular arithmetical methods is a slow and cumbersome operation, and any roots can be more rapidly found by using logarithms.
When the power to which a number is to be raised is not an integer, say 1.62 , the use of either logarithms or a scientific calculator becomes the only practical means of solution.
The reciprocal $R$ of a number $N$ is obtained by dividing 1 by the number; $R=1 / N$. Reciprocals are useful in some calculations because they avoid the use of negative characteristics as in calculations with logarithms and in trigonometry. In trigonometry, the values cosecant, secant, and cotangent are often used for convenience and are the reciprocals of the sine, cosine, and tangent, respectively (see page 83). The reciprocal of a fraction, for instance $3 / 4$, is the fraction inverted, since $1 \div 3 / 4=1 \times 4 / 3=4 / 3$.

## Powers of Ten Notation

Powers of ten notation is used to simplify calculations and ensure accuracy, particularly with respect to the position of decimal points, and also simplifies the expression of numbers which are so large or so small as to be unwieldy. For example, the metric (SI) pressure unit pascal is equivalent to 0.00000986923 atmosphere or 0.0001450377 pound $/$ inch $^{2}$. In powers of ten notation, these figures are $9.86923 \times 10^{-6}$ atmosphere and $1.450377 \times 10^{-4}$ pound $/ \mathrm{inch}^{2}$. The notation also facilitates adaptation of numbers for electronic data processing and computer readout.

Expressing Numbers in Powers of Ten Notation.-In this system of notation, every number is expressed by two factors, one of which is some integer from 1 to 9 followed by a decimal and the other is some power of 10 .

Thus, 10,000 is expressed as $1.0000 \times 10^{4}$ and 10,463 as $1.0463 \times 10^{4}$. The number 43 is expressed as $4.3 \times 10$ and 568 is expressed. as $5.68 \times 10^{2}$.
In the case of decimals, the number 0.0001 , which as a fraction is $1 / 10,000$, is expressed as 1 $\times 10^{-4}$ and 0.0001463 is expressed as $1.463 \times 10^{-4}$. The decimal 0.498 is expressed as 4.98 $\times 10^{-1}$ and 0.03146 is expressed as $3.146 \times 10^{-2}$.
Rules for Converting Any Number to Powers of Ten Notation.-Any number can be converted to the powers of ten notation by means of one of two rules.
Rule 1: If the number is a whole number or a whole number and a decimal so that it has digits to the left of the decimal point, the decimal point is moved a sufficient number of places to the left to bring it to the immediate right of the first digit. With the decimal point shifted to this position, the number so written comprises the first factor when written in powers of ten notation.
The number of places that the decimal point is moved to the left to bring it immediately to the right of the first digit is the positive index or power of 10 that comprises the second factor when written in powers of ten notation.
Thus, to write 4639 in this notation, the decimal point is moved three places to the left giving the two factors: $4.639 \times 10^{3}$. Similarly,

$$
\begin{aligned}
431.412 & =4.31412 \times 10^{2} \\
986388 & =9.86388 \times 10^{5}
\end{aligned}
$$

Rule 2: If the number is a decimal, i.e., it has digits entirely to the right of the decimal point, then the decimal point is moved a sufficient number of places to the right to bring it immediately to the right of the first digit. With the decimal point shifted to this position, the number so written comprises the first factor when written in powers of ten notation.
The number of places that the decimal point is moved to the right to bring it immediately to the right of the first digit is the negative index or power of 10 that follows the number when written in powers of ten notation.
Thus, to bring the decimal point in 0.005721 to the immediate right of the first digit, which is 5, it must be moved three places to the right, giving the two factors: $5.721 \times 10^{-3}$. Similarly,

$$
\begin{aligned}
0.469 & =4.69 \times 10^{-1} \\
0.0000516 & =5.16 \times 10^{-5}
\end{aligned}
$$

Multiplying Numbers Written in Powers of Ten Notation.-When multiplying two numbers written in the powers of ten notation together, the procedure is as follows:

1) Multiply the first factor of one number by the first factor of the other to obtain the first factor of the product.
2) Add the index of the second factor (which is some power of 10 ) of one number to the index of the second factor of the other number to obtain the index of the second factor (which is some power of 10 ) in the product. Thus:

$$
\begin{aligned}
\left(4.31 \times 10^{-2}\right) \times(9.0125 \times 10) & = \\
(4.31 \times 9.0125) \times 10^{-2+1} & =38.844 \times 10^{-1} \\
\left(5.986 \times 10^{4}\right) \times\left(4.375 \times 10^{3}\right) & = \\
(5.986 \times 4.375) \times 10^{4+3} & =26.189 \times 10^{7}
\end{aligned}
$$

In the preceding calculations, neither of the results shown are in the conventional powers of ten form since the first factor in each has two digits. In the conventional powers of ten notation, the results would be

$$
38.844 \times 10^{-1}=3.884 \times 10^{0}=3.884
$$

since $10^{\circ}=1$, and

$$
26.189 \times 10^{7}=2.619 \times 10^{8}
$$

in each case rounding off the first factor to three decimal places.
When multiplying several numbers written in this notation together, the procedure is the same. All of the first factors are multiplied together to get the first factor of the product and all of the indices of the respective powers of ten are added together, taking into account their respective signs, to get the index of the second factor of the product. Thus, $(4.02 \times$ $\left.10^{-3}\right) \times(3.987 \times 10) \times\left(4.863 \times 10^{5}\right)=(4.02 \times 3.987 \times 4.863) \times\left(10^{-3+1+5}\right)=77.94 \times 10^{3}=$ $7.79 \times 10^{4}$ rounding off the first factor to two decimal places.
Dividing Numbers Written in Powers of Ten Notation.-When dividing one number by another when both are written in this notation, the procedure is as follows:

1) Divide the first factor of the dividend by the first factor of the divisor to get the first factor of the quotient.
2) Subtract the index of the second factor of the divisor from the index of the second factor of the dividend, taking into account their respective signs, to get the index of the second factor of the quotient. Thus:

$$
\begin{aligned}
\left(4.31 \times 10^{-2}\right) \div(9.0125 \times 10) & = \\
(4.31 \div 9.0125) \times\left(10^{-2-1}\right) & =0.4782 \times 10^{-3}=4.782 \times 10^{-4}
\end{aligned}
$$

It can be seen that this system of notation is helpful where several numbers of different magnitudes are to be multiplied and divided.
Example: Find the quotient of $\frac{250 \times 4698 \times 0.00039}{43678 \times 0.002 \times 0.0147}$
Solution: Changing all these numbers to powers of ten notation and performing the operations indicated:

$$
\begin{aligned}
\frac{\left(2.5 \times 10^{2}\right) \times\left(4.698 \times 10^{3}\right) \times\left(3.9 \times 10^{-4}\right)}{\left(4.3678 \times 10^{4}\right) \times\left(2 \times 10^{-3}\right) \times\left(1.47 \times 10^{-2}\right)} & = \\
=\frac{(2.5 \times 4.698 \times 3.9)\left(10^{2+3-4}\right)}{(4.3678 \times 2 \times 1.47)\left(10^{4-3-2}\right)} & =\frac{45.8055 \times 10}{12.8413 \times 10^{-1}} \\
& =3.5670 \times 10^{1-(-1)} \\
& =3.5670 \times 10^{2} \\
& =356.70
\end{aligned}
$$

## Preferred Numbers

American National Standard for Preferred Numbers.-This ANSI Standard Z17.11973 covers basic series of preferred numbers which are independent of any measurement system and therefore can be used with metric or customary units.
The numbers are rounded values of the following five geometric series of numbers: $10^{N / 5}, 10^{N / 10}, 10^{N / 20}, 10^{N / 40}$, and $10^{N / 80}$, where $N$ is an integer in the series $0,1,2,3$, etc. The designations used for the five series are respectively R5, R10, R20, R40, and R80.
The R5 series gives 5 numbers approximately 60 per cent apart, the R10 series gives 10 numbers approximately 25 per cent apart, the R20 series gives 20 numbers approximately 12 per cent apart, the R40 series gives 40 numbers approximately 6 per cent apart, and the R80 series gives 80 numbers approximately 3 per cent apart.

## ALGEBRA AND EQUATIONS

## Rearrangement and Transposition of Terms in Formulas

A formula is a rule for a calculation expressed by using letters and signs instead of writing out the rule in words; by this means, it is possible to condense, in a very small space, the essentials of long and cumbersome rules. The letters used in formulas simply stand in place of the figures that are to be substituted when solving a specific problem.
As an example, the formula for the horsepower transmitted by belting may be written

$$
P=\frac{S V W}{33,000}
$$

where $P=$ horsepower transmitted; $S=$ working stress of belt per inch of width in pounds; $V=$ velocity of belt in feet per minute; and, $W=$ width of belt in inches.
If the working stress $S$, the velocity $V$, and the width $W$ are known, the horsepower can be found directly from this formula by inserting the given values. Assume $S=33 ; V=600$; and $W=5$. Then

$$
P=\frac{33 \times 600 \times 5}{33,000}=3
$$

Assume that the horsepower $P$, the stress $S$, and the velocity $V$ are known, and that the width of belt, $W$, is to be found. The formula must then be rearranged so that the symbol $W$ will be on one side of the equals sign and all the known quantities on the other. The rearranged formula is as follows:

$$
\frac{P \times 33,000}{S V}=W
$$

The quantities ( $S$ and $V$ ) that were in the numerator on the right side of the equals sign are moved to the denominator on the left side, and " 33,000 ," which was in the denominator on the right side of the equals sign, is moved to the numerator on the other side. Symbols that are not part of a fraction, like " $P$ " in the formula first given, are to be considered as being numerators (having the denominator 1 ).
Thus, any formula of the form $A=B / C$ can be rearranged as follows:

$$
A \times C=B \quad \text { and } \quad C=\frac{B}{A}
$$

Suppose a formula to be of the form

$$
\begin{gathered}
A=\frac{B \times C}{D} \\
D=\frac{B \times C}{A} \quad \frac{A \times D}{C}=B \quad \frac{A \times D}{B}=C
\end{gathered}
$$

Then
The method given is only directly applicable when all the quantities in the numerator or denominator are standing independently or are factors of a product. If connected by + or signs, the entire numerator or denominator must be moved as a unit, thus,

Given:

$$
\begin{gathered}
\frac{B+C}{A}=\frac{D+E}{F} \\
\frac{F}{A}=\frac{D+E}{B+C} \\
F=\frac{A(D+E)}{B+C}
\end{gathered}
$$

A quantity preceded by a + or - sign can be transposed to the opposite side of the equals sign by changing its sign; if the sign is + , change it to - on the other side; if it is - , change it to + . This process is called transposition of terms.
Example: $\quad B+C=A-D \quad$ then $\quad \begin{aligned} & A=B+C+D \\ & B=A-D-C \\ & C=A-D-B\end{aligned}$

## Sequence of Performing Arithmetic Operations

When several numbers or quantities in a formula are connected by signs indicating that additions, subtractions, multiplications, and divisions are to be made, the multiplications and divisions should be carried out first, in the sequence in which they appear, before the additions or subtractions are performed.
Example:

$$
\begin{aligned}
& 10+26 \times 7-2=10+182-2=190 \\
& 18 \div 6+15 \times 3=3+45=48 \\
& 12+14 \div 2-4=12+7-4=15
\end{aligned}
$$

When it is required that certain additions and subtractions should precede multiplications and divisions, use is made of parentheses () and brackets [ ]. These signs indicate that the calculation inside the parentheses or brackets should be carried out completely by itself before the remaining calculations are commenced. If one bracket is placed inside another, the one inside is first calculated.

Example:

$$
\begin{aligned}
& (6-2) \times 5+8=4 \times 5+8=20+8=28 \\
& 6 \times(4+7) \div 22=6 \times 11 \div 22=66 \div 22=3 \\
& 2+[10 \times 6(8+2)-4] \times 2=2+[10 \times 6 \times 10-4] \times 2 \\
& =2+[600-4] \times 2=2+596 \times 2=2+1192=1194
\end{aligned}
$$

The parentheses are considered as a sign of multiplication; for example, $6(8+2)=6 \times(8$ $+2)$.
The line or bar between the numerator and denominator in a fractional expression is to be considered as a division sign. For example,

$$
\frac{12+16+22}{10}=(12+16+22) \div 10=50 \div 10=5
$$

In formulas, the multiplication sign $(\times)$ is often left out between symbols or letters, the values of which are to be multiplied. Thus,

$$
A B=A \times B \quad \text { and } \quad \frac{A B C}{D}=(A \times B \times C) \div D
$$

## Ratio and Proportion

The ratio between two quantities is the quotient obtained by dividing the first quantity by the second. For example, the ratio between 3 and 12 is $1 / 4$, and the ratio between 12 and 3 is 4. Ratio is generally indicated by the sign $(:)$; thus, $12: 3$ indicates the ratio of 12 to 3 .

A reciprocal, or inverse ratio, is the opposite of the original ratio. Thus, the inverse ratio of $5: 7$ is $7: 5$.
In a compound ratio, each term is the product of the corresponding terms in two or more simple ratios. Thus, when

$$
8: 2=4 \quad 9: 3=3 \quad 10: 5=2
$$

then the compound ratio is

$$
\begin{aligned}
8 \times 9 \times 10: 2 \times 3 \times 5 & =4 \times 3 \times 2 \\
720: 30 & =24
\end{aligned}
$$

Proportion is the equality of ratios. Thus,

$$
6: 3=10: 5 \quad \text { or } \quad 6: 3:: 10: 5
$$

The first and last terms in a proportion are called the extremes; the second and third, the means. The product of the extremes is equal to the product of the means. Thus,

$$
25: 2=100: 8 \quad \text { and } \quad 25 \times 8=2 \times 100
$$

If three terms in a proportion are known, the remaining term may be found by the following rules:
The first term is equal to the product of the second and third terms, divided by the fourth.
The second term is equal to the product of the first and fourth terms, divided by the third.
The third term is equal to the product of the first and fourth terms, divided by the second.
The fourth term is equal to the product of the second and third terms, divided by the first.
Example: Let $x$ be the term to be found, then,

$$
\begin{array}{ll}
x: 12=3.5: 21 & x=\frac{12 \times 3.5}{21}=\frac{42}{21}=2 \\
1 / 4: x=14: 42 & x=\frac{1 / 4 \times 42}{14}=\frac{1}{4} \times 3=\frac{3}{4} \\
5: 9=x: 63 & x=\frac{5 \times 63}{9}=\frac{315}{9}=35 \\
1 / 4: 7 / 8=4: x & x=\frac{7 / 8 \times 4}{1 / 4}=\frac{31 / 2}{1 / 4}=14
\end{array}
$$

If the second and third terms are the same, that number is the mean proportional between the other two. Thus, $8: 4=4: 2$, and 4 is the mean proportional between 8 and 2. The mean proportional between two numbers may be found by multiplying the numbers together and extracting the square root of the product. Thus, the mean proportional between 3 and 12 is found as follows:

$$
3 \times 12=36 \quad \text { and } \quad \sqrt{36}=6
$$

which is the mean proportional.
Practical Examples Involving Simple Proportion.-If it takes 18 days to assemble 4 lathes, how long would it take to assemble 14 lathes?
Let the number of days to be found be $x$. Then write out the proportion as follows:

$$
\begin{aligned}
4: 18 & =14: x \\
\text { (lathes }: \text { days } & =\text { lathes }: \text { days })
\end{aligned}
$$

Now find the fourth term by the rule given:

$$
x=\frac{18 \times 14}{4}=63 \text { days }
$$

Thirty-four linear feet of bar stock are required for the blanks for 100 clamping bolts. How many feet of stock would be required for 912 bolts?
Let $x=$ total length of stock required for 912 bolts.

$$
\begin{aligned}
34: 100 & =x: 912 \\
(\text { feet }: \text { bolts } & =\text { feet }: \text { bolts })
\end{aligned}
$$

Then, the third term $x=(34 \times 912) / 100=310$ feet, approximately.

Inverse Proportion.-In an inverse proportion, as one of the items involved increases, the corresponding item in the proportion decreases, or vice versa. For example, a factory employing 270 men completes a given number of typewriters weekly, the number of working hours being 44 per week. How many men would be required for the same production if the working hours were reduced to 40 per week?
The time per week is in an inverse proportion to the number of men employed; the shorter the time, the more men. The inverse proportion is written:

$$
270: x=40: 44
$$

(men, 44-hour basis: men, 40-hour basis = time, 40 -hour basis: time, 44 -hour basis) Thus

$$
\frac{270}{x}=\frac{40}{44} \quad \text { and } \quad x=\frac{270 \times 44}{40}=297 \mathrm{men}
$$

Problems Involving Both Simple and Inverse Proportions.-If two groups of data are related both by direct (simple) and inverse proportions among the various quantities, then a simple mathematical relation that may be used in solving problems is as follows:

Product of all directly proportional items in first group
Product of all inversely proportional items in first group

$$
=\frac{\text { Product of all directly proportional items in second group }}{\text { Product of all inversely proportional items in second group }}
$$

Example: If a man capable of turning 65 studs in a day of 10 hours is paid $\$ 6.50$ per hour, how much per hour ought a man be paid who turns 72 studs in a 9 -hour day, if compensated in the same proportion?
The first group of data in this problem consists of the number of hours worked by the first man, his hourly wage, and the number of studs which he produces per day; the second group contains similar data for the second man except for his unknown hourly wage, which may be indicated by $x$.
The labor cost per stud, as may be seen, is directly proportional to the number of hours worked and the hourly wage. These quantities, therefore, are used in the numerators of the fractions in the formula. The labor cost per stud is inversely proportional to the number of studs produced per day. (The greater the number of studs produced in a given time the less the cost per stud.) The numbers of studs per day, therefore, are placed in the denominators of the fractions in the formula. Thus,

$$
\begin{aligned}
\frac{10 \times 6.50}{65} & =\frac{9 \times x}{72} \\
x & =\frac{10 \times 6.50 \times 72}{65 \times 9}=\$ 8.00 \text { per hour }
\end{aligned}
$$

## Percentage

If out of 100 pieces made, 12 do not pass inspection, it is said that 12 per cent ( 12 of the hundred) are rejected. If a quantity of steel is bought for $\$ 100$ and sold for $\$ 140$, the profit is 28.6 per cent of the selling price.
The per cent of gain or loss is found by dividing the amount of gain or loss by the original number of which the percentage is wanted, and multiplying the quotient by 100 .
Example: Out of a total output of 280 castings a day, 30 castings are, on an average, rejected. What is the percentage of bad castings?

$$
\frac{30}{280} \times 100=10.7 \text { per cent }
$$

If by a new process 100 pieces can be made in the same time as 60 could formerly be made, what is the gain in output of the new process over the old, expressed in per cent?

Original number, 60 ; gain $100-60=40$. Hence,

$$
\frac{40}{60} \times 100=66.7 \text { per cent }
$$

Care should be taken always to use the original number, or the number of which the percentage is wanted, as the divisor in all percentage calculations. In the example just given, it is the percentage of gain over the old output 60 that is wanted and not the percentage with relation to the new output too. Mistakes are often made by overlooking this important point.

## Interest

Interest is money paid for the use of money lent for a certain time. Simple interest is the interest paid on the principal (money lent) only. When simple interest that is due is not paid, and its amount is added to the interest-bearing principal, the interest calculated on this new principal is called compound interest. The compounding of the interest into the principal may take place yearly or more often, according to circumstances.
Interest Formulas.-The symbols used in the formulas to calculate various types of interest are:
$P=$ principal or amount of money lent
$I=$ nominal annual interest rate stated as a percentage, i.e., 10 per cent per annum
$I_{e}=$ effective annual interest rate when interest is compounded more often than once a year (see Nominal vs. Effective Interest Rates)
$i=$ nominal annual interest rate per cent expressed as a decimal, i.e., if $I=12$ per cent, then $i=12 / 100=0.12$
$n=$ number of annual interest periods
$m=$ number of interest compounding periods in one year
$S=$ a sum of money at the end of $n$ interest periods from the present date that is equivalent to $P$ with added interest $i$
$R=$ the payment at the end of each period in a uniform series of payments continuing for $n$ periods, the entire series equivalent to $P$ at interest rate $i$
Note: The exact amount of interest for one day is $1 / 365$ of the interest for one year. Banks, however, customarily take the year as composed of 12 months of 30 days, making a total of 360 days to a year. This method is also used for home-mortgage-type payments, so that the interest rate per month is $30 / 360=1 / 12$ of the annual interest rate. For example, if $I$ is a 12 per cent per annum nominal interest rate, then for a 30 -day period, the interest rate is $(12 \times 1 / 12)=1.0$ per cent per month. The decimal rate per month is then $1.0 / 100=$ 0.01 .

Simple Interest.-The formulas for simple interest are:

$$
\begin{array}{ll}
\text { Interest for } n \text { years } & =\text { Pin } \\
\text { Total amount after } n \text { years, } S & =P+P \text { in }
\end{array}
$$

Example: For $\$ 250$ that has been lent for three years at 6 per cent simple interest: $P=250$; $I=6 ; i=I / 100=0.06 ; n=3$.

$$
S=250+(250 \times 0.06 \times 3)=250+45=\$ 295
$$

Compound Interest.-The following formulas apply when compound interest is to be computed and assuming that the interest is compounded annually.

$$
\begin{aligned}
S & =P(1+i)^{n} \\
P & =S /(1+i)^{n} \\
i & =(S / P)^{1 / n}-1 \\
n & =(\log S-\log P) / \log (1+i)
\end{aligned}
$$

Example: At 10 per cent interest compounded annually for 10 years, a principal amount $P$ of $\$ 1000$ becomes a sum $S$ of

$$
S=1000(1+10 / 100)^{10}=\$ 2,593.74
$$

If a sum $S=\$ 2593.74$ is to be accumulated, beginning with a principal $P=\$ 1,000$ over a period $n=10$ years, the interest rate $i$ to accomplish this would have to be $i=$ $(2593.74 / 1000)^{1 / 10}-1=0.09999$, which rounds to 0.1 , or 10 per cent.
For a principal $P=\$ 500$ to become $S=\$ 1,000$ at 6 per cent interest compounded annually, the number of years $n$ would have to be

$$
\begin{aligned}
n & =(\log 1000-\log 500) / \log (1+0.06) \\
& =(3-2.69897) / 0.025306=11.9 \text { years }
\end{aligned}
$$

To triple the principal $P=\$ 500$ to become $S=\$ 1,500$, the number of years would have to be

$$
\begin{aligned}
n & =(\log 1500-\log 500) / \log (1+0.06) \\
& =(3.17609-2.69897) / 0.025306=18.85 \text { years }
\end{aligned}
$$

Interest Compounded More Often Than Annually.-If interest is payable $m$ times a year, it will be computed $m$ times during each year, or $n m$ times during $n$ years. The rate for each compounding period will be $i / m$ if $i$ is the nominal annual decimal interest rate. Therefore, at the end of $n$ years, the amount $S$ will be: $S=P(1+i / m)^{n m}$.
As an example, if $P=\$ 1,000 ; n$ is 5 years, the interest payable quarterly, and the annual rate is 6 per cent, then $n=5 ; m=4 ; i=0.06 ; i / m=0.06 / 4=0.015$; and $n m=5 \times 4=20$, so that

$$
S=1000(1+0.015)^{20}=\$ 1,346.86
$$

Nominal vs. Effective Interest Rates.—Deposits in savings banks, automobile loans, interest on bonds, and many other transactions of this type involve computation of interest due and payable more often than once a year. For such instances, there is a difference between the nominal annual interest rate stated to be the cost of borrowed money and the effective rate that is actually charged.
For example, a loan with interest charged at 1 per cent per month is described as having an interest rate of 12 per cent per annum. To be precise, this rate should be stated as being a nominal 12 per cent per annum compounded monthly; the actual or effective rate for monthly payments is 12.7 per cent. For quarterly compounding, the effective rate would be 12.6 per cent:

$$
I_{e}=(1+I / m)^{m}-1
$$

In this formula, $I_{e}$ is the effective annual rate, $I$ is the nominal annual rate, and $m$ is the number of times per year the money is compounded.
Example: For a nominal per annum rate of 12 per cent, with monthly compounding, the effective per annum rate is

$$
I_{e}=(1+0.12 / 12)^{12}-1=0.1268=12.7 \text { per cent effective per annum rate }
$$

Example: Same as before but with quarterly compounding:

$$
I_{e}=(1+0.12 / 4)^{4}-1=0.1255=12.6 \text { per cent effective per annum rate }
$$

Example: Same as before but with annual compounding.

$$
I_{e}=(1+0.12 / 1)^{1}-1=0.12=12 \text { per cent effective per annum rate }
$$

This last example shows that for once-a-year-compounding, the nominal and effective per annum rates are identical.
Finding Unknown Interest Rates.-If a single payment of $P$ dollars is to produce a sum of $S$ dollars after $n$ annual compounding periods, the per annum decimal interest rate is found using:

$$
i=\sqrt[n]{\frac{S}{P}}-1
$$

Present Value and Discount.-The present value or present worth $P$ of a given amount $S$ is the amount $P$ that, when placed at interest $i$ for a given time $n$, will produce the given amount $S$.

$$
\text { At simple interest, } P=S /(1+n i)
$$

At compound interest, $P=S /(1+i)^{n}$
The true discount $D$ is the difference between $S$ and $P: D=S-P$.
These formulas are for an annual interest rate. If interest is payable other than annually, modify the formulas as indicated in the formulas in the section Interest Compounded More Often Than Annually.
Example: Required the present value and discount of $\$ 500$ due in six months at 6 per cent simple interest. Here, $S=500 ; n=6 / 12=0.5$ year; $i=0.06$. Then, $P=500 /(1+0.5 \times 0.06)$ $=\$ 485.44$.
Required the sum that, placed at 5 per cent compound interest, will in three years produce $\$ 5,000$. Here, $S=5000 ; i=0.05 ; n=3$. Then,

$$
P=5000 /(1+0.05)^{3}=\$ 4,319.19
$$

Annuities.-An annuity is a fixed sum paid at regular intervals. In the formulas that follow, yearly payments are assumed. It is customary to calculate annuities on the basis of compound interest. If an annuity $A$ is to be paid out for $n$ consecutive years, the interest rate being $i$, then the present value $P$ of the annuity is

$$
P=A \frac{(1+i)^{n}-1}{i(1+i)^{n}}
$$

Example: If an annuity of $\$ 200$ is to be paid for 10 years, what is the present amount of money that needs to be deposited if the interest is 5 per cent. Here, $A=200 ; i=0.05 ; n=10$ :

$$
P=200 \frac{(1+0.05)^{10}-1}{0.05(1+0.05)^{10}}=\$ 1,544.35
$$

The annuity a principal $P$ drawing interest at the rate $i$ will give for a period of $n$ years is

$$
A=P \frac{i(1+i)^{n}}{(1+i)^{n}-1}
$$

Example: A sum of $\$ 10,000$ is placed at 4 per cent. What is the amount of the annuity payable for 20 years out of this sum: Here, $P=10000 ; i=0.04 ; n=20$ :

$$
A=10,000 \frac{0.04(1+0.04)^{20}}{(1+0.04)^{20}-1}=\$ 735.82
$$

If at the beginning of each year a sum $A$ is set aside at an interest rate $i$, the total value $S$ of the sum set aside, with interest, at the end of $n$ years, will be

$$
S=A \frac{(1+i)\left[(1+i)^{n}-1\right]}{i}
$$

If at the end of each year a sum $A$ is set aside at an interest rate $i$, then the total value $S$ of the principal, with interest, at the end of $n$ years will be

$$
S=A \frac{(1+i)^{n}-1}{i}
$$

If a principal $P$ is increased or decreased by a sum $A$ at the end of each year, then the value of the principal after $n$ years will be

$$
S=P(1+i)^{n} \pm A \frac{(1+i)^{n}-1}{i}
$$

If the sum $A$ by which the principal $P$ is decreased each year is greater than the total yearly interest on the principal, then the principal, with the accumulated interest, will be entirely used up in $n$ years:

$$
n=\frac{\log A-\log (A-i P)}{\log (1+i)}
$$

Sinking Funds.-Amortization is "the extinction of debt, usually by means of a sinking fund." The sinking fund is created by a fixed investment $R$ placed each year at compound interest for a term of years $n$, and is therefore an annuity of sufficient size to produce at the end of the term of years the amount $S$ necessary for the repayment of the principal of the debt, or to provide a definite sum for other purposes. Then,

$$
S=R \frac{(1+i)^{n}-1}{i} \quad \text { and } \quad R=S \frac{i}{(1+i)^{n}-1}
$$

Example: If $\$ 2,000$ is invested annually for 10 years at 4 per cent compound interest, as a sinking fund, what would be the total amount of the fund at the expiration of the term? Here, $R=2000 ; n=10 ; i=0.04$ :

$$
S=2000 \frac{(1+0.04)^{10}-1}{0.04}=\$ 24,012.21
$$

## Evaluating Investments in Industrial Assets

Investment in industrial assets such as machine tools, processing equipment, and other means of production may not be attractive unless the cost of such investment can be recovered with interest. The interest, or rate of return, should be equal to, or greater than, some specified minimum rate for each of such investments. Three methods used in analyzing prospective investments are

1) Annual cost of the investment at a specified minimum acceptable rate of return used as the interest rate.
2) Present worth, using as an interest rate a specified minimum acceptable rate of return.
3) Prospective rate of return compared to a specified minimum acceptable rate.

Annual Cost Method.-In the annual cost method, comparisons are made among alternative investment plans. If the annual costs in any investment plan form a non-uniform series of disbursements from year to year, a much used method for reducing all comparisons to an equivalent basis is as follows: Take each of the annual disbursements and use the present worth method developed in the next section to bring all annual costs down to a common present worth date, usually called "year 0 ." When this has been done, each present worth is converted to an equivalent uniform annual series of disbursements using the applicable formulas from Table 1.

Table 1. Summary of Useful Interest Formulas

| The meanings of the symbols $P, R, S, L, i, n$, and $F$ are as follows: <br> $P=$ Principal sum of money at the present time. Also the present worth of a future payment in a series of equal payments <br> $R=$ Single payment in a series of $n$ equal payments made at the end of each interest period <br> $S=$ A sum, after $n$ interest period, equal to the compound amount of a principal sum, $P$, or the sum of the compound amounts of the payments, $R$, at interest rate $i$ <br> $i=$ Nominal annual interest rate expressed as a decimal <br> $n=$ Number of interest periods, usually annual <br> $L=$ Salvage value of an asset at the end of its projected useful life <br> $F=(1+i)^{n}$ for which values are tabulated in Table 2 |  |  |  |
| :---: | :---: | :---: | :---: |
| To Find | Given | Formula |  |
| Simple interest, Sum | $P$, find $S$ | $S=P(1+n i)$ | (1) |
| Single payment, Compound-amount | $P$, find $S$ | $S=P F$ | (2) |
| Single payment, Present-worth | $S$, find $P$ | $P=\frac{S}{F}$ | (3) |
| Equal-payment series, Compound-amount | $R$, find $S$ | $S=R \frac{(F-1)}{i}$ | (4) |
| Equal-payment series, Sinking-fund | $S$, find $R$ | $=S \frac{i}{(F-1)}$ | (5) |
| Equal-payment series, Present-worth | $R$, find $P$ | $P=R \frac{(F-1)}{i F}$ | (6) |
| Equal-payment series, Capital-recovery | $P$, find $R$ | $R=P \frac{i F}{(F-1)}$ | (7) |
| Equal-payment series with salvage value, Capital-recovery | $P$ and $L$, find $R$ | $R=(P-L)$ |  |

Example 1 (Annual Cost Calculations): An investment of $\$ 15,000$ is being considered to reduce labor and labor-associated costs in a materials handling operation from $\$ 8,200$ a year to $\$ 3,300$. This operation is expected to be used for 10 years before being changed or discontinued entirely. In addition to the initial investment of $\$ 15,000$ and the annual cost of \$3,300 for labor, there are additional annual costs for power, maintenance, insurance, and property taxes of $\$ 1,800$ associated with the revised operation. Based on comparisons of annual costs, should the $\$ 15,000$ investment be made or the present operation continued?
The present annual cost of the operation is $\$ 8,200$ for labor and labor-associated costs. The proposed operation has an annual cost of $\$ 3,300$ for labor and labor extras plus $\$ 1,800$ for additional power, maintenance, insurance, and taxes, plus the annual cost of recovering the initial investment of $\$ 15,000$ at some interest rate (minimum acceptable rate of return).
Assuming that 10 per cent would be an acceptable rate of return on this investment over a period of 10 years, the annual amount to be recovered on the initial investment would be $\$ 15,000$ multiplied by the capital recovery factor calculated using Formula (7) in Table 1. From Table 2, the factor $F$ for 10 per cent and 10 years is seen to be 2.594 .
Putting this value into Formula (7) gives:

$$
R=P \frac{i F}{F-1}=15,000 \frac{0.1 \times 2.594}{2.594-1}=\$ 2,442
$$

Adding this amount to the $\$ 5,100$ annual cost associated with the investment $(\$ 3,300+$ $\$ 1,800=\$ 5,100$ ) gives a total annual cost of $\$ 7,542$, which is less than the present annual cost of $\$ 8,200$. Thus, the investment is justified unless there are other considerations such
as the effects of income taxes, salvage values, expected life, uncertainty about the required rate of return, changes in the cost of borrowed funds, and others.
A tabulation of annual costs of alternative plans A, B, C, etc., is a good way to compare costs item by item. For Example 1:

| Item | Plan A | Plan B |  |
| :--- | :--- | :---: | ---: |
| 1 | Labor and labor extras | $\$ 8,200.00$ | $\$ 3,300.00$ |
| 2 | Annual cost of $\$ 15,000$ investment using Formula (7), Table 2 |  | $2,442.00$ |
| 3 | Power |  | 400.00 |
| 4 | Maintenance |  | $1,100.00$ |
| 5 | Property taxes and insurance |  | 300.00 |
|  | Total annual cost | $\$ 8,200.00$ | $\$ 7,542.00$ |

Example 2 (Annual Cost Considering Salvage Value): If in Example 1 the salvage value of the equipment installed was $\$ 5,000$ at the end of 10 years, what effect does this have on the annual cost of the proposed investment of $\$ 15,000$ ?
The only item in the annual cost of Example 1 that will be affected is the capital recovery amount of $\$ 2,442$. The following formula gives the amount of annual capital recovery when salvage value is considered:

$$
R=(P-L) \frac{i F}{(F-1)}+L i=(15,000-5,000) \frac{0.1 \times 2.594}{2.594-1}+5,000 \times 0.1=\$ 2,127
$$

Adding this amount to the $\$ 5,100$ annual cost determined previously gives a total annual cost of $\$ 7,227$, which is $\$ 315$ less than the previous annual cost of $\$ 7,542$ for the proposed investment.
Present Worth Method.-A present worth calculation may be described as the discounting of a future payment, or a series of payments, to a cash value on the present date based on a selected interest rate. The present date is referred to as "day 0," or "year 0." Initial costs are already at zero date (present worth date), so no factors need be applied to initial, or "up-front," costs. On the other hand, if salvage values are to be considered, these must be reduced to present worth and subtracted from the present worth of the initial investment.
The present worths of each of the alternative investments are then compared to find the lowest cost alternative. The present worth of the lowest cost alternative may then be converted to a uniform series of annual costs and these annual costs compared with an existing, in-place, annual cost. Present worth calculations are often referred to as discounted cash flow because this term describes both the data required and the method of calculation. Cash flow refers to the requirement that data must be supplied in the form of amounts and dates of receipts and payouts, and discounted refers to the calculation of the present worth of each of one or more future payments. The rate of return used in such calculations should be the minimum attractive interest rate before taxes.
Example 3 (Present Worth Calculation): Present worths are calculated as of the zero date of the payments being compared. Up-front (zero-day) disbursements are already at their present worth and no interest factors should be applied to them; the present worths of salvage values are subtracted to get the present worth of the net disbursements because the present worth of a salvage value, in effect, reduces the amount of required initial disbursements.
A) Find the present value of a salvage value of $\$ 1000$ from the sale of equipment after 10 years if the expected rate of return (interest rate) is 10 per cent? Using Formula (3) from Table 1 and the value of $F=2.594$ for $n=10$ years and $i=0.1$ from Table 2, the present worth $P=1000 / 2.594=\$ 385.51$.
B) In Example 1, the annual cost of an investment of $\$ 15,000$ at 10 per cent over 10 years was $\$ 2,442$. Convert this annual outlay back to its present worth.

Using Formula (6) and the value 2.594 from Table $2, P=2,442 \times(2.594-1) /(0.1 \times$ $2.594)=\$ 15,005$, which rounds to $\$ 15,000$.

Table 2. Values of $F=(1+i)^{n}$ for Selected Rates of Interest, $i$, and Number of Annual Interest Periods, $n$

| Number of Years, $n$ | Annual Interest Rate, $i$, Expressed as a Decimal |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 0.050 | 0.060 | 0.070 | 0.080 | 0.090 | 0.100 | 0.110 | 0.120 | 0.130 | 0.140 | 0.150 | 0.160 |
|  | Factor $F=(1+i)^{n}$ |  |  |  |  |  |  |  |  |  |  |  |
| 1 | 1.050 | 1.060 | 1.070 | 1.080 | 1.090 | 1.100 | 1.110 | 1.120 | 1.130 | 1.140 | 1.150 | 1.160 |
| 2 | 1.103 | 1.124 | 1.145 | 1.166 | 1.188 | 1.210 | 1.232 | 1.254 | 1.277 | 1.300 | 1.323 | 1.346 |
| 3 | 1.158 | 1.191 | 1.225 | 1.260 | 1.295 | 1.331 | 1.368 | 1.405 | 1.443 | 1.482 | 1.521 | 1.561 |
| 4 | 1.216 | 1.262 | 1.311 | 1.360 | 1.412 | 1.464 | 1.518 | 1.574 | 1.630 | 1.689 | 1.749 | 1.811 |
| 5 | 1.276 | 1.338 | 1.403 | 1.469 | 1.539 | 1.611 | 1.685 | 1.762 | 1.842 | 1.925 | 2.011 | 2.100 |
| 6 | 1.340 | 1.419 | 1.501 | 1.587 | 1.677 | 1.772 | 1.870 | 1.974 | 2.082 | 2.195 | 2.313 | 2.436 |
| 7 | 1.407 | 1.504 | 1.606 | 1.714 | 1.828 | 1.949 | 2.076 | 2.211 | 2.353 | 2.502 | 2.660 | 2.826 |
| 8 | 1.477 | 1.594 | 1.718 | 1.851 | 1.993 | 2.144 | 2.305 | 2.476 | 2.658 | 2.853 | 3.059 | 3.278 |
| 9 | 1.551 | 1.689 | 1.838 | 1.999 | 2.172 | 2.358 | 2.558 | 2.773 | 3.004 | 3.252 | 3.518 | 3.803 |
| 10 | 1.629 | 1.791 | 1.967 | 2.159 | 2.367 | 2.594 | 2.839 | 3.106 | 3.395 | 3.707 | 4.046 | 4.411 |
| 11 | 1.710 | 1.898 | 2.105 | 2.332 | 2.580 | 2.853 | 3.152 | 3.479 | 3.836 | 4.226 | 4.652 | 5.117 |
| 12 | 1.796 | 2.012 | 2.252 | 2.518 | 2.813 | 3.138 | 3.498 | 3.896 | 4.335 | 4.818 | 5.350 | 5.936 |
| 13 | 1.886 | 2.133 | 2.410 | 2.720 | 3.066 | 3.452 | 3.883 | 4.363 | 4.898 | 5.492 | 6.153 | 6.886 |
| 14 | 1.980 | 2.261 | 2.579 | 2.937 | 3.342 | 3.797 | 4.310 | 4.887 | 5.535 | 6.261 | 7.076 | 7.988 |
| 15 | 2.079 | 2.397 | 2.759 | 3.172 | 3.642 | 4.177 | 4.785 | 5.474 | 6.254 | 7.138 | 8.137 | 9.266 |
| 16 | 2.183 | 2.540 | 2.952 | 3.426 | 3.970 | 4.595 | 5.311 | 6.130 | 7.067 | 8.137 | 9.358 | 10.748 |
| 17 | 2.292 | 2.693 | 3.159 | 3.700 | 4.328 | 5.054 | 5.895 | 6.866 | 7.986 | 9.276 | 10.761 | 12.468 |
| 18 | 2.407 | 2.854 | 3.380 | 3.996 | 4.717 | 5.560 | 6.544 | 7.690 | 9.024 | 10.575 | 12.375 | 14.463 |
| 19 | 2.527 | 3.026 | 3.617 | 4.316 | 5.142 | 6.116 | 7.263 | 8.613 | 10.197 | 12.056 | 14.232 | 16.777 |
| 20 | 2.653 | 3.207 | 3.870 | 4.661 | 5.604 | 6.727 | 8.062 | 9.646 | 11.523 | 13.743 | 16.367 | 19.461 |
| 21 | 2.786 | 3.400 | 4.141 | 5.034 | 6.109 | 7.400 | 8.949 | 10.804 | 13.021 | 15.668 | 18.822 | 22.574 |
| 22 | 2.925 | 3.604 | 4.430 | 5.437 | 6.659 | 8.140 | 9.934 | 12.100 | 14.714 | 17.861 | 21.645 | 26.186 |
| 23 | 3.072 | 3.820 | 4.741 | 5.871 | 7.258 | 8.954 | 11.026 | 13.552 | 16.627 | 20.362 | 24.891 | 30.376 |
| 24 | 3.225 | 4.049 | 5.072 | 6.341 | 7.911 | 9.850 | 12.239 | 15.179 | 18.788 | 23.212 | 28.625 | 35.236 |
| 25 | 3.386 | 4.292 | 5.427 | 6.848 | 8.623 | 10.835 | 13.585 | 17.000 | 21.231 | 26.462 | 32.919 | 40.874 |
| 26 | 3.556 | 4.549 | 5.807 | 7.396 | 9.399 | 11.918 | 15.080 | 19.040 | 23.991 | 30.167 | 37.857 | 47.414 |
| 27 | 3.733 | 4.822 | 6.214 | 7.988 | 10.245 | 13.110 | 16.739 | 21.325 | 27.109 | 34.390 | 43.535 | 55.000 |
| 28 | 3.920 | 5.112 | 6.649 | 8.267 | 11.167 | 14.421 | 18.580 | 23.884 | 30.633 | 39.204 | 50.066 | 63.800 |
| 29 | 4.116 | 5.418 | 7.114 | 9.317 | 12.172 | 15.863 | 20.624 | 26.750 | 34.616 | 44.693 | 57.575 | 74.009 |
| 30 | 4.322 | 5.743 | 7.612 | 10.063 | 13.268 | 17.449 | 22.892 | 29.960 | 39.116 | 50.950 | 66.212 | 85.850 |

Prospective Rate of Return Method (Discounted Cash Flow).-This method of calculating the prospective return on an investment has variously been called the discounted cash flow method, the Investor's Method, the Profitability Index, and the interest rate of return, but discounted cash flow is the most common terminology in industry.

The term "discounted cash flow" is most descriptive of the process because "cash flow" describes the amounts and dates of the receipts and disbursements and "discounted" refers to the calculation of present worth. Calculating the present worth of future payments is often described as discounting the payments to the present "zero" date.

The process is best illustrated by an example. The data in Table 3 are a tabulation of the cash flows by amount and year for two different plans of investment, the fourth column showing the differences in cash flows for each year and the differences in the totals. This type of information could equally well represent a comparison involving a choice between two different machine tools, investments in rental properties, or any other situation where the difference between two or more alternative investments are to be evaluated.
The differences in cash flows in the fourth column of Table 3 consist of a disbursement of $\$ 15,000$ at date zero and receipts of $\$ 3,000$ per year for 10 years. The rate of return on the net cash flow can be calculated from these data using the principal that the rate of return is that interest rate at which the present worth of the net cash flow is zero.
In this example, the present worth of the net cash flow will be 0 if the present worth of the $\$ 15,000$ disbursements is numerically equal to the present worth of the uniform annual series of receipts of $\$ 3,000$. For the disbursement of $\$ 15,000$, the present worth is already $\$ 15,000$, because it was made on date 0 . The uniform annual series of receipts of $\$ 3,000$ a year for 10 years must be converted to present worth using Formula (6) from Table 1. The interest rate needed to calculate the factor $F$ in Formula (6) to get the necessary present worth conversion factor is not known, so that a series of trial-and-error substitutions of assumed interest rates must be made to find the correct present value factor. As a first guess, assume an interest rate of 15 per cent. Then, from Table 2 , for 15 per cent and 10 years, $F=4.046$, and substituting in Formula (6) of Table 1,

$$
P=3000 \frac{4.046-1}{0.15 \times 4.046}=15,056 \text { nearly }
$$

so that the present worth of the net cash flow at 15 per cent interest $(-\$ 15,000+\$ 15,056=$ $\$ 56)$ is slightly more than 0 . If a 16 per cent interest rate is tried, $P$ is calculated as $\$ 14,499$, which is too small by $\$ 501$ and is about 10 times larger than the previous difference of $\$ 56$. By interpolation, the interest rate should be approximately 15.1 per cent ( 0.1 per cent above 15 per cent, or 0.9 per cent less than 16 per cent $)$. Then $F=(1+0.151)^{10}=4.0809$, and $P=3,000(F-1) /(0.151 \times 4.0809)=3,000(4.0809-1) /(0.151 \times 4.0809)=14,999$, nearly. Thus, the present worth of the net cash flow at 15.1 per cent $(-\$ 15,000+\$ 14,999=$ $-\$ 1$ ) is only slightly less than 0 , and the prospective rate of return may be taken as 15.1 per cent.

Table 3. Comparison of Cash Flows for Two Competing Plans

| Year | Annual Costs <br> Plan A | Annual Costs <br> Plan B | Net Cash Flow <br> B - A |
| :---: | :---: | :---: | :---: |
| 0 | $-\$ 8,000$ | $-\$ 15,000$ | $-\$ 15,000$ |
| 1 | $-8,000$ | $-5,000$ | $+3,000$ |
| 2 | $-8,000$ | $-5,000$ | $+3,000$ |
| 3 | $-8,000$ | $-5,000$ | $+3,000$ |
| 4 | $-8,000$ | $-5,000$ | $+3,000$ |
| 5 | $-8,000$ | $-5,000$ | $+3,000$ |
| 6 | $-8,000$ | $-5,000$ | $+3,000$ |
| 7 | $-8,000$ | $-5,000$ | $+3,000$ |
| 8 | $-8,000$ | $-5,000$ | $+3,000$ |
| 9 | $-8,000$ | $-5,000$ | $+3,000$ |
| 10 | $-\$ 80,000$ | $-5,000$ | $+3,000$ |
| Totals | $-\$ 65,000$ | $+\$ 15,000$ |  |

## Principal Algebraic Expressions and Formulas

$$
\begin{aligned}
& a \times a=a a=a^{2} \\
& a \times a \times a=a a a=a^{3} \\
& a \times b=a b \\
& a^{2} b^{2}=(a b)^{2} \\
& a^{2} a^{3}=a^{2+3}=a^{5} \\
& a^{4} \div a^{3}=a^{4-3}=a \\
& a^{0}=1 \\
& a^{2}-b^{2}=(a+b)(a-b) \\
& (a+b)^{2}=a^{2}+2 a b+b^{2} \\
& (a-b)^{2}=a^{2}-2 a b+b^{2} \\
& \sqrt{a} \times \sqrt{a}=a \\
& \sqrt[3]{a} \times \sqrt[3]{a} \times \sqrt[3]{a}=a \\
& (\sqrt[3]{a})^{3}=a \\
& \sqrt[3]{a^{2}}=(\sqrt[3]{a})^{2}=a^{2 / 3} \\
& \sqrt[4]{\sqrt[3]{a}}=4 \times \sqrt[3]{a}=\sqrt[3]{\sqrt[4]{a}} \\
& \sqrt{a}+\sqrt{b}=\sqrt{a+b+2 \sqrt{a b}}
\end{aligned}
$$

## Equations

An equation is a statement of equality between two expressions, as $5 x=105$. The unknown quantity in an equation is generally designated by the letter $x$. If there is more than one unknown quantity, the others are designated by letters also selected at the end of the alphabet, as $y, z, u, t$, etc.
An equation of the first degree is one which contains the unknown quantity only in the first power, as $3 x=9$. A quadratic equation is one which contains the unknown quantity in the second, but no higher, power, as $x^{2}+3 x=10$.
Solving Equations of the First Degree with One Unknown.-Transpose all the terms containing the unknown $x$ to one side of the equals sign, and all the other terms to the other side. Combine and simplify the expressions as far as possible, and divide both sides by the coefficient of the unknown $x$. (See the rules given for transposition of formulas.)
Example:

$$
\begin{aligned}
22 x-11 & =15 x+10 \\
22 x-15 x & =10+11 \\
7 x & =21 \\
x & =3
\end{aligned}
$$

Solution of Equations of the First Degree with Two Unknowns.-The form of the simplified equations is

$$
\begin{aligned}
a x+b y & =c \\
a_{1} x+b_{1} y & =c_{1}
\end{aligned}
$$

Then,

$$
x=\frac{c b_{1}-c_{1} b}{a b_{1}-a_{1} b} \quad y=\frac{a c_{1}-a_{1} c}{a b_{1}-a_{1} b}
$$

Example:

$$
\begin{aligned}
3 x+4 y & =17 \\
5 x-2 y & =11 \\
x=\frac{17 \times(-2)-11 \times 4}{3 \times(-2)-5 \times 4}= & \frac{-34-44}{-6-20}=\frac{-78}{-26}=3
\end{aligned}
$$

The value of $y$ can now be most easily found by inserting the value of $x$ in one of the equations:

$$
5 \times 3-2 y=11 \quad 2 y=15-11=4 \quad y=2
$$

Solution of Quadratic Equations with One Unknown.-If the form of the equation is $a x^{2}+b x+c=0$, then

$$
x=\frac{-b \pm \sqrt{b^{2}-4 a c}}{2 a}
$$

Example: Given the equation, $1 x^{2}+6 x+5=0$, then $a=1, b=6$, and $c=5$.

$$
x=\frac{-6 \pm \sqrt{6^{2}-4 \times 1 \times 5}}{2 \times 1}=\frac{(-6)+4}{2}=-1 \quad \text { or } \quad \frac{(-6)-4}{2}=-5
$$

If the form of the equation is $a x^{2}+b x=c$, then

$$
x=\frac{-b \pm \sqrt{b^{2}+4 a c}}{2 a}
$$

Example: A right-angle triangle has a hypotenuse 5 inches long and one side which is one inch longer than the other; find the lengths of the two sides.
Let $x=$ one side and $x+1=$ other side; then $x^{2}+(x+1)^{2}=5^{2}$ or $x^{2}+x^{2}+2 x+1=25$; or $2 x^{2}$ $+2 x=24$; or $x^{2}+x=12$. Now referring to the basic formula, $a x^{2}+b x=c$, we find that $a=1$, $b=1$, and $c=12$; hence,

$$
x=\frac{-1 \pm \sqrt{1+4 \times 1 \times 12}}{2 \times 1}=\frac{(-1)+7}{2}=3 \quad \text { or } \quad x=\frac{(-1)-7}{2}=-4
$$

Since the positive value (3) would apply in this case, the lengths of the two sides are $x=3$ inches and $x+1=4$ inches.
Cubic Equations.-If the given equation has the form: $x^{3}+a x+b=0$ then

$$
x=\left(-\frac{b}{2}+\sqrt{\frac{a^{3}}{27}+\frac{b^{2}}{4}}\right)^{1 / 3}+\left(-\frac{b}{2}-\sqrt{\frac{a^{3}}{27}+\frac{b^{2}}{4}}\right)^{1 / 3}
$$

The equation $x^{3}+p x^{2}+q x+r=0$, may be reduced to the form $x_{1}{ }^{3}+a x_{1}+b=0$ by substituting $x_{1}-\frac{p}{3}$ for $x$ in the given equation.

Series.-Some hand calculations, as well as computer programs of certain types of mathematical problems, may be facilitated by the use of an appropriate series. For example, in some gear problems, the angle corresponding to a given or calculated involute function is found by using a series together with an iterative procedure such as the Newton-Raphson
method described on page 35 . The following are those series most commonly used for such purposes. In the series for trigonometric functions, the angles $x$ are in radians ( 1 radian $=180 / \pi$ degrees $)$. The expression $\exp \left(-x^{2}\right)$ means that the base $e$ of the natural logarithm system is raised to the $-x^{2}$ power; $e=2.7182818$.
(1) $\sin x=x-x^{3} / 3!+x^{5} / 5!-x^{7} / 7!+\cdots$
(2) $\cos x=1-x^{2} / 2!+x^{4} / 4!-x^{6} / 6!+\cdots$
(3) $\tan x=x+x^{3} / 3+2 x^{5} / 15+17 x^{7} / 315+62 x^{9} / 2835+\cdots$
(4) $\arcsin x=x+x^{3} / 6+1 \cdot 3 \cdot x^{5} /(2 \cdot 4 \cdot 5)$ $+1 \cdot 3 \cdot 5 \cdot x^{7} /(2 \cdot 4 \cdot 6 \cdot 7)+\cdots$
(5) $\arccos x=\pi / 2-\arcsin x$
(6) $\arctan x=x-x^{3} / 3+x^{5} / 5-x^{7} / 7+\cdots$
(7) $e^{x}=1+x+x^{2} / 2!+x^{3} / 3!+\cdots$
(8) $\exp \left(-x^{2}\right)=1-x^{2}+x^{4} / 2!-x^{6} / 3!+\cdots$
(9) $a^{x}=1+x \log _{e} a+\left(x \log _{e} a\right)^{2} / 2!+\left(x \log _{e} a\right)^{3} / 3!+\cdots$
(10) $\quad 1 /(1+x)=1-x+x^{2}-x^{3}+x^{4}-\cdots$
(11) $\quad 1 /(1-x)=1+x+x^{2}+x^{3}+x^{4}+\cdots$
(12) $1 /(1+x)^{2}=1-2 x+3 x^{2}-4 x^{3}+5 x^{4}-\cdots$
(13) $1 /(1-x)^{2}=1+2 x+3 x^{2}+4 x^{3}+5 x^{5}+\cdots$

$$
\begin{equation*}
\sqrt{(1+x)}=1+x / 2-x^{2} /(2 \cdot 4)+1 \cdot 3 \cdot x^{3} /(2 \cdot 4 \cdot 6) \tag{14}
\end{equation*}
$$

$$
-1 \cdot 3 \cdot 5 \cdot x^{4} /(2 \cdot 4 \cdot 6 \cdot 8)-\cdots
$$ ) $1 /(\sqrt{1+x})=1-x / 2+1 \cdot 3 \cdot x^{2} /(2 \cdot 4)-1 \cdot 3 \cdot 5 \cdot x^{3} /(2 \cdot 4 \cdot 6)$ $+\cdots$

(16) $(a+x)^{n}=a^{n}+n a^{n-1} x+n(n-1) a^{n-2} x^{2} / 2$ ! $+n(n-1)(n-2) a^{n-3} x^{3} / 3!+\cdots$
for all values of $x$.
for all values of $x$.
for $|x|<\pi / 2$.
for $|x| \leq 1$.
for $|x| \leq 1$.
for all values of $x$.
for all values of $x$.
for all values of $x$.
for $|x|<1$.
for $|x|<1$.
for $|x|<1$.
for $|x|<1$.
for $|x|<1$.
for $|x|<1$.
for $x^{2}<a^{2}$.

Derivatives of Functions.-The following are formulas for obtaining the derivatives of basic mathematical functions. In these formulas, the letter $a$ denotes a constant; the letter $x$ denotes a variable; and the letters $u$ and $v$ denote functions of the variable $x$. The expression $\mathrm{d} / \mathrm{d} x$ means the derivative with respect to $x$, and as such applies to whatever expression in parentheses follows it. Thus, $\mathrm{d} / \mathrm{d} x(a x)$ means the derivative with respect to $x$ of the product ( $a x$ ) of the constant $a$ and the variable $x$, as given by formula (3).
To simplify the form of the formulas, the symbol $D$ is used to represent $\mathrm{d} / \mathrm{d} x$. Thus, D is equivalent to $\mathrm{d} / \mathrm{d} x$ and other forms as follows:

$$
\mathrm{D}(a x)=\frac{\mathrm{d}(a x)}{\mathrm{d} x}=\frac{\mathrm{d}}{\mathrm{~d} x}(a x)
$$

1) $\mathrm{D}(a)=0 \quad$ 2) $\mathrm{D}(x)=1 \quad$ 3) $\mathrm{D}(a x)=a \cdot \mathrm{D}(x)=a \cdot 1=a$
2) $\mathrm{D}(u+v)=\mathrm{D}(u)+\mathrm{D}(v)$ Example: $\mathrm{D}\left(x^{4}+2 x^{2}\right)=4 x^{3}+4 x$
3) $\mathrm{D}(u v)=v \cdot \mathrm{D}(u)+u \cdot \mathrm{D}(v)$ Example: $\mathrm{D}\left(x^{2} \cdot a x^{3}\right)=a x^{3} \cdot 2 x+x^{2} \cdot 3 a x^{2}=5 a x^{4}$
4) $\mathrm{D}(u / v)=\frac{v \cdot \mathrm{D}(u)-u \cdot \mathrm{D}(v)}{v^{2}}$ Example: $\mathrm{D}\left(a x^{2} / \sin x\right)=\left(2 a x \cdot \sin x-a x^{2} \cdot \cos x\right) / \sin ^{2} x$
5) $\mathrm{D}\left(x^{n}\right)=n \cdot x^{n-1}$ Example: $\mathrm{D}\left(5 x^{7}\right)=35 x^{6}$
6) $\mathrm{D}\left(e^{x}\right)=e^{x}$
7) $\mathrm{D}\left(a^{x}\right)=a^{x} \cdot \log _{e} a$ Example: $\mathrm{D}\left(11^{x}\right)-11^{x} \cdot \log _{e} 11$
8) $\mathrm{D}\left(u^{v}\right)=v \cdot u^{v-1} \cdot \mathrm{D}(u)+u^{v} \cdot \log _{e} u \cdot \mathrm{D}(v)$
9) $\mathrm{D}\left(\log _{e} x\right)=1 / x$
10) $\mathrm{D}\left(\log _{a} x\right)=1 / x \cdot \log _{e} a=\log _{a} e / x$
11) $\mathrm{D}(\sin x)=\cos x \quad$ Example: $\mathrm{D}(a \cdot \sin x)=a \cdot \cos x$
12) $\mathrm{D}(\cos x)=\sin x \quad 15) \mathrm{D}(\tan x)=\sec ^{2} x$

Solving Numerical Equations Having One Unknown.-The Newton-Raphson method is a procedure for solving various kinds of numerical algebraic and transcendental equations in one unknown. The steps in the procedure are simple and can be used with either a handheld calculator or as a subroutine in a computer program.
Examples of types of equations that can be solved to any desired degree of accuracy by this method are

$$
\begin{gathered}
f(x)=x^{2}-101=0, \quad f(x)=x^{3}-2 x^{2}-5=0 \\
\text { and } f(x)=2.9 x-\cos x-1=0
\end{gathered}
$$

The procedure begins with an estimate, $r_{1}$, of the root satisfying the given equation. This estimate is obtained by judgment, inspection, or plotting a rough graph of the equation and observing the value $r_{1}$ where the curve crosses the $x$ axis. This value is then used to calculate values $r_{2}, r_{3}, \ldots, r_{n}$ progressively closer to the exact value.
Before continuing, it is necessary to calculate the first derivative. $f^{\prime}(x)$, of the function. In the above examples, $f^{\prime}(x)$ is, respectively, $2 x, 3 x^{2}-4 x$, and $2.9+\sin x$. These values were found by the methods described in Derivatives of Functions on page 34.
In the steps that follow,
$r_{1}$ is the first estimate of the value of the root of $f(x)=0$;
$f\left(r_{1}\right)$ is the value of $f(x)$ for $x=r_{1}$;
$f^{\prime}(x)$ is the first derivative of $f(x)$;
$f^{\prime}\left(r_{1}\right)$ is the value of $f^{\prime}(x)$ for $x=r_{1}$.
The second approximation of the root of $f(x)=0, r_{2}$, is calculated from

$$
r_{2}=r_{1}-\left[f\left(r_{1}\right) / f^{\prime}\left(r_{1}\right)\right]
$$

and, to continue further approximations,

$$
r_{n}=r_{n-1}-\left[f\left(r_{n-1}\right) / f^{\prime}\left(r_{n-1}\right)\right]
$$

Example: Find the square root of 101 using Newton-Raphson methods. This problem can be restated as an equation to be solved, i.e., $f(x)=x^{2}-101=0$
Step 1. By inspection, it is evident that $r_{1}=10$ may be taken as the first approximation of the root of this equation. Then, $f\left(r_{1}\right)=f(10)=10^{2}-101=-1$
Step 2. The first derivative, $f^{\prime}(x)$, of $x^{2}-101$ is $2 x$ as stated previously, so that

$$
f^{\prime}(10)=2(10)=20 .
$$

Then,

$$
\begin{aligned}
\left.r_{2}=r_{1}-f\left(r_{l}\right)\right) f^{\prime}\left(r_{1}\right)=10-(-1) / 20 & =10+0.05=10.05 . \\
\text { Check: } 10.05^{2} & =101.0025 ; \text { error }=0.0025
\end{aligned}
$$

Step 3. The next, better approximation is

$$
\begin{aligned}
r_{3} & =r_{2}-\left[f\left(r_{2}\right) / f^{\prime}\left(r_{2}\right)\right]=10.05-\left[f(10.05) / f^{\prime}(10.05)\right] \\
& =10.05-\left[\left(10.05^{2}-101\right) / 2(10.05)\right]=10.049875
\end{aligned}
$$

Check: $10.049875^{2}=100.9999875 ;$ error $=0.0000125$

## Coordinate Systems

Rectangular, Cartesian Coordinates.-In a Cartesian coordinate system the coordinate axes are perpendicular to one another, and the same unit of length is chosen on the two axes. This rectangular coordinate system is used in the majority of cases.
The general form of an equation of a line in a Cartesian coordinate system is $y=m x+b$, where $(x, y)$ is a point on the line, $m$ is the slope (the rate at which the line is increasing or decreasing), and $b$ is the $y$ coordinate, the $y$-intercept, of the point $(0, b)$ on the $y$-axis where the line intersects the axis at $x=0$.

Another form of the equation of a line is the point-slope form $\left(y-y_{1}\right)=m\left(x-x_{1}\right)$. The slope, $m$, is defined as a ratio of the change in the $y$ coordinates, $y_{2}-y_{1}$, to the change in the $x$ coordinates, $x_{2}-x_{1}$,

$$
m=\frac{\Delta y}{\Delta x}=\frac{y_{2}-y_{1}}{x_{2}-x_{1}}
$$

Example 1:Find the general equation of a line passing through the points $(3,2)$ and $(5,6)$, and it's intersection point with the $y$-axis.
First, find the slope using the equation above

$$
m=\frac{\Delta y}{\Delta x}=\frac{6-2}{5-3}=\frac{4}{2}=2
$$

The line has a general form of $y=2 x+b$, and the value of the constant $b$ can be determined by substituting the coordinates of a point on the line into the general form. Using point $(3,2), 2=2 \times 3+b$ and rearranging, $b=2-6=-4$. As a check, using another point on the line, (5,6), yields equivalent results, $y=6=2 \times 5+b$ and $b=6-10=-4$.
The equation of the line, therefore, is $y=2 x-4$, indicating that line $y=2 x-4$ intersects the $y$-axis at point $(0,-4)$, the $y$-intercept.
Example 2: Using the point-slope form find the equation of a line passing through the point $(3,2)$ and having a slope of 2 .

$$
\begin{aligned}
(y-2) & =2(x-3) \\
y & =2 x-6+2 \\
y & =2 x-4
\end{aligned}
$$

Because the slope, 2 , is positive the line is increasing and the line passes through the $y$ axis at the $y$-intercept at a value of -4 .
Polar Coordinates.- Another coordinate system is determined by a fixed point O, the origin or pole, and a zero direction or axis through it, on which positive lengths can be laid off and measured, as a number line. A point $P$ can be fixed to the zero direction line at a distance $r$ away and then rotated in a positive sense at an angle $u$. The angle, $u$, in polar coordinates can take on values from $0^{\circ}$ to $360^{\circ}$. A point in polar coordinates takes the form of ( $u, r$ ).

Changing Coordinate Systems.-For simplicity it may be assumed that the origin on a Cartesian coordinate system coincides with the pole on a polar coordinate system, and it's axis with the x -axis. Then, if point P has polar coordinates of $(u, r)$ and Cartesian coordinates of $(x, y)$, by trigonometry $x=r \times \cos (u)$ and $y=r \times \sin (u)$. By the Pythagorean theorem and trigonometry

$$
r=\sqrt{x^{2}+y^{2}} \quad \theta=\operatorname{atan} \frac{y}{x}
$$

Example 1: Convert the Cartesian coordinate $(3,2)$ into polar coordinates.

$$
r=\sqrt{3^{2}+2^{2}}=\sqrt{9+4}=\sqrt{13}=3.6 \quad \theta=\operatorname{atan} \frac{2}{3}=33.78^{\circ}
$$

Therefore the point $(3.6,33.78)$ is the polar form of the Cartesian point $(3,2)$.
Graphically, the polar and Cartesian coordinates are related in the following figure


Example 2: Convert the polar form $(5,608)$ to Cartesian coordinates. By trigonometry, $x$ $=r \times \cos (u)$ and $y=r \times \sin (u)$. Then $x=5 \cos 608=2.5$ and $y=5 \sin 608=4.33$. Therefore, the Cartesian point equivalent is $(2.5,4.33)$.
Spherical Coordinates.-It is convenient in certain problems, for example, those concerned with spherical surfaces, to introduce non-parallel coordinates. An arbitrary point $P$ in space can be expressed in terms of the distance $r$ between point $P$ and the origin $O$, the angle $\phi$ that $O P^{\prime}$ makes with the $x-y$ plane, and the angle $\lambda$ that the projection $O P^{\prime}$ (of the segment $O P$ onto the $x-y$ plane) makes with the positive $x$-axis.


The rectangular coordinates of a point in space can therefore be calculated by the following formulas

Relationship Between Spherical and Rectangular Coordinates

| Spherical to Rectangular | Rectangular to Spherical |  |
| :---: | :--- | :--- |
| $x=\cos \phi \cos \lambda$ | $r=\sqrt{x^{2}+y^{2}+z^{2}}$ |  |
| $y=r \cos \phi \sin \lambda$ | $\phi=\operatorname{atan} \frac{z}{\sqrt{x^{2}+y^{2}}}$ | $\left(\right.$ for $\left.x^{2}+y^{2} \neq 0\right)$ |
| $z=r \sin \phi$ | $\lambda=\operatorname{atan} \frac{y}{x}$ | (for $x>0, y>0$ ) |
|  | $\lambda=\pi+\operatorname{atan} \frac{y}{x}$ | (for $x<0$ ) |
|  | $\lambda=2 \pi+\operatorname{atan} \frac{y}{x}$ | (for $x>0, \mathrm{y}<0$ ) |

Example: What are the spherical coordinates of the point $P(3,4,-12)$ ?

$$
\begin{gathered}
r=\sqrt{3^{2}+(-4)^{2}+(-12)^{2}}=13 \\
\phi=\operatorname{atan} \frac{-12}{\sqrt{3^{2}+(-4)^{2}}}=\operatorname{atan}-\frac{12}{5}=-67.38^{\circ} \\
\lambda=360^{\circ}+\operatorname{atan}-\frac{4}{3}=360^{\circ}-53.13^{\circ}=306.87^{\circ}
\end{gathered}
$$

The spherical coordinates of $P$ are therefore $r=13, \phi=267.388$, and $\lambda=306.878$.
Cylindrical Coordinates.-For problems on the surface of a cylinder it is convenient to use cylindrical coordinates. The cylindrical coordinates $r, \theta, z$, of $P$ coincide with the polar coordinates of the point $\mathrm{P}^{\prime}$ in the $\mathrm{x}-\mathrm{y}$ plane and the rectangular $z$-coordinate of $P$. This gives the conversion formula. Those for $\theta$ hold only if $x^{2}+y^{2} \neq 0 ; \theta$ is undetermined if $x=y=0$.

| Cylindrical to Rectangular | Rectangular to Cylindrical |
| :---: | :---: |
| $x=r \cos \theta$ | $r=\frac{1}{\sqrt{x^{2}+y^{2}}}$ |
| $y=r \sin \theta$ | $\cos \theta=\frac{x}{\sqrt{x^{2}+y^{2}}}$ |
| $z=z$ |  |
| $z=\frac{y}{\sqrt{x^{2}+y^{2}}}$ |  |

Example: Given the cylindrical coordinates of a point $P, r=3, \theta=-30^{\circ}, z=51$, find the rectangular coordinates. Using the above formulas $x=3 \cos \left(-30^{\circ}\right)=3 \cos \left(30^{\circ}\right)=2.598 ; y$ $=3 \sin \left(-30^{\circ}\right)=-3 \sin \left(30^{\circ}\right)=-1.5$; and $z=51$. Therefore, the rectangular coordinates of point $P$ are $x=2.598, y=-1.5$, and $z=51$.

## Imaginary and Complex Numbers

Complex or Imaginary Numbers.-Complex or imaginary numbers represent a class of mathematical objects that are used to simplify certain problems, such as the solution of polynomial equations. The basis of the complex number system is the unit imaginary number $i$ that satisfies the following relations:

$$
i^{2}=(-i)^{2}=-1 \quad i=\sqrt{-1} \quad-i=-\sqrt{-1}
$$

In electrical engineering and other fields, the unit imaginary number is often represented by $j$ rather than $i$. However, the meaning of the two terms is identical.
Rectangular or Trigonometric Form: Every complex number, $Z$, can be written as the sum of a real number and an imaginary number. When expressed as a sum, $Z=a+b i$, the complex number is said to be in rectangular or trigonometric form. The real part of the number is $a$, and the imaginary portion is $b i$ because it has the imaginary unit assigned to it.
Polar Form: A complex number $Z=a+b i$ can also be expressed in polar form, also known as phasor form. In polar form, the complex number $Z$ is represented by a magnitude $r$ and an angle $\theta$ as follows:

$$
Z=r \angle \theta
$$

where $\angle \theta=$ a direction, the angle whose tangent is $b \div a$, thus $\theta=\operatorname{atan} \frac{b}{a}$; and, $r=$ a magnitude $=\sqrt{a^{2}+b^{2}}$.
A complex number can be plotted on a real-imaginary coordinate system known as the complex plane. The figure below illustrates the relationship between the rectangular coordinates $a$ and $b$, and the polar coordinates $r$ and $\theta$.


Complex Number in the Complex Plane
The rectangular form can be determined from $r$ and $\theta$ as follows:

$$
a=r \cos \theta \quad b=r \sin \theta \quad a+b i=r \cos \theta+i r \sin \theta=r(\cos \theta+i \sin \theta)
$$

The rectangular form can also be written using Euler's Formula:

$$
e^{ \pm i \theta}=\cos \theta \pm i \sin \theta \quad \sin \theta=\frac{e^{i \theta}-e^{-i \theta}}{2 i} \quad \cos \theta=\frac{e^{i \theta}+e^{-i \theta}}{2}
$$

Complex Conjugate: Complex numbers commonly arise in finding the solution of polynomials. A polynomial of $n^{\text {th }}$ degree has $n$ solutions, an even number of which are complex and the rest are real. The complex solutions always appear as complex conjugate pairs in the form $a+b i$ and $a-b i$. The product of these two conjugates, $(a+b i) \times(a-b i)=a^{2}+b^{2}$, is the square of the magnitude $r$ illustrated in the previous figure.

## Operations on Complex Numbers

Example 3, Addition: When adding two complex numbers, the real parts and imaginary parts are added separately, the real parts added to real parts and the imaginary to imaginary parts. Thus,

$$
\begin{aligned}
& \left(a_{1}+i b_{1}\right)+\left(a_{2}+i b_{2}\right)=\left(a_{1}+a_{2}\right)+i\left(b_{1}+b_{2}\right) \\
& \left(a_{1}+i b_{1}\right)-\left(a_{2}+i b_{2}\right)=\left(a_{1}-a_{2}\right)+i\left(b_{1}-b_{2}\right) \\
& (3+4 i)+(2+i)=(3+2)+(4+1) i=5+5 i
\end{aligned}
$$

Example 4, Multiplication: Multiplication of two complex numbers requires the use of the imaginary unit, $i^{2}=-1$ and the algebraic distributive law.

$$
\begin{gathered}
\left(a_{1}+i b_{1}\right)\left(a_{2}+i b_{2}\right)=a_{1} a_{2}+i a_{1} b_{2}+i a_{2} b_{1}+i^{2} b_{1} b_{2} \\
=a_{1} a_{2}+i a_{1} b_{2}+i a_{2} b_{1}-b_{1} b_{2} \\
(7+2 i) \times(5-3 i)=(7)(5)-(7)(3 i)+(2 i)(5)-(2 i)(3 i) \\
= \\
=35-21 i+10 i-6 i^{2} \\
= \\
=45-21 i+10 i-(6)(-1)
\end{gathered}
$$

Multiplication of two complex numbers, $Z_{1}=r_{1}\left(\cos \theta_{1}+i \sin \theta_{1}\right)$ and $Z_{2}=r_{2}\left(\cos \theta_{2}+\right.$ $i \sin \theta_{2}$ ), results in the following:

$$
Z_{1} \times Z_{2}=r_{1}\left(\cos \theta_{1}+i \sin \theta_{1}\right) \times r_{2}\left(\cos \theta_{2}+i \sin \theta_{2}\right)=r_{1} r_{2}\left[\cos \left(\theta_{1}+\theta_{2}\right)+i \sin \left(\theta_{1}+\theta_{2}\right)\right]
$$

Example 5, Division: Divide the following two complex numbers, $2+3 i$ and $4-5 i$. Dividing complex numbers makes use of the complex conjugate.

$$
\frac{2+3 i}{4-5 i}=\frac{(2+3 i)(4+5 i)}{(4-5 i)(4+5 i)}=\frac{8+12 i+10 i+15 i^{2}}{16+20 i-20 i-25 i^{2}}=\frac{-7+22 i}{16+25}=\left(\frac{-7}{41}\right)+i\left(\frac{22}{41}\right)
$$

Example 6: Convert the complex number $8+6 i$ into phasor form.
First find the magnitude of the phasor vector and then the direction.

$$
\text { magnitude }=\sqrt{8^{2}+6^{2}}=\sqrt{100}=10 \quad \text { direction }=\operatorname{atan} \frac{6}{8}=\operatorname{atan} 0.75=36.87^{\circ}
$$

$$
\text { phasor }=10 \angle 36.87^{\circ}
$$

## Break-Even Analysis

Break-Even Analysis.-Break-even analysis is a method of comparing two or more alternatives to determine which works best. Frequently, cost is the basis of the comparison, with the least expensive alternative being the most desirable. Break-even analysis can be applied in situations such as: to determine if it is more efficient and cost effective to use HSS, carbide, or ceramic tooling; to compare coated versus uncoated carbide tooling; to decide which of several machines should be used to produce a part; or to decide whether to buy a new machine for a particular job or to continue to use an older machine. The techniques used to solve any of these problems are the same; however, the details will be different, depending on the type of comparison being made. The remainder of this section deals with break-even analysis based on comparing the costs of manufacturing a product using different machines.
Choosing a Manufacturing Method: The object of this analysis is to decide which of several machines can produce parts at the lowest cost. In order to compare the cost of producing a part, all the costs involved in making that part must be considered. The cost of manufacturing any number of parts can be expressed as the sum: $C_{T}=C_{F}+n \times C_{V}$, where $C_{T}$ is the total cost of manufacturing one part, $C_{F}$ is the sum of the fixed costs of making the parts, $n$ is the number of parts made, and $C_{V}$ is the total variable costs per piece made.
Fixed costs are manufacturing costs that have to be paid whatever the number of parts is produced and usually before any parts can be produced. They include the cost of drafting and CNC part programs, the cost of special tools and equipment required to make the part, and the cost of setting up the machine for the job. Fixed costs are generally one-time charges that occur at the beginning of a job or are recurrent charges that do not depend on the number of pieces made, such as those that might occur each time a job is run again.
Variable costs depend on the number of parts produced and are expressed as the cost per part made. The variable costs include the cost of materials, the cost of machine time, the cost of the labor directly involved in making the part, and the portion of the overhead that is attributable to production of the part. Variable costs can be expressed as: $C_{V}=$ material cost + machine cost + labor cost + overhead cost. When comparing alternatives, if the same cost is incurred by each alternative, then that cost can be eliminated from the analysis without affecting the result. For example, the cost of material is frequently omitted from a manufacturing analysis if each machine is going to make parts from the same stock and if there is not going to be a significant difference in the amount of scrap produced by each method. The time to produce one part is needed to determine the machine, labor, and overhead costs. The total time expressed in hours per part is $t_{T}=t_{f}+t_{s}$, where $t_{f}$ equals the floor-tofloor production time for one part and $t_{s}$ the setup time per part. The setup time, $t_{s}$, is the time spent setting up the machine and periodically reconditioning tooling, divided by the number of parts made per setup.
Material cost equals the cost of the materials divided by the number of parts made.

Machine cost is the portion of a machine's total cost that is charged toward the production of each part. It is found by multiplying the machine rate (cost of the machine per hour) by the machine time per part, $t_{f}$. The machine hourly rate is calculated by dividing the lifetime costs (including purchase price, insurance, maintenance, etc.) by the estimated lifetime hours of operation of the machine. The total operating hours may be difficult to determine but a reasonable number can be based on experience and dealer information.
Labor costs are the wages paid to people who are directly involved in the manufacture of the part. The labor cost per part is the labor rate per hour multiplied by the time needed to manufacture each part, $t_{T}$. Indirect labor, which supports but is not directly involved in the manufacture of the part, is charged as overhead.
Overhead cost is the cost of producing an item that is not directly related to the cost of manufacture. Overhead includes the cost of management and other support personnel, building costs, heating and cooling, and similar expenses. Often, overhead is estimated as a percentage of the largest component cost of producing a part. For example, if direct labor is the largest expense in producing a part, the overhead can be estimated as a percentage of the direct labor costs. On the other hand, if equipment costs are higher, the overhead would be based on a percentage of the machine cost. Depending on the company, typical overhead charges range from about 150 to 800 per cent of the highest variable cost.
Most of the time, the decision to use one machine or another for making parts depends on how many pieces are needed. For example, given three machines $A, B$, and $C$, if only a few parts need to be produced, then, in terms of cost, machine $A$ might be the best; if hundreds of parts are needed, then machine $B$ might be best; and, if thousands of components are to be manufactured, then machine $C$ may result in the lowest cost per part. Break-even analysis reveals how many components need to be produced before a particular machine becomes more cost effective than another.
To use break-even analysis, the cost of operating each machine needs to be established. The costs are plotted on a graph as a function of the number of components to be manufactured to learn which machine can make the required parts for the least cost. The following graph is a plot of the fixed and variable costs of producing a quantity of parts on two different machines, Machine 1 and Machine 2. Fixed costs for each machine are plotted on the vertical cost axis. Variable costs for each machine are plotted as a line that intersects the cost axis at the fixed cost for each respective machine. The variable cost line is constructed with a slope that is equal to the cost per part, that is, for each part made, the line rises by an amount equal to the cost per part. If the calculations necessary to produce the graph are done carefully, the total cost of producing any quantity of parts can be found from the data plotted on the graph.


Quantity of Parts

As an example, the graph shown is a comparison of the cost of manufacturing a quantity of a small part on a manually operated milling machine (Machine 1) and on a CNC machining center (Machine 2). The fixed costs (fixed costs $=$ lead time $\times$ lead time rate + setup time $\times$ setup rate) for the manual machine are $\$ 190$ and the fixed costs for the CNC machine are higher at $\$ 600$. The fixed cost for each machine is the starting point of the line representing the cost of manufacturing a quantity of parts with that machine. The variable costs plotted are: $\$ 18$ per piece for the manual machine and $\$ 5$ per piece for the CNC mill.

The variable costs are calculated using the machine, labor, and overhead costs. The cost of materials is not included because it is assumed that materials cost will be the same for parts made on either machine and there will be no appreciable difference in the amount of scrap generated. The original cost of Machine 1 (the manual milling machine) is $\$ 19,000$ with an estimated operating life of 16,000 hours, so the hourly operating cost is 19,000 / $16,000=\$ 1.20$ per hour. The labor rate is $\$ 17$ per hour and the overhead is estimated as 1.6 times the labor rate, or $\$ 17 \times 1.6=\$ 27.20$ per hour. The time, $t_{f}$, needed to complete each part on Machine 1 is estimated as 24 minutes ( 0.4 hour). Therefore, by using Machine 1, the variable cost per part excluding material is $(1.20+17.00+27.20) \$ / \mathrm{h} \times 0.4 \mathrm{~h} / \mathrm{part}=\$ 18$ per part. For Machine 2 (the CNC machining center), the machine cost is calculated at $\$ 3$ per hour, which is based on a $\$ 60,000$ initial cost (including installation, maintenance, insurance, etc.) and 20,000 hours of estimated lifetime. The cost of labor is $\$ 15$ per hour for Machine 2 and the overhead is again calculated at 1.6 times the labor rate, or $\$ 24$ per hour. Each part is estimated to take 7.2 minutes $(0.12 \mathrm{~h})$ to make, so the variable cost per part made on Machine 2 is $(3+15+24) \$ / \mathrm{h} \times 0.12 \mathrm{~h} /$ part $=\$ 5$ per part.

The lines representing the variable cost of operating each machine intersect at only one point on the graph. The intersection point corresponds to a quantity of parts that can be made by either the CNC or manual machine for the same cost, which is the break-even point. In the figure, the break-even point is 31.5 parts and the cost of those parts is $\$ 757$, or about $\$ 24$ apiece, excluding materials. The graph shows that if fewer than 32 parts need to be made, the total cost will be lowest if the manual machine is used because the line representing Machine 1 is lower (representing lower cost) than the line representing Machine 2. On the other hand, if more than 31 parts are going to be made, the CNC machine will produce them for a lower cost. It is easy to see that the per piece cost of manufacturing is lower on the CNC machine because the line for Machine 2 rises at a slower rate than the line for Machine 1. For producing only a few parts, the manual machine will make them less expensively than the CNC because the fixed costs are lower, but once the CNC part program has been written, the CNC can also run small batches efficiently because very little setup work is required.

The quantity of parts corresponding to the break-even point is known as the break-even quantity $Q_{b}$. The break-even quantity can be found without the use of the graph by using the following break-even equation: $Q_{b}=\left(C_{F 1}-C_{F 2}\right) /\left(C_{V 2}-C_{V 1}\right)$. In this equation, the $C_{F 1}$ and $C_{F 2}$ are the fixed costs for Machine 1 and Machine 2, respectively: $C_{V 1}$ and $C_{V 2}$ are the variable costs for Machine 1 and Machine 2, respectively.

Break-even analysis techniques are also useful for comparing performance of more than two machines. Plot the manufacturing costs for each machine on a graph as before and then compare the costs of the machines in pairs using the techniques described. For example, if an automatic machine such as a rotary transfer machine is included as Machine 3 in the preceding analysis, then three lines representing the costs of operating each machine would be plotted on the graph. The equation to find the break-even quantities is applied three times in succession, for Machines 1 and 2, for Machines 1 and 3, and again for Machines 2 and 3 . The result of this analysis will show the region (range of quantities) within which each machine is most profitable.

## GEOMETRY

## Arithmetical Progression

An arithmetical progression is a series of numbers in which each consecutive term differs from the preceding one by a fixed amount called the common difference, $d$. Thus, 1, 3, 5, 7, etc., is an arithmetical progression where the difference $d$ is 2 . The difference here is added to the preceding term, and the progression is called increasing. In the series $13,10,7,4$, etc., the difference is ( -3 ), and the progression is called decreasing. In any arithmetical progression (or part of progression), let

$$
\begin{aligned}
a & =\text { first term considered } \\
l & =\text { last term considered } \\
n & =\text { number of terms } \\
d & =\text { common difference } \\
S & =\text { sum of } n \text { terms }
\end{aligned}
$$

Then the general formulas are $l=a+(n-1) d \quad$ and $\quad S=\frac{a+l}{2} \times n$
In these formulas, $d$ is positive in an increasing and negative in a decreasing progression. When any three of the preceding live quantities are given, the other two can be found by the formulas in the accompanying table of arithmetical progression.
Example: In an arithmetical progression, the first term equals 5, and the last term 40. The difference is 7 . Find the sum of the progression.

$$
S=\frac{a+l}{2 d}(l+d-a)=\frac{5+40}{2 \times 7}(40+7-5)=135
$$

## Geometrical Progression

A geometrical progression or a geometrical series is a series in which each term is derived by multiplying the preceding term by a constant multiplier called the ratio. When the ratio is greater than 1 , the progression is increasing; when less than 1 , it is decreasing. Thus, $2,6,18,54$, etc., is an increasing geometrical progression with a ratio of 3 , and 24, 12,6 , etc., is a decreasing progression with a ratio of $1 / 2$.
In any geometrical progression (or part of progression), let

$$
\begin{aligned}
a & =\text { first term } \\
l & =\text { last (or } n \text { th) term } \\
n & =\text { number of terms } \\
r & =\text { ratio of the progression } \\
S & =\text { sum of } n \text { terms }
\end{aligned}
$$

Then the general formulas are $l=a r^{n-1} \quad$ and $\quad S=\frac{r l-a}{r-1}$
When any three of the preceding five quantities are given, the other two can be found by the formulas in the accompanying table. For instance, geometrical progressions are used for finding the successive speeds in machine tool drives, and in interest calculations.

Example: The lowest speed of a lathe is 20 rpm . The highest speed is 225 rpm . There are 18 speeds. Find the ratio between successive speeds.

$$
\text { Ratio } r=\sqrt[n-1]{\frac{l}{a}}=\sqrt[17]{\frac{225}{20}}=\sqrt[17]{11.25}=1.153
$$

Formulas for Arithmetical Progression

| To Find | Given | Use Equation |
| :---: | :---: | :---: |
| $a$ | $\begin{array}{ccc} d & l & n \\ d & n & S \\ d & l & S \\ l & n & S \end{array}$ | $\begin{aligned} & a=l-(n-1) d \\ & a=\frac{S}{n}-\frac{n-1}{2} \times d \\ & a=\frac{d}{2} \pm \frac{1}{2} \sqrt{(2 l+d)^{2}-8 d S} \\ & a=\frac{2 S}{n}-l \end{aligned}$ |
| $d$ | $\begin{array}{ccc} a & l & n \\ a & n & S \\ a & l & S \\ l & n & S \end{array}$ | $\begin{aligned} & d=\frac{l-a}{n-1} \\ & d=\frac{2 S-2 a n}{n(n-1)} \\ & d=\frac{l^{2}-a^{2}}{2 S-l-a} \\ & d=\frac{2 n l-2 S}{n(n-1)} \end{aligned}$ |
| $l$ | $\begin{array}{lll} a & d & n \\ a & d & S \\ a & n & S \\ d & n & S \end{array}$ | $\begin{aligned} & l=a+(n-1) d \\ & l=-\frac{d}{2} \pm \frac{1}{2} \sqrt{8 d S+(2 a-d)^{2}} \\ & l=\frac{2 S}{n}-a \\ & l=\frac{S}{n}+\frac{n-1}{2} \times d \end{aligned}$ |
| $n$ | $\begin{array}{lll} a & d & l \\ a & d & S \\ a & l & S \\ d & l & S \end{array}$ | $\begin{aligned} & n=1+\frac{l-a}{d} \\ & n=\frac{d-2 a}{2 d} \pm \frac{1}{2 d} \sqrt{8 d S+(2 a-d)^{2}} \\ & n=\frac{2 S}{a+l} \\ & n=\frac{2 l+d}{2 d} \pm \frac{1}{2 d} \sqrt{(2 l+d)^{2}-8 d S} \end{aligned}$ |
| $S$ | $\begin{array}{lll} a & d & n \\ a & d & l \\ a & l & n \\ d & l & n \end{array}$ | $\begin{aligned} & S=\frac{n}{2}[2 a+(n-1) d] \\ & S=\frac{a+l}{2}+\frac{l^{2}-a^{2}}{2 d}=\frac{a+l}{2 d}(l+d-a) \\ & S=\frac{n}{2}(a+l) \\ & S=\frac{n}{2}[2 l-(n-1) d] \end{aligned}$ |

Formulas for Geometrical Progression

\begin{tabular}{|c|c|c|c|c|}
\hline To Find \& \multicolumn{3}{|c|}{Given} \& Use Equation \\
\hline \(a\) \& \begin{tabular}{l}
\(l\) \\
\(n\) \\
\(l\) \\
\(l\)
\end{tabular} \&  \& \begin{tabular}{l}
\(S\) \\
\(S\) \\
\(S\)
\end{tabular} \& \[
\begin{aligned}
\& a=\frac{l}{r^{n-1}} \\
\& a=\frac{(r-1) S}{r^{n}-1} \\
\& a=l r-(r-1) S \\
\& a(S-a)^{n-1}=l(S-1)^{n-1}
\end{aligned}
\] \\
\hline \(l\) \&  \& \begin{tabular}{l}
\(r\) \\
\(n\)
\end{tabular} \& \begin{tabular}{l}
\(S\) \\
\(S\) \\
\(S\)
\end{tabular} \& \[
\begin{aligned}
\& l=a r^{n-1} \\
\& l=\frac{1}{r}[a+(r-1) S] \\
\& l(S-l)^{n-1}=a(S-a)^{n-1} \\
\& l=\frac{S(r-1) r^{n-1}}{r^{n}-1}
\end{aligned}
\] \\
\hline \(n\) \&  \& \(l\)
\(r\)
\(l\) \& \(S\)
\(S\)
\(S\) \& \[
\begin{aligned}
\& n=\frac{\log l-\log a}{\log r}+1 \\
\& n=\frac{\log [a+(r-1) S]-\log a}{\log r} \\
\& n=\frac{\log l-\log a}{\log (S-a)-\log (S-l)}+1 \\
\& n=\frac{\log l-\log [l r-(r-1) S]}{\log r}+1
\end{aligned}
\] \\
\hline \(r\) \& \begin{tabular}{l}
\(a\) \\
\(a\) \\
\(a\)
\end{tabular} \& \begin{tabular}{l}
\(n\) \\
\(l\) \\
\(n\)
\end{tabular} \& \(n\)
\(S\)
\(S\)
\(S\) \& \[
\begin{aligned}
r \& =\sqrt[n-1]{\sqrt{\frac{l}{a}}} \\
r^{n} \& =\frac{S r}{a}+\frac{a-S}{a} \\
r \& =\frac{S-a}{S-l} \\
r^{n} \& =\frac{S r^{n-1}}{S-l}-\frac{l}{S-l}
\end{aligned}
\] \\
\hline \(S\) \& \(a\)
\(a\)
\(a\) \& \(n\)
\(l\)
\(l\)
\(l\)
\(n\) \& \(r\)
\(r\)

$n$ \& $$
\begin{aligned}
& S=\frac{a\left(r^{n}-1\right)}{r-1} \\
& S=\frac{l r-a}{r-1} \\
& S=\frac{\sqrt[n-1]{l^{n}}-\sqrt[n-1]{a^{n}}}{n-\sqrt[1]{l-\sqrt[1]{n}} \sqrt{a}} \\
& S=\frac{l\left(r^{n}-1\right)}{(r-1) r^{n-1}}
\end{aligned}
$$ <br>

\hline
\end{tabular}

## Geometrical Propositions

The sum of the three angles in a triangle always equals 180
degrees. Hence, if two angles are known, the third angle can always
be found.

Geometrical Propositions
If line $A B$ divides angle $C A D$ into two equal parts, it also divides
line $C D$ into two equal parts and is at right angles to it.
angles into two equal parts also bisects the side opposite the angle
and is at right angles to it.
If two sides in a triangle are equal-that is, if the triangle is an
isosceles triangle - then the angles opposite these sides also are
equal.

Geometrical Propositions
If one side of a triangle is produced, then the exterior angle is
equal to the sum of the two interior opposite angles.
Angle $D=$ angle $A+$ angle $B$

Geometrical Propositions
If a line is tangent to a circle, then it is also at right angles to a
line drawn from the center of the circle to the point of tangency-
that is, to a radial line through the point of tangency.

Geometrical Propositions
If two chords intersect each other in a circle, then the rectangle of
Ihe segments of the one equals the rectangle of the segments of the
other.

Geometrical Constructions
To divide a line $A B$ into two equal parts:
With the ends $A$ and $B$ as centers and a radius greater than one-
half the line, draw circular arcs. Through the intersections $C$ and $D$,
draw line $C D$. This line divides $A B$ into two equal parts and is also
perpendicular to $A B$.

Geometrical Constructions
To draw a straight line parallel to a given line $A B$, at a given dis-
Tance from it:
With any points $C$ and $D$ on $A B$ as centers, draw circular arcs
with the given distance as radius. Line $E F$, drawn to touch the cir-
cular arcs, is the required parallel line.

Geometrical Constructions
To draw a circular arc with a given radius through two given
points $A$ and $B$ :
With $A$ and $B$ as centers, and the given radius as radius, draw cir-
cular arcs intersecting at $C$. With $C$ as a center, and the same radius,
draw a circular arc through $A$ and $B$.

Geometrical Constructions
To describe a circle about a square and to inscribe a circle in a
square:
The centers of both the circumscribed and inscribed circles are
located at the point $E$, where the two diagonals of the square inter-
sect. The radius of the circumscribed circle is $A E$, and of the
inscribed circle, $E F$.

Geometrical Constructions
In
Divide line $A B$ into a number of equal parts and divide $B C$ into
the same number of parts. From the division points on $A B$, draw
horizontal lines. From the division points on $B C$, draw lines to
point $A$. The points of intersection between lines drawn from points
numbered alike are points on the parabola.

## Areas and Volumes

The Prismoidal Formula.-The prismoidal formula is a general formula by which the volume of any prism, pyramid or frustum of a pyramid may be found.

$$
\begin{aligned}
A_{1} & =\text { area at one end of the body } \\
A_{2} & =\text { area at the other end } \\
A_{m} & =\text { area of middle section between the two end surfaces } \\
h & =\text { height of body }
\end{aligned}
$$

Then, volume $V$ of the body is $V=\frac{h}{6}\left(A_{1}+4 A_{m}+A_{2}\right)$
Pappus or Guldinus Rules.-By means of these rules the area of any surface of revolution and the volume of any solid of revolution may be found. The area of the surface swept out by the revolution of a line $A B C$ (see illustration) about the axis $D E$ equals the length of the line multiplied by the length of the path of its center of gravity, $P$. If the line is of such a shape that it is difficult to determine its center of gravity, then the line may be divided into a number of short sections, each of which may be considered as a straight line, and the areas swept out by these different sections, as computed by the rule given, may be added to find the total area. The line must lie wholly on one side of the axis of revolution and must be in the same plane.


The volume of a solid body formed by the revolution of a surface $F G H J$ about axis $K L$ equals the area of the surface multiplied by the length of the path of its center of gravity. The surface must lie wholly on one side of the axis of revolution and in the same plane.


Example: By means of these rules, the area and volume of a cylindrical ring or torus may be found. The torus is formed by a circle $A B$ being rotated about axis $C D$. The center of gravity of the circle is at its center. Hence, with the dimensions given in the illustration, the length of the path of the center of gravity of the circle is $3.1416 \times 10=31.416$ inches. Multiplying by the length of the circumference of the circle, which is $3.1416 \times 3=9.4248$ inches, gives $31.416 \times 9.4248=296.089$ square inches which is the area of the torus.

The volume equals the area of the circle, which is $0.7854 \times 9=7.0686$ square inches, multiplied by the path of the center of gravity, which is 31.416 , as before; hence,

Volume $=7.0686 \times 31.416=222.067$ cubic inches

Approximate Method for Finding the Area of a Surface of Revolution.-The accompanying illustration is shown in order to give an example of the approximate method based on Guldinus' rule, that can be used for finding the area of a symmetrical body. In the illustration, the dimensions in common fractions are the known dimensions; those in decimals are found by actual measurements on a figure drawn to scale.
The method for finding the area is as follows: First, separate such areas as are cylindrical, conical, or spherical, as these can be found by exact formulas. In the illustration $A B C D$ is a cylinder, the area of the surface of which can be easily found. The top area $E F$ is simply a circular area, and can thus be computed separately. The remainder of the surface generated by rotating line $A F$ about the axis $G H$ is found by the approximate method explained in the previous section. From point $A$, set off equal distances on line $A F$. In the illustration, each division indicated is $1 / 8$
 inch long. From the central or middle point of each of these parts draw a line at right angles to the axis of rotation $G H$, measure the length of these lines or diameters (the length of each is given in decimals), add all these lengths together and multiply the sum by the length of one division set off on line $A F$ (in this case, $1 / 8 \mathrm{inch}$ ), and multiply this product by $\pi$ to find the approximate area of the surface of revolution.
In setting off divisions $1 / 8$ inch long along line $A F$, the last division does not reach exactly to point $F$, but only to a point 0.03 inch below it. The part 0.03 inch high at the top of the cup can be considered as a cylinder of $1 / 2$ inch diameter and 0.03 inch height, the area of the cylindrical surface of which is easily computed. By adding the various surfaces together, the total surface of the cup is found as follows:
Cylinder, $15 / 8$ inch diameter, 0.41 inch high
2.093 square inches

Circle, $1 / 2$ inch diameter
0.196 square inch

Cylinder, $1 / 2$ inch diameter, 0.03 inch high
Irregular surface
0.047 square inch

Total
3.868 square inches

Area of Plane Surfaces of Irregular Outline.-One of the most useful and accurate methods for determining the approximate area of a plane figure or irregular outline is known as Simpson's Rule. In applying Simpson's Rule to find an area the work is done in four steps:

1) Divide the area into an even number, $N$, of parallel strips of equal width $W$; for example, in the accompanying diagram, the area has been divided into 8 strips of equal width.
2) Label the sides of the strips $V_{0}, V_{1}, V_{2}$, etc., up to $V_{N}$.
3) Measure the heights $V_{0}, V_{1}, V_{2}, \ldots, V_{N}$ of the sides of the strips.
4) Substitute the heights $V_{0}, V_{1}$, etc., in the following formula to find the area $A$ of the figure:

$$
A=\frac{W}{3}\left[\left(V_{0}+V_{N}\right)+4\left(V_{1}+V_{3}+\cdots+V_{N-1}\right)+2\left(V_{2}+V_{4}+\cdots+V_{N}\right.\right.
$$

Example: The area of the accompanying figure was divided into 8 strips on a full-size drawing and the following data obtained. Calculate the area using Simpson's Rule.

$$
\begin{aligned}
& W=1 /{ }^{\prime \prime} \\
& V_{0}=0^{\prime \prime} \\
& V_{1}=3 / 4 \\
& V_{2}=1 / 4 / 4 \\
& V_{3}=1 / \frac{1}{2} \\
& V_{4}=15 /{ }^{\prime \prime} \\
& V_{5}=2 \frac{1}{4} /{ }^{\prime \prime} \\
& V_{6}=21 /{ }^{\prime \prime} \\
& V_{7}=1 \frac{3}{4} /{ }^{\prime \prime} \\
& V_{8}=1 / 2
\end{aligned}
$$



Substituting the given data in the Simpson formula,

$$
\begin{aligned}
A & =\frac{1 / 2}{3}[(0+1 / 2)+4(3 / 4+11 / 2+21 / 4+13 / 4)+2(11 / 4+15 / 8+21 / 2)] \\
& =1 / 6[(1 / 2)+4(61 / 4)+2(53 / 8)]=1 / 6[361 / 4] \\
& =6.04 \text { square inches }
\end{aligned}
$$

In applying Simpson's Rule, it should be noted that the larger the number of strips into which the area is divided the more accurate the results obtained.
Areas Enclosed by Cycloidal Curves.-The area between a cycloid and the straight line upon which the generating circle rolls, equals three times the area of the generating circle (see diagram, page 63). The areas between epicycloidal and hypocycloidal curves and the "fixed circle" upon which the generating circle is rolled, may be determined by the following formulas, in which $a=$ radius of the fixed circle upon which the generating circle rolls; $b=$ radius of the generating circle; $A=$ the area for the epicycloidal curve; and $A_{1}=$ the area for the hypocycloidal curve.

$$
A=\frac{3.1416 b^{2}(3 a+2 b)}{a} \quad A_{1}=\frac{3.1416 b^{2}(3 a-2 b)}{a}
$$

Find the Contents of Cylindrical Tanks at Different Levels.-In conjunction with the table Segments of Circles for Radius $=1$ presented on pages 80 and 81, the following relations can give a close approximation of the liquid contents, at any level, in a cylindrical tank.


A long measuring rule calibrated in length units or simply a plain stick can be used for measuring contents at a particular level. In turn, the rule or stick can be graduated to serve as a volume gauge for the tank in question. The only requirements are that the cross-section of the tank is circular; the tank's dimensions are known; the gauge rod is inserted vertically
through the top center of the tank so that it rests on the exact bottom of the tank; and that consistent English or metric units are used throughout the calculations.
$K=C r^{2} L=$ Tank Constant (remains the same for any given tank)
$V_{T}=\pi K$, for a tank that is completely full
$V_{s}=K A$
$V=V_{\mathrm{s}}$ when tank is less than half full
$V=V_{T}-V_{s}=V_{T}-K A$, when tank is more than half full
where $C=$ liquid volume conversion factor, the exact value of which depends on the length and liquid volume units being used during measurement: 0.00433 U.S. gal/in ${ }^{3} ; 7.48$ U.S. gal/ft ${ }^{3} ; 0.00360$ U.K. gal/in ${ }^{3} ; ~ 6.23$ U.K. gal/ft ${ }^{3} ; ~ 0.001$ liter/ $\mathrm{cm}^{3}$; or 1000 liters $/ \mathrm{m}^{3}$
$V_{T}=$ total volume of liquid tank can hold
$V_{s}=$ volume formed by segment of circle having depth $=x$ in given tank (see diagram)
$V=$ volume of liquid at particular level in tank
$d=$ diameter of tank; $L=$ length of tank; $r=$ radius of $\operatorname{tank}(=1 / 2$ diameter $)$
$A=$ segment area of a corresponding unit circle taken from pages 80 or 81
$y=$ actual depth of contents in tank as shown on a gauge rod or stick
$x=$ depth of the segment of a circle to be considered in given tank. As can be seen in above diagram, $x$ is the actual depth of contents $(y)$ when the tank is less than half full, and is the depth of the void $(d-y)$ above the contents when the tank is more than half full. From pages 80 and 81 it can also be seen that $h$, the height of a segment of a corresponding unit circle, is $x / r$
Example: A tank is 20 feet long and 6 feet in diameter. Convert a long inch-stick into a gauge that is graduated at 1000 and 3000 U.S. gallons.

$$
L=20 \times 12=240 \mathrm{in} . \quad r=\frac{6}{2} \times 12=36 \mathrm{in} .
$$

From Formula (1): $K=0.00433(36)^{2}(240)=1347$
From Formula (2): $V_{T}=3.142 \times 1347=4232$ US gal.
The 72-inch mark from the bottom on the inch-stick can be graduated for the rounded full volume " 4230 "; and the halfway point 36 " for $4230 / 2$ or " 2115 ." It can be seen that the 1000 -gal mark would be below the halfway mark. From Formulas (3) and (4):
$A_{1000}=\frac{1000}{1347}=0.7424$ from page $81, h$ can be interpolated as 0.5724 ; and $x=y=36 \times 0.5724=20.61$. If the desired level of accuracy permits, interpolation can be omitted by choosing $h$ directly from the table on page 81 for the value of $A$ nearest that calculated above.
Therefore, the 1000 -gal mark is graduated $205 / 8$ from bottom of rod.
It can be seen that the 3000 mark would be above the halfway mark. Therefore, the circular segment considered is the cross-section of the void space at the top of the tank. From Formulas (3) and (5):

$$
A_{3000}=\frac{4230-3000}{1347}=0.9131 ; h=0.6648 ; x=36 \times 0.6648=23.93^{\prime \prime}
$$

Therefore, the 3000 -gal mark is $72.00-23.93=48.07$, or at the $481 / 16$ mark from the bottom.

## Areas and Dimensions of Plane Figures

In the following tables are given formulas for the areas of plane figures, together with other formulas relating to their dimensions and properties; the surfaces of solids; and the volumes of solids. The notation used in the formulas is, as far as possible, given in the illustration accompanying them; where this has not been possible, it is given at the beginning of each set of formulas.

Examples are given with each entry, some in English and some in metric units, showing the use of the preceding formula.

## Square:



$$
\begin{aligned}
\text { Area }=A & =s^{2}=1 / 2 d^{2} \\
s & =0.7071 d=\sqrt{A} \\
d & =1.414 s=1.414 \sqrt{A}
\end{aligned}
$$

Example: Assume that the side $s$ of a square is 15 inches. Find the area and the length of the diagonal.

$$
\begin{aligned}
\text { Area } & =A=s^{2}=15^{2}=225 \text { square inches } \\
\text { Diagonal } & =d=1.414 s=1.414 \times 15=21.21 \text { inches }
\end{aligned}
$$

Example: The area of a square is 625 square inches. Find the length of the side $s$ and the diagonal $d$.

$$
\begin{aligned}
& s=\sqrt{A}=\sqrt{625}=25 \text { inches } \\
& d=1.414 \sqrt{A}=1.414 \times 25=35.35 \text { inches }
\end{aligned}
$$

Rectangle:


$$
\begin{aligned}
\text { Area }=A & =a b=a \sqrt{d^{2}-a^{2}}=b \sqrt{d^{2}-b^{2}} \\
d & =\sqrt{a^{2}+b^{2}} \\
a & =\sqrt{d^{2}-b^{2}}=A \div b \\
a & =\sqrt{d^{2}-a^{2}}=A \div a
\end{aligned}
$$

Example: The side $a$ of a rectangle is 12 centimeters, and the area 70.5 square centimeters. Find the length of the side $b$, and the diagonal $d$.

$$
\begin{aligned}
& b=A \div a=70.5 \div 12=5.875 \text { centimeters } \\
& d=\sqrt{a^{2}+b^{2}}=\sqrt{12^{2}+5.875^{2}}=\sqrt{178.516}=13.361 \text { centimeters }
\end{aligned}
$$

Example: The sides of a rectangle are 30.5 and 11 centimeters long. Find the area.

$$
\text { Area }=A=a \times b=30.5 \times 11=335.5 \text { square centimeters }
$$

## Parallelogram:



$$
\begin{aligned}
\text { Area }=A & =a b \\
a & =A \div b \\
b & =A \div a
\end{aligned}
$$

Note: The dimension $a$ is measured at right angles to line $b$.
Example: The base $b$ of a parallelogram is 16 feet. The height $a$ is 5.5 feet. Find the area.

$$
\text { Area }=A=a \times b=5.5 \times 16=88 \text { square feet }
$$

Example: The area of a parallelogram is 12 square inches. The height is 1.5 inches. Find the length of the base b .

$$
b=A \div a=12 \div 1.5=8 \text { inches }
$$

Right-Angled Triangle:


$$
\text { Area } \begin{aligned}
A & =\frac{b c}{2} \\
a & =\sqrt{b^{2}+c^{2}} \\
b & =\sqrt{a^{2}-c^{2}} \\
c & =\sqrt{a^{2}-b^{2}}
\end{aligned}
$$

Example: The sides $b$ and $c$ in a right-angled triangle are 6 and 8 inches. Find side $a$ and the area

$$
\begin{aligned}
& a=\sqrt{b^{2}+c^{2}}=\sqrt{6^{2}+8^{2}}=\sqrt{36+64}=\sqrt{100}=10 \text { inches } \\
& A=\frac{b \times c}{2}=\frac{6 \times 8}{2}=\frac{48}{2}=24 \text { square inches }
\end{aligned}
$$

Example: If $a=10$ and $b=6$ had been known, but not $c$, the latter would have been found as follows:

$$
c=\sqrt{a^{2}-b^{2}}=\sqrt{10^{2}-6^{2}}=\sqrt{100-36}=\sqrt{64}=8 \text { inches }
$$

## Acute-Angled Triangle:



$$
\begin{aligned}
\text { Area }=A & =\frac{b h}{2}=\frac{b}{2} \sqrt{a^{2}-\left(\frac{a^{2}+b^{2}-c^{2}}{2 b}\right)^{2}} \\
\text { If } S & =1 / 2(a+b+c), \text { then } \\
A & =\sqrt{S(S-a)(S-b)(S-c)}
\end{aligned}
$$

Example: If $a=10, b=9$, and $c=8$ centimeters, what is the area of the triangle?

$$
\begin{aligned}
A & =\frac{b}{2} \sqrt{a^{2}-\left(\frac{a^{2}+b^{2}-c^{2}}{2 b}\right)^{2}}=\frac{9}{2} \sqrt{10^{2}-\left(\frac{10^{2}+9^{2}-8^{2}}{2 \times 9}\right)^{2}}=4.5 \sqrt{100-\left(\frac{117}{18}\right)^{2}} \\
& =4.5 \sqrt{100-42.25}=4.5 \sqrt{57.75}=4.5 \times 7.60=34.20 \text { square centimeters }
\end{aligned}
$$

## Obtuse-Angled Triangle:



$$
\begin{aligned}
\text { Area }=A & =\frac{b h}{2}=\frac{b}{2} \sqrt{a^{2}-\left(\frac{c^{2}-a^{2}-b^{2}}{2 b}\right)^{2}} \\
\text { If } \mathrm{S} & =1 / 2(a+b+c), \text { then } \\
A & =\sqrt{S(S-a)(S-b)(S-c)}
\end{aligned}
$$

Example: The side $a=5$, side $b=4$, and side $c=8$ inches. Find the area.

$$
\begin{aligned}
S & =\frac{1}{2}(a+b+c)=1 / 2(5+4+8)=1 / 2 \times 17=8.5 \\
A & =\sqrt{S(S-a)(S-b)(S-c)}=\sqrt{8.5(8.5-5)(8.5-4)(8.5-8)} \\
& =\sqrt{8.5 \times 3.5 \times 4.5 \times 0.5}=\sqrt{66.937}=8.18 \text { square inches }
\end{aligned}
$$

## Trapezoid:



$$
\text { Area }=A=\frac{(a+b) h}{2}
$$

Note: In Britain, this figure is called a trapezium and the one below it is known as a trapezoid, the terms being reversed.
Example: Side $a=23$ meters, side $b=32$ meters, and height $h=$ 12 meters. Find the area.

$$
A=\frac{(a+b) h}{2}=\frac{(23+32) 12}{2}=\frac{55 \times 12}{2}=330 \text { square meters }
$$

Trapezium:
Area $=A=\frac{(H+h) a+b h+c H}{2}$


A trapezium can also be divided into two triangles as indicated by the dashed line. The area of each of these triangles is computed, and the results added to find the area of the trapezium.
Example: Let $a=10, b=2, c=3, h=8$, and $H=12$ inches. Find the area.

$$
\begin{aligned}
A & =\frac{(H+h) a+b h+c H}{2}=\frac{(12+8) 10+2 \times 8+3 \times 12}{2} \\
& =\frac{20 \times 10+16+36}{2}=\frac{252}{2}=126 \text { square inches }
\end{aligned}
$$

## Regular Hexagon:


$A=2.598 s^{2}=2.598 R^{2}=3.464 r^{2}$
$R=s=$ radius of circumscribed circle $=1.155 r$
$r=$ radius of inscribed circle $=0.866 s=0.866 R$
$s=R=1.155 r$
Example: The side $s$ of a regular hexagon is 40 millimeters. Find the area and the radius $r$ of the inscribed circle.

$$
\begin{aligned}
A & =2.598 s^{2}=2.598 \times 40^{2}=2.598 \times 1600=4156.8 \text { square millimeters } \\
r & =0.866 s=0.866 \times 40=34.64 \text { millimeters }
\end{aligned}
$$

Example: What is the length of the side of a hexagon that is drawn around a circle of 50 millimeters radius?-Here $r=50$. Hence, $s=1.155 r=1.155 \times 50=57.75$ millimeters

## Regular Octagon:

| $A$ | $=$ area $=4.828 s^{2}=2.828 R^{2}=3.314 r^{2}$ |
| ---: | :--- |
| $R$ | $=$ radius of circumscribed circle $=1.307 s=1.082 r$ |
| $r$ | $=$ radius of inscribed circle $=1.207 s=0.924 R$ |
| $s$ | $=0.765 R=0.828 r$ |
| Example: Find the area and the length of the side of an octagon |  |
| that is inscribed in a circle of 12 inches diameter. |  |
| Diameter of circumscribed circle $=12$ inches; hence, $R=6$ |  |
| inches. |  |
| $A$ | $=2.828 R^{2}=2.828 \times 6^{2}=2.828 \times 36=101.81$ squre inches |
| $s$ | $=0.765 R=0.765 \times 6=4.590$ inches |

## Regular Polygon:



$$
\begin{array}{ll}
A=\text { area } & n=\text { number of sides } \\
\alpha=360^{\circ} \div n & \beta=180^{\circ}-\alpha \\
A=\frac{n s r}{2}=\frac{n s}{2} \sqrt{R^{2}-\frac{s^{2}}{4}} \\
R=\sqrt{r^{2}+\frac{s^{2}}{4}} \quad r=\sqrt{R^{2}-\frac{s^{2}}{4}} \quad s=2 \sqrt{R^{2}-r^{2}}
\end{array}
$$

Example: Find the area of a polygon having 12 sides, inscribed in a circle of 8 centimeters radius. The length of the side $s$ is 4.141 centimeters.

$$
\begin{aligned}
A & =\frac{n s}{2} \sqrt{R^{2}-\frac{s^{2}}{4}}=\frac{12 \times 4.141}{2} \sqrt{8^{2}-\frac{4.141^{2}}{4}}=24.846 \sqrt{59.713} \\
& =24.846 \times 7.727=191.98 \text { square centimeters }
\end{aligned}
$$

Circle:
$\begin{aligned} \text { Area } & =A=\pi r^{2}=3.1416 r^{2}=0.7854 d^{2} \\ \text { Circumference } & =C=2 \pi r=6.832 r=3.1416 d\end{aligned}$
$r=C \div 6.2832=\sqrt{A \div 3.1416}=0.564 \sqrt{A}$
$d=C \div 3.1416=\sqrt{A \div 0.7854}=1.128 \sqrt{A}$
Length of arc for center angle of $1^{\circ}=0.008727 d$
Length of arc for center angle of $n^{\circ}=0.008727 n d$
Example: Find the area $A$ and circumference $C$ of a circle with a diameter of $23 / 4$ inches.

$$
\begin{aligned}
& A=0.7854 d^{2}=0.7854 \times 2.75^{2}=0.7854 \times 2.75 \times 2.75=5.9396 \text { square inches } \\
& C=3.1416 d=3.1416 \times 2.75=8.6394 \text { inches }
\end{aligned}
$$

Example: The area of a circle is 16.8 square inches. Find its diameter.

$$
d=1.128 \sqrt{A}=1.128 \sqrt{16.8}=1.128 \times 4.099=4.624 \text { inches }
$$

## Circular Sector:



$$
\begin{aligned}
\text { Length of arc } & =l=\frac{r \times \alpha \times 3.1416}{180}=0.01745 r \alpha=\frac{2 A}{r} \\
\text { Area } & =A=1 / 2 r l=0.008727 \alpha r^{2} \\
\text { Angle, in degrees } & =\alpha=\frac{57.296 l}{r} \quad r=\frac{2 A}{l}=\frac{57.296 l}{\alpha}
\end{aligned}
$$

Example: The radius of a circle is 35 millimeters, and angle $\alpha$ of a sector of the circle is 60 degrees. Find the area of the sector and the length of arc $l$.

$$
\begin{aligned}
A & =0.008727 \alpha r^{2}=0.008727 \times 60 \times 35^{2}=641.41 \mathrm{~mm}^{2}=6.41 \mathrm{~cm}^{2} \\
l & =0.01745 r \alpha=0.01745 \times 35 \times 60=36.645 \text { millimeters }
\end{aligned}
$$

Circular Segment:


$$
\begin{aligned}
& A=\text { area } \quad l=\text { length of arc } \quad \alpha=\text { angle, in degrees } \\
& c=2 \sqrt{h(2 r-h)} \quad A=1 / 2[r l-c(r-h)] \\
& r=\frac{c^{2}+4 h^{2}}{8 h} \quad l=0.01745 r \alpha \\
& h=r-1 / 2 \sqrt{4 r^{2}-c^{2}}=r[1-\cos (\alpha / 2)] \quad \alpha=\frac{57.296 l}{r}
\end{aligned}
$$

Example: The radius $r$ is 60 inches and the height $h$ is 8 inches. Find the length of the chord $c$.

$$
c=2 \sqrt{h(2 r-h)}=2 \sqrt{8 \times(2 \times 60-8)}=2 \sqrt{896}=2 \times 29.93=59.86 \text { inches }
$$

Example: If $c=16$, and $h=6$ inches, what is the radius of the circle of which the segment is a part?

$$
r=\frac{c^{2}+4 h^{2}}{8 h}=\frac{16^{2}+4 \times 6^{2}}{8 \times 6}=\frac{256+144}{48}=\frac{400}{48}=81 / 3 \text { inches }
$$

## Cycloid:

Area $=A=3 \pi r^{2}=9.4248 r^{2}=2.3562 d^{2}$
$=3 \times$ area of generating circle

Circular Ring:


$$
\begin{aligned}
\text { Area }=A & =\pi\left(R^{2}-r^{2}\right)=3.1416\left(R^{2}-r^{2}\right) \\
& =3.1416(R+r)(R-r) \\
& =0.7845\left(D^{2}-d^{2}\right)=0.7854(D+d)(D-d)
\end{aligned}
$$

Example: Let the outside diameter $D=12$ centimeters and the inside diameter $d=8$ centimeters. Find the area of the ring.

$$
\begin{aligned}
A & =0.7854\left(D^{2}-d^{2}\right)=0.7854\left(12^{2}-8^{2}\right)=0.7854(144-64)=0.7854 \times 80 \\
& =62.83 \text { square centimeters }
\end{aligned}
$$

By the alternative formula:

$$
\begin{aligned}
A & =0.7854(D+d)(D-d)=0.7854(12+8)(12-8)=0.7854 \times 20 \times 4 \\
& =62.83 \text { square centimeters }
\end{aligned}
$$

Circular Ring Sector:


$$
\begin{aligned}
A & =\text { area } \quad \alpha=\text { angle, in degrees } \\
A & =\frac{\alpha \pi}{360}\left(R^{2}-r^{2}\right)=0.00873 \alpha\left(R^{2}-r^{2}\right) \\
& =\frac{\alpha \pi}{4 \times 360}\left(D^{2}-d^{2}\right)=0.00218 \alpha\left(D^{2}-d^{2}\right)
\end{aligned}
$$

Example: Find the area, if the outside radius $R=5$ inches, the inside radius $r=2$ inches, and $\alpha=72$ degrees.

$$
\begin{aligned}
A & =0.00873 \alpha\left(R^{2}-r^{2}\right)=0.00873 \times 72\left(5^{2}-2^{2}\right) \\
& =0.6286(25-4)=0.6286 \times 21=13.2 \text { square inches }
\end{aligned}
$$

## Spandrel or Fillet:



$$
\text { Area }=A=r^{2}-\frac{\pi r^{2}}{4}=0.215 r^{2}=0.1075 c^{2}
$$

Example: Find the area of a spandrel, the radius of which is 0.7 inch.

$$
A=0.215 r^{2}=0.215 \times 0.7^{2}=0.105 \text { square inch }
$$

Example: If chord $c$ were given as 2.2 inches, what would be the area?

$$
A=0.1075 c^{2}=0.1075 \times 2.2^{2}=0.520 \text { square inch }
$$

## Parabola:



$$
\text { Area }=A=2 / 3 x y
$$

(The area is equal to two-thirds of a rectangle which has $x$ for its base and $y$ for its height.)
Example: Let $x$ in the illustration be 15 centimeters, and $y, 9$ centimeters. Find the area of the shaded portion of the parabola. $A=2 / 3 \times x y=2 / 3 \times 15 \times 9=10 \times 9=90$ square centimeters

Parabola:


$$
l=\text { length of arc }=\frac{p}{2}\left[\sqrt{\frac{2 x}{p}\left(1+\frac{2 x}{p}\right)}+\ln \left(\sqrt{\frac{2 x}{p}}+\sqrt{1+\frac{2 x}{p}}\right)\right]
$$

When $x$ is small in proportion to $y$, the following is a close approximation:

$$
l=y\left[1+\frac{2}{3}\left(\frac{x}{y}\right)^{2}-\frac{2}{5}\left(\frac{x}{y}\right)^{4}\right] \text { or } l=\sqrt{y^{2}+\frac{4}{3} x^{2}}
$$

Example: If $x=2$ and $y=24$ feet, what is the approximate length $l$ of the parabolic curve?

$$
\begin{aligned}
l & =y\left[1+\frac{2}{3}\left(\frac{x}{y}\right)^{2}-\frac{2}{5}\left(\frac{x}{y}\right)^{4}\right]=24\left[1+\frac{2}{3}\left(\frac{2}{24}\right)^{2}-\frac{2}{5}\left(\frac{2}{24}\right)^{4}\right] \\
& =24\left[1+\frac{2}{3} \times \frac{1}{144}-\frac{2}{5} \times \frac{1}{20,736}\right]=24 \times 1.0046=24.11 \text { feet }
\end{aligned}
$$

Segment of Parabola:


Area $\mathrm{BFC}=A=2 / 3$ area of parallelogram BCDE
If FG is the height of the segment, measured at right angles to BC , then:

$$
\text { Area of segment } \mathrm{BFC}=2 / 3 \mathrm{BC} \times \mathrm{FG}
$$

Example: The length of the chord $B C=19.5$ inches. The distance between lines $B C$ and $D E$, measured at right angles to $B C$, is 2.25 inches. This is the height of the segment. Find the area.

Area $=A=2 / 3 \mathrm{BC} \times \mathrm{FG}=2 / 3 \times 19.5 \times 2.25=29.25$ square inches

## Hyperbola:



$$
\text { Area } \mathrm{BCD}=A=\frac{x y}{2}-\frac{a b}{2} \ln \left(\frac{x}{a}+\frac{y}{b}\right)
$$

Example: The half-axes $a$ and $b$ are 3 and 2 inches, respectively. Find the area shown shaded in the illustration for $x=8$ and $y=5$.

Inserting the known values in the formula:

$$
\begin{aligned}
A & =\frac{8 \times 5}{2}-\frac{3 \times 2}{2} \times \ln \left(\frac{8}{3}+\frac{5}{2}\right)=20-3 \times \ln 5.167 \\
& =20-3 \times 1.6423=20-4.927=15.073 \text { square inches }
\end{aligned}
$$

## Ellipse:



$$
\text { Area }=A=\pi a b=3.1416 a b
$$

An approximate formula for the perimeter is

$$
\begin{gathered}
\text { Perimeter }=P=3.1416 \sqrt{2\left(a^{2}+b^{2}\right)} \\
\text { A closer approximation is } P=3.1416 \sqrt{2\left(a^{2}+b^{2}\right)-\frac{(a-b)^{2}}{2.2}}
\end{gathered}
$$

Example: The larger or major axis is 200 millimeters. The smaller or minor axis is 150 millimeters.
Find the area and the approximate circumference. Here, then, $a=100$, and $b=75$.

$$
A=3.1416 a b=3.1416 \times 100 \times 75=23,562 \text { square millimeters }=235.62 \text { square centimeters }
$$

$$
\begin{aligned}
P & =3.1416 \sqrt{2\left(a^{2}+b^{2}\right)}=3.1416 \sqrt{2\left(100^{2}+75^{2}\right)}=3.1416 \sqrt{2 \times 15,625} \\
& =3.1416 \sqrt{31,250}=3.1416 \times 176.78=555.37 \text { millimeters }=(55.537 \text { centimeters })
\end{aligned}
$$

## Volumes of Solids

Cube:


Example: The side of a cube equals 9.5 centimeters. Find its volume.

$$
\text { Volume }=V=s^{3}=9.5^{3}=9.5 \times 9.5 \times 9.5=857.375 \text { cubic centimeters }
$$

Example: The volume of a cube is 231 cubic centimeters. What is the length of the side?

$$
s=\sqrt[3]{V}=\sqrt[3]{231}=6.136 \text { centimeters }
$$

## Square Prism:



$$
\begin{gathered}
\text { Volume }=V=a b c \\
a=\frac{V}{b c} \quad b=\frac{V}{a c} \quad c=\frac{V}{a b}
\end{gathered}
$$

Example: In a square prism, $a=6, b=5, c=4$. Find the volume.

$$
V=a \times b \times c=6 \times 5 \times 4=120 \text { cubic inches }
$$

Example: How high should a box be made to contain 25 cubic feet, if it is 4 feet long and $21 / 2$ feet wide? Here, $a=4, c=2.5$, and $V=25$. Then,

$$
b=\text { depth }=\frac{V}{a c}=\frac{25}{4 \times 2.5}=\frac{25}{10}=2.5 \text { feet }
$$

## Prism:



$$
\begin{aligned}
& V=\text { volume } \\
& A=\text { area of end surface } \\
& V=h \times A
\end{aligned}
$$

The area $A$ of the end surface is found by the formulas for areas of plane figures on the preceding pages. Height $h$ must be measured perpendicular to the end surface.
Example: A prism, having for its base a regular hexagon with a side $s$ of 7.5 centimeters, is 25 centimeters high. Find the volume.

> Area of hexagon $=A=2.598 s^{2}=2.598 \times 56.25=146.14$ square centimeters
> Volume of prism $=h \times A=25 \times 146.14=3653.5$ cubic centimeters

## Pyramid:



Volume $=V=\frac{1}{3} h \times$ area of base
If the base is a regular polygon with $n$ sides, and $s=$ length of side, $r=$ radius of inscribed circle, and $R=$ radius of circumscribed circle, then:

$$
V=\frac{n s r h}{6}=\frac{n s h}{6} \sqrt{R^{2}-\frac{s^{2}}{4}}
$$

Example: A pyramid, having a height of 9 feet, has a base formed by a rectangle, the sides of which are 2 and 3 feet, respectively. Find the volume.

Area of base $=2 \times 3=6$ square feet; $h=9$ feet
Volume $=V=1 / 3 h \times$ area of base $=1 / 3 \times 9 \times 6=18$ cubic feet

Frustum of Pyramid:


$$
\text { Volume }=V=\frac{h}{3}\left(A_{1}+A_{2}+\sqrt{A_{1} \times A_{2}}\right)
$$

Example: The pyramid in the previous example is cut off $41 / 2$ feet from the base, the upper part being removed. The sides of the rectangle forming the top surface of the frustum are, then, 1 and $1 \frac{1}{2}$ feet long, respectively. Find the volume of the frustum.

Area of top $=A_{1}=1 \times 1 \frac{1}{2}=11 / 2$ sq. ft. $\quad$ Area of base $=A_{2}=2 \times 3=6 \mathrm{sq} . \mathrm{ft}$.

$$
V=\frac{4 \cdot 5}{3}(1.5+6+\sqrt{1.5 \times 6})=1.5(7.5+\sqrt{9})=1.5 \times 10.5=15.75 \text { cubic feet }
$$

## Wedge:



$$
\text { Volume }=V=\frac{(2 a+c) b h}{6}
$$

Example: Let $a=4$ inches, $b=3$ inches, and $c=5$ inches. The height $h=4.5$ inches. Find the volume.

$$
\begin{aligned}
V & =\frac{(2 a+c) b h}{6}=\frac{(2 \times 4+5) \times 3 \times 4.5}{6}=\frac{(8+5) \times 13.5}{6} \\
& =\frac{175.5}{6}=29.25 \text { cubic inches }
\end{aligned}
$$

## Cylinder:



Volume $=V=3.1416 r^{2} h=0.7854 d^{2} h$
Area of cylindrical surface $=S=6.2832 r h=3.1416 d h$
Total area $A$ of cylindrical surface and end surfaces:

$$
A=6.2832 r(r+h)=3.1416 d(1 / 2 d+h)
$$

Example: The diameter of a cylinder is 2.5 inches. The length or height is 20 inches. Find the volume and the area of the cylindrical surface $S$.

$$
\begin{aligned}
& V=0.7854 d^{2} h=0.7854 \times 2.5^{2} \times 20=0.7854 \times 6.25 \times 20=98.17 \text { cubic inches } \\
& S=3.1416 d h=3.1416 \times 2.5 \times 20=157.08 \text { square inches }
\end{aligned}
$$

## Portion of Cylinder:



$$
\begin{aligned}
\text { Volume }=V & =1.5708 r^{2}\left(h_{1}+h_{2}\right) \\
& =0.3927 d^{2}\left(h_{1}+h_{2}\right) \\
\text { Cylindrical surface area }=S & =3.1416 r\left(h_{1}+h_{2}\right) \\
& =1.5708 d\left(h_{1}+h_{2}\right)
\end{aligned}
$$

Example: A cylinder 125 millimeters in diameter is cut off at an angle, as shown in the illustration. Dimension $h_{1}=150$, and $h_{2}=100 \mathrm{~mm}$. Find the volume and the area $S$ of the cylindrical surface.

$$
\begin{aligned}
V & =0.3927 d^{2}\left(h_{1}+h_{2}\right)=0.3927 \times 125^{2} \times(150+100) \\
& =0.3927 \times 15,625 \times 250=1,533,984 \text { cubic millimeters }=1534 \mathrm{~cm}^{3} \\
S & =1.5708 d\left(h_{1}+h_{2}\right)=1.5708 \times 125 \times 250 \\
& =49,087.5 \text { square millimeters }=490.9 \text { square centimeters }
\end{aligned}
$$

Portion of Cylinder:


$$
\text { Volume }=V=\left(2 / 3 a^{3} \pm b \times \text { area } \mathrm{ABC}\right) \frac{h}{r \pm b}
$$

Cylindrical surface area $=S=(a d \pm b \times$ length of $\operatorname{arc} \mathrm{ABC}) \frac{h}{r \pm b}$
Use + when base area is larger, and - when base area is less than one-half the base circle.

Example: Find the volume of a cylinder so cut off that line $A C$ passes through the center of the base circle - that is, the base area is a half-circle. The diameter of the cylinder $=5$ inches, and the height $h=$ 2 inches.

In this case, $a=2.5 ; b=0$; area $A B C=0.5 \times 0.7854 \times 5^{2}=9.82 ; r=2.5$.

$$
V=\left(\frac{2}{3} \times 2.5^{3}+0 \times 9.82\right) \frac{2}{2.5+0}=\frac{2}{3} \times 15.625 \times 0.8=8.33 \text { cubic inches }
$$

Hollow Cylinder:


$$
\begin{aligned}
\text { Volume }=V & =3.1416 h\left(R^{2}-r^{2}\right)=0.7854 h\left(D^{2}-d^{2}\right) \\
& =3.1416 h t(2 R-t)=3.1416 h t(D-t) \\
& =3.1416 h t(2 r+t)=3.1416 h t(d+t) \\
& =3.1416 h t(R+r)=1.5708 h t(D+d)
\end{aligned}
$$

Example: A cylindrical shell, 28 centimeters high, is 36 centimeters in outside diameter, and 4 centimeters thick. Find its volume.

$$
\begin{aligned}
V=3.1416 h t(D-t) & =3.1416 \times 28 \times 4(36-4)=3.1416 \times 28 \times 4 \times 32 \\
& =11,259.5 \text { cubic centimeters }
\end{aligned}
$$

Cone:


$$
\begin{aligned}
\qquad \text { Volume }=V= & \frac{3.1416 r^{2} h}{3}=1.0472 r^{2} h=0.2618 d^{2} h \\
\text { Conical surface area }=A= & 3.1416 r \sqrt{r^{2}+h^{2}}=3.1416 r s \\
& =1.5708 d s \\
s= & \sqrt{r^{2}+h^{2}}=\sqrt{\frac{d^{2}}{4}+h^{2}}
\end{aligned}
$$

Example: Find the volume and area of the conical surface of a cone, the base of which is a circle of 6 inches diameter, and the height of which is 4 inches.

$$
\begin{aligned}
V & =0.2618 d^{2} h=0.2618 \times 6^{2} \times 4=0.2618 \times 36 \times 4=37.7 \text { cubic inches } \\
A & =3.1416 r \sqrt{r^{2}+h^{2}}=3.1416 \times 3 \times \sqrt{3^{2}+4^{2}}=9.4248 \times \sqrt{25} \\
& =47.124 \text { square inches }
\end{aligned}
$$

## Frustum of Cone:



$$
\begin{aligned}
& V=\text { volume } \quad A=\text { area of conical surface } \\
& V=1.0472 h\left(R^{2}+R r+r^{2}\right)=0.2618 h\left(D^{2}+D d+d^{2}\right) \\
& A=3.1416 s(R+r)=1.5708 s(D+d) \\
& a=R-r \quad s=\sqrt{a^{2}+h^{2}}=\sqrt{(R-r)^{2}+h^{2}}
\end{aligned}
$$

Example: Find the volume of a frustum of a cone of the following dimensions: $D=8$ centimeters; $d=4$ centimeters; $h=5$ centimeters.

$$
\begin{aligned}
V & =0.2618 \times 5\left(8^{2}+8 \times 4+4^{2}\right)=0.2618 \times 5(64+32+16) \\
& =0.2618 \times 5 \times 112=146.61 \text { cubic centimeters }
\end{aligned}
$$

Sphere:


$$
\begin{aligned}
\text { Volume } & =V=\frac{4 \pi r^{3}}{3}=\frac{\pi d^{3}}{6}=4.1888 r^{3}=0.5236 d^{3} \\
\text { Surface area } & =A=4 \pi r^{2}=\pi d^{2}=12.5664 r^{2}=3.1416 d^{2}
\end{aligned}
$$

$$
r=\sqrt[3]{\frac{3 V}{4 \pi}}=0.6024 \sqrt[3]{V}
$$

Example: Find the volume and the surface of a sphere 6.5 centimeters diameter.

$$
\begin{aligned}
& V=0.5236 d^{3}=0.5236 \times 6.5^{3}=0.5236 \times 6.5 \times 6.5 \times 6.5=143.79 \mathrm{~cm}^{3} \\
& A=3.1416 d^{2}=3.1416 \times 6.5^{2}=3.1416 \times 6.5 \times 6.5=132.73 \mathrm{~cm}^{2}
\end{aligned}
$$

Example: The volume of a sphere is 64 cubic centimeters. Find its radius.

$$
r=0.6204 \sqrt[3]{64}=0.6204 \times 4=2.4816 \text { centimeters }
$$

## Spherical Sector:



$$
\begin{aligned}
V= & \frac{2 \pi r^{2} h}{3}=2.0944 r^{2} h=\text { Volume } \\
A= & 3.1416 r(2 h+1 / 2 c) \\
& =\text { total area of conical and spherical surface } \\
c= & 2 \sqrt{h(2 r-h)}
\end{aligned}
$$

Example: Find the volume of a sector of a sphere 6 inches in diameter, the height $h$ of the sector being 1.5 inch. Also find the length of chord $c$. Here $r=3$ and $h=1.5$.

$$
\begin{aligned}
& V=2.0944 r^{2} h=2.0944 \times 3^{2} \times 1.5=2.0944 \times 9 \times 1.5=28.27 \text { cubic inches } \\
& c=2 \sqrt{h(2 r-h)}=2 \sqrt{1.5(2 \times 3-1.5)}=2 \sqrt{6.75}=2 \times 2.598=5.196 \text { inches }
\end{aligned}
$$

## Spherical Segment:

$$
\begin{aligned}
& V=\text { volume } \quad A=\text { area of spherical surface } \\
& V=3.1416 h^{2}\left(r-\frac{h}{3}\right)=3.1416 h\left(\frac{c^{2}}{8}+\frac{h^{2}}{6}\right) \\
& A=2 \pi r h=6.2832 r h=3.1416\left(\frac{c^{2}}{4}+h^{2}\right) \\
& c=2 \sqrt{h(2 r-h)} ; \quad r=\frac{c^{2}+4 h^{2}}{8 h}
\end{aligned}
$$



Example: A segment of a sphere has the following dimensions: $h=50$ millimeters; $c=125$ millimeters. Find the volume $V$ and the radius of the sphere of which the segment is a part.

$$
\begin{aligned}
& V=3.1416 \times 50 \times\left(\frac{125^{2}}{8}+\frac{50^{2}}{6}\right)=157.08 \times\left(\frac{15,625}{8}+\frac{2500}{6}\right)=372,247 \mathrm{~mm}^{3}=372 \mathrm{~cm}^{3} \\
& r=\frac{125^{2}+4 \times 50^{2}}{8 \times 50}=\frac{15,625+10,000}{400}=\frac{25,625}{400}=64 \text { millimeters }
\end{aligned}
$$

## Ellipsoid:



$$
\text { Volume }=V=\frac{4 \pi}{3} a b c=4.1888 a b c
$$

In an ellipsoid of revolution, or spheroid, where $c=b$ :

$$
V=4.1888 a b^{2}
$$

Example: Find the volume of a spheroid in which $a=5$, and $b=$ $c=1.5$ inches.

$$
V=4.1888 \times 5 \times 1.5^{2}=47.124 \text { cubic inches }
$$

Spherical Zone:


$$
\begin{aligned}
\text { Volume }=V & =0.5236 h\left(\frac{3 c_{1}^{2}}{4}+\frac{3 c_{2}^{2}}{4}+h^{2}\right) \\
A & =2 \pi r h=6.2832 r h=\text { area of spherical surface } \\
r & =\sqrt{\frac{c_{2}^{2}}{4}+\left(\frac{c_{2}^{2}-c_{1}^{2}-4 h^{2}}{8 h}\right)^{2}}
\end{aligned}
$$

Example: In a spherical zone, let $c_{1}=3 ; c_{2}=4$; and $h=1.5$ inch. Find the volume.

$$
V=0.5236 \times 1.5 \times\left(\frac{3 \times 3^{2}}{4}+\frac{3 \times 4^{2}}{4}+1.5^{2}\right)=0.5236 \times 1.5 \times\left(\frac{27}{4}+\frac{48}{4}+2.25\right)=16.493 \mathrm{in}^{3}
$$

## Spherical Wedge:



Example: Find the area of the spherical surface and the volume of a wedge of a sphere. The diameter of the sphere is 100 millimeters, and the center angle $\alpha$ is 45 degrees.

$$
\begin{aligned}
& V=0.0116 \times 45 \times 50^{3}=0.0116 \times 45 \times 125,000=65,250 \mathrm{~mm}^{3}=65.25 \mathrm{~cm}^{3} \\
& A=0.0349 \times 45 \times 50^{2}=3926.25 \text { square millimeters }=39.26 \mathrm{~cm}^{2}
\end{aligned}
$$

## Hollow Sphere:



$$
\begin{aligned}
V= & \text { volume of material used } \\
& \text { to make a hollow sphere } \\
V & =\frac{4 \pi}{3}\left(R^{3}-r^{3}\right)=4.1888\left(R^{3}-r^{3}\right) \\
= & \frac{\pi}{6}\left(D^{3}-d^{3}\right)=0.5236\left(D^{3}-d^{3}\right)
\end{aligned}
$$

Example: Find the volume of a hollow sphere, 8 inches in outside diameter, with a thickness of material of 1.5 inch.
Here $R=4 ; r=4-1.5=2.5$.

$$
V=4.1888\left(4^{3}-2.5^{3}\right)=4.1888(64-15.625)=4.1888 \times 48.375=202.63 \text { cubic inches }
$$

## Paraboloid:



$$
\begin{aligned}
& \text { Volume }=V=1 / 2 \pi r^{2} h=0.3927 d^{2} h \\
& \qquad \begin{array}{r}
\text { Area }=A=\frac{2 \pi}{3 p}\left[\sqrt{\left(\frac{d^{2}}{4}+p^{2}\right)^{3}}-p^{3}\right] \\
\text { in which } p=\frac{d^{2}}{8 h}
\end{array}
\end{aligned}
$$

Example: Find the volume of a paraboloid in which $h=300$ millimeters and $d=125$ millimeters.

$$
V=0.3927 d^{2} h=0.3927 \times 125^{2} \times 300=1,840,781 \mathrm{~mm}^{3}=1,840.8 \mathrm{~cm}^{3}
$$

Paraboloidal Segment:


$$
\begin{aligned}
\text { Volume }=V & =\frac{\pi}{2} h\left(R^{2}+r^{2}\right)=1.5708 h\left(R^{2}+r^{2}\right) \\
& =\frac{\pi}{8} h\left(D^{2}+d^{2}\right)=0.3927 h\left(D^{2}+d^{2}\right)
\end{aligned}
$$

Example: Find the volume of a segment of a paraboloid in which $D=5$ inches, $d=3$ inches, and $h=6$ inches.

$$
\begin{aligned}
V & =0.3927 h\left(D^{2}+d^{2}\right)=0.3927 \times 6 \times\left(5^{2}+3^{2}\right) \\
& =0.3927 \times 6 \times 34=80.11 \text { cubic inches }
\end{aligned}
$$

## Torus:



$$
\begin{aligned}
\text { Volume }=V & =2 \pi^{2} R r^{2}=19.739 R r^{2} \\
& =\frac{\pi^{2}}{4} D d^{2}=2.4674 D d^{2} \\
\text { Area of surface }=A & =4 \pi^{2} R r=39.478 R r \\
& =\pi^{2} D d=9.8696 D d
\end{aligned}
$$

Example: Find the volume and area of surface of a torus in which $d=1.5$ and $D=5$ inches.

$$
\begin{aligned}
V & =2.4674 \times 5 \times 1.5^{2}=2.4674 \times 5 \times 2.25=27.76 \text { cubic inches } \\
A & =9.8696 \times 5 \times 1.5=74.022 \text { square inches }
\end{aligned}
$$

## Barrel:

$V=$ approximate volume.


If the sides are bent to the arc of a circle:

$$
V=\frac{1}{12} \pi h\left(2 D^{2}+d^{2}\right)=0.262 h\left(2 D^{2}+d^{2}\right)
$$

If the sides are bent to the arc of a parabola:

$$
V=0.209 h\left(2 D^{2}+D d+3 / 4 d^{2}\right)
$$

Example: Find the approximate contents of a barrel, the inside dimensions of which are $D=60$ centimeters, $d=50$ centimeters; $h=120$ centimeters.

$$
\begin{aligned}
V & =0.262 h\left(2 D^{2}+d^{2}\right)=0.262 \times 120 \times\left(2 \times 60^{2}+50^{2}\right) \\
& =0.262 \times 120 \times(7200+2500)=0.262 \times 120 \times 9700 \\
& =304,968 \text { cubic centimeters }=0.305 \text { cubic meter }
\end{aligned}
$$

## Ratio of Volumes:



If $d=$ base diameter and height of a cone, a paraboloid and a cylinder, and the diameter of a sphere, then the volumes of these bodies are to each other as follows:

Cone:paraboloid:sphere:cylinder $=1 / 3: 1 / 2: 2 / 3: 1$

Example: Assume, as an example, that the diameter of the base of a cone, paraboloid, and cylinder is 2 inches, that the height is 2 inches, and that the diameter of a sphere is 2 inches. Then the volumes, written in formula form, are as follows:

Cone Paraboloid Sphere Cylinder

$$
\frac{3.1416 \times 2^{2} \times 2}{12}: \frac{3.1416 \times(2 p)^{2} \times 2}{8}: \frac{3.1416 \times 2^{3}}{6}: \frac{3.1416 \times 2^{2} \times 2}{4}=1 / 3: 1 / 2: 2 / 3: 1
$$

## Packing Circles in Circles and Rectangles

Diameter of Circle Enclosing a Given Number of Smaller Circles.-Four of many possible compact arrangements of circles within a circle are shown at A, B, C, and D in Fig. 1. To determine the diameter of the smallest enclosing circle for a particular number of enclosed circles all of the same size, three factors that influence the size of the enclosing circle should be considered. These are discussed in the paragraphs that follow, which are based on the article "How Many Wires Can Be Packed into a Circular Conduit," by Jacques Dutka, Machinery, October 1956.

1) Arrangement of Center or Core Circles: The four most common arrangements of center or core circles are shown cross-sectioned in Fig. 1. It may seem, offhand, that the "A" pattern would require the smallest enclosing circle for a given number of enclosed circles but this is not always the case since the most compact arrangement will, in part, depend on the number of circles to be enclosed.


Fig. 1. Arrangements of Circles within a Circle
2) Diameter of Enclosing Circle When Outer Layer of Circles Is Complete: Successive, complete "layers" of circles may be placed around each of the central cores, Fig. 1, of 1, 2, 3 , or 4 circles as the case may be. The number of circles contained in arrangements of complete "layers" around a central core of circles, as well as the diameter of the enclosing circle, may be obtained using the data in Table 1. Thus, for example, the "A" pattern in Fig. 1 shows, by actual count, a total of 19 circles arranged in two complete "layers" around a central core consisting of one circle; this agrees with the data shown in the left half of Table 1 for $n=2$.

To determine the diameter of the enclosing circle, the data in the right half of Table 1 is used. Thus, for $n=2$ and an "A" pattern, the diameter $D$ is 5 times the diameter $d$ of the enclosed circles.
3) Diameter of Enclosing Circle When Outer Layer of Circles Is Not Complete: In most cases, it is possible to reduce the size of the enclosing circle from that required if the outer layer were complete. Thus, for example, the "B" pattern in Fig. 1 shows that the central core consisting of 2 circles is surrounded by 1 complete layer of 8 circles and 1 partial, outer layer of 4 circles, so that the total number of circles enclosed is 14 . If the outer layer were complete, then (from Table 1) the total number of enclosed circles would be 24 and the diameter of the enclosing circle would be $6 d$; however, since the outer layer is composed of only 4 circles out of a possible 14 for a complete second layer, a smaller diameter of enclosing circle may be used. Table 2 shows that for a total of 14 enclosed circles arranged in a " B " pattern with the outer layer of circles incomplete, the diameter for the enclosing circle is $4.606 d$.

Table 2 can be used to determine the smallest enclosing circle for a given number of circles to be enclosed by direct comparison of the "A," "B," and "C" columns. For data outside the range of Table 2, use the formulas in Dr. Dutka's article.

Table 1. Number of Circles Contained in Complete Layers of Circles and Diameter of Enclosing Circle (English or metric units)

| No. Complete Layers Over Core, $n$ | Number of Circles in Center Pattern |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 1 | 2 | 3 | 4 | 1 | 2 | 3 | 4 |
|  | Arrangement of Circles in Center Pattern (see Fig. 1) |  |  |  |  |  |  |  |
|  | "A" | "B" | "C" | "D" | "A" | "B" | "C" | "D" |
|  | Number of Circles, $N$, Enclosed |  |  |  | Diameter, $D$, of Enclosing Circle ${ }^{\text {a }}$ |  |  |  |
| 0 | 1 | 2 | 3 | 4 | d | $2 d$ | $2.155 d$ | $2.414 d$ |
| 1 | 7 | 10 | 12 | 14 | $3 d$ | $4 d$ | 4.055d | $4.386 d$ |
| 2 | 19 | 24 | 27 | 30 | $5 d$ | $6 d$ | 6.033d | 6.379 d |
| 3 | 37 | 44 | 48 | 52 | $7 d$ | $8 d$ | $8.024 d$ | 8.375d |
| 4 | 61 | 70 | 75 | 80 | $9 d$ | 10 d | $10.018 d$ | 10.373d |
| 5 | 91 | 102 | 108 | 114 | 11 d | 12 d | 12.015d | $12.372 d$ |
| $n$ | b | b | b | , | b | b | b | b |

${ }^{\text {a }}$ Diameter $D$ is given in terms of $d$, the diameter of the enclosed circles.
${ }^{\text {b }}$ For $n$ complete layers over core, the number of enclosed circles $N$ for the "A" center pattern is $3 n^{2}$ $+3 n+1$; for "B," $3 n^{2}+5 n+2$; for "C," $3 n^{2}+6 n+3$; for "D," $3 n^{2}+7 n+4$; while the diameter $D$ of the enclosing circle for "A" center pattern is $(2 n+1) d$; for "B," $(2 n+2) d$; for "C," $\left(1+2 \sqrt{n^{2}+n+1 / 3}\right) d$ and for "D," $\left(1+\sqrt{4 n^{2}+5.644 n+2}\right) d$.

Table 2. Factors for Determining Diameter, $D$, of Smallest Enclosing Circle for Various Numbers, $N$, of Enclosed Circles (English or metric units)

| $\stackrel{\text { No. }}{N}$ | Center Circle Pattern |  |  | $\left.\begin{gathered} \text { No. } \\ N \end{gathered} \right\rvert\,$ | Center Circle Pattern |  |  | $\begin{gathered} \text { No. } \\ N \end{gathered}$ | Center Circle Pattern |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | "A" | "B" | "C" |  | "A" | "B" | "C" |  | "A" | "B" | "C" |
|  | Diameter Factor $K$ |  |  |  | Diameter Factor $K$ |  |  |  | Diameter Factor $K$ |  |  |
| 2 | 3 | 2 | ... | 34 | 7.001 | 7.083 | 7.111 | 66 | 9.718 | 9.545 | 9.327 |
| 3 | 3 | 2.733 | 2.155 | 35 | 7.001 | 7.245 | 7.111 | 67 | 9.718 | 9.545 | 9.327 |
| 4 | 3 | 2.733 | 3.310 | 36 | 7.001 | 7.245 | 7.111 | 68 | 9.718 | 9.545 | 9.327 |
| 5 | 3 | 3.646 | 3.310 | 37 | 7.001 | 7.245 | 7.430 | 69 | 9.718 | 9.661 | 9.327 |
| 6 | 3 | 3.646 | 3.310 | 38 | 7.929 | 7.245 | 7.430 | 70 | 9.718 | 9.661 | 10.019 |
| 7 | 3 | 3.646 | 4.056 | 39 | 7.929 | 7.558 | 7.430 | 71 | 9.718 | 9.889 | 10.019 |
| 8 | 4.465 | 3.646 | 4.056 | 40 | 7.929 | 7.558 | 7.430 | 72 | 9.718 | 9.889 | 10.019 |
| 9 | 4.465 | 4 | 4.056 | 41 | 7.929 | 7.558 | 7.430 | 73 | 9.718 | 9.889 | 10.019 |
| 10 | 4.465 | 4 | 4.056 | 42 | 7.929 | 7.558 | 7.430 | 74 | 10.166 | 9.889 | 10.019 |
| 11 | 4.465 | 4.606 | 4.056 | 43 | 7.929 | 8.001 | 8.024 | 75 | 10.166 | 10 | 10.019 |
| 12 | 4.465 | 4.606 | 4.056 | 44 | 8.212 | 8.001 | 8.024 | 76 | 10.166 | 10 | 10.238 |
| 13 | 4.465 | 4.606 | 5.164 | 45 | 8.212 | 8.001 | 8.024 | 77 | 10.166 | 10.540 | 10.238 |
| 14 | 5 | 4.606 | 5.164 | 46 | 8.212 | 8.001 | 8.024 | 78 | 10.166 | 10.540 | 10.238 |
| 15 | 5 | 5.359 | 5.164 | 47 | 8.212 | 8.001 | 8.024 | 79 | 10.166 | 10.540 | 10.452 |
| 16 | 5 | 5.359 | 5.164 | 48 | 8.212 | 8.001 | 8.024 | 80 | 10.166 | 10.540 | 10.452 |
| 17 | 5 | 5.359 | 5.164 | 49 | 8.212 | 8.550 | 8.572 | 81 | 10.166 | 10.540 | 10.452 |
| 18 | 5 | 5.359 | 5.164 | 50 | 8.212 | 8.550 | 8.572 | 82 | 10.166 | 10.540 | 10.452 |
| 19 | 5 | 5.583 | 5.619 | 51 | 8.212 | 8.550 | 8.572 | 83 | 10.166 | 10.540 | 10.452 |
| 20 | 6.292 | 5.583 | 5.619 | 52 | 8.212 | 8.550 | 8.572 | 84 | 10.166 | 10.540 | 10.452 |
| 21 | 6.292 | 5.583 | 5.619 | 53 | 8.212 | 8.811 | 8.572 | 85 | 10.166 | 10.644 | 10.866 |
| 22 | 6.292 | 5.583 | 6.034 | 54 | 8.212 | 8.811 | 8.572 | 86 | 11 | 10.644 | 10.866 |
| 23 | 6.292 | 6.001 | 6.034 | 55 | 8.212 | 8.811 | 9.083 | 87 | 11 | 10.644 | 10.866 |
| 24 | 6.292 | 6.001 | 6.034 | 56 | 9.001 | 8.811 | 9.083 | 88 | 11 | 10.644 | 10.866 |
| 25 | 6.292 | 6.197 | 6.034 | 57 | 9.001 | 8.938 | 9.083 | 89 | 11 | 10.849 | 10.866 |
| 26 | 6.292 | 6.197 | 6.034 | 58 | 9.001 | 8.938 | 9.083 | 90 | 11 | 10.849 | 10.866 |
| 27 | 6.292 | 6.568 | 6.034 | 59 | 9.001 | 8.938 | 9.083 | 91 | 11 | 10.849 | 11.067 |
| 28 | 6.292 | 6.568 | 6.774 | 60 | 9.001 | 8.938 | 9.083 | 92 | 11.393 | 10.849 | 11.067 |
| 29 | 6.292 | 6.568 | 6.774 | 61 | 9.001 | 9.186 | 9.083 | 93 | 11.393 | 11.149 | 11.067 |
| 30 | 6.292 | 6.568 | 6.774 | 62 | 9.718 | 9.186 | 9.083 | 94 | 11.393 | 11.149 | 11.067 |
| 31 | 6.292 | 7.083 | 7.111 | 63 | 9.718 | 9.186 | 9.083 | 95 | 11.393 | 11.149 | 11.067 |
| 32 | 7.001 | 7.083 | 7.111 | 64 | 9.718 | 9.186 | 9.327 | 96 | 11.393 | 11.149 | 11.067 |
| 33 | 7.001 | 7.083 | 7.111 | 65 | 9.718 | 9.545 | 9.327 | 97 | 11.393 | 11.441 | 11.264 |

Table 2. (Continued) Factors for Determining Diameter, D, of Smallest Enclosing Circle for Various Numbers, $N$, of Enclosed Circles (English or metric units)

| $\underset{N}{\mathrm{No}} \mathrm{~N}$ | Center Circle Pattern |  |  | $\stackrel{\text { No. }}{N}$ | Center Circle Pattern |  |  | $\begin{gathered} \text { No. } \\ N \end{gathered}$ | Center Circle Pattern |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | "A" | "B" | "C" |  | "A" | "B" | "C" |  | "A" | "B" | "C" |
|  | Diameter Factor $K$ |  |  |  | Diameter Factor $K$ |  |  |  | Diameter Factor $K$ |  |  |
| 98 | 11.584 | 11.441 | 11.264 | 153 | 14.115 | 14 | 14.013 | 208 | 16.100 | 16 | 16.144 |
| 99 | 11.584 | 11.441 | 11.264 | 154 | 14.115 | 14 | 14.013 | 209 | 16.100 | 16.133 | 16.144 |
| 100 | 11.584 | 11.441 | 11.264 | 155 | 14.115 | 14.077 | 14.013 | 210 | 16.100 | 16.133 | 16.144 |
| 101 | 11.584 | 11.536 | 11.264 | 156 | 14.115 | 14.077 | 14.013 | 211 | 16.100 | 16.133 | 16.144 |
| 102 | 11.584 | 11.536 | 11.264 | 157 | 14.115 | 14.077 | 14.317 | 212 | 16.621 | 16.133 | 16.144 |
| 103 | 11.584 | 11.536 | 12.016 | 158 | 14.115 | 14.077 | 14.317 | 213 | 16.621 | 16.395 | 16.144 |
| 104 | 11.584 | 11.536 | 12.016 | 159 | 14.115 | 14.229 | 14.317 | 214 | 16.621 | 16.395 | 16.276 |
| 105 | 11.584 | 11.817 | 12.016 | 160 | 14.115 | 14.229 | 14.317 | 215 | 16.621 | 16.395 | 16.276 |
| 106 | 11.584 | 11.817 | 12.016 | 161 | 14.115 | 14.229 | 14.317 | 216 | 16.621 | 16.395 | 16.276 |
| 107 | 11.584 | 11.817 | 12.016 | 162 | 14.115 | 14.229 | 14.317 | 217 | 16.621 | 16.525 | 16.276 |
| 108 | 11.584 | 11.817 | 12.016 | 163 | 14.115 | 14.454 | 14.317 | 218 | 16.621 | 16.525 | 16.276 |
| 109 | 11.584 | 12 | 12.016 | 164 | 14.857 | 14.454 | 14.317 | 219 | 16.621 | 16.525 | 16.276 |
| 110 | 12.136 | 12 | 12.016 | 165 | 14.857 | 14.454 | 14.317 | 220 | 16.621 | 16.525 | 16.535 |
| 111 | 12.136 | 12.270 | 12.016 | 166 | 14.857 | 14.454 | 14.317 | 221 | 16.621 | 16.589 | 16.535 |
| 112 | 12.136 | 12.270 | 12.016 | 167 | 14.857 | 14.528 | 14.317 | 222 | 16.621 | 16.589 | 16.535 |
| 113 | 12.136 | 12.270 | 12.016 | 168 | 14.857 | 14.528 | 14.317 | 223 | 16.621 | 16.716 | 16.535 |
| 114 | 12.136 | 12.270 | 12.016 | 169 | 14.857 | 14.528 | 14.614 | 224 | 16.875 | 16.716 | 16.535 |
| 115 | 12.136 | 12.358 | 12.373 | 170 | 15 | 14.528 | 14.614 | 225 | 16.875 | 16.716 | 16.535 |
| 116 | 12.136 | 12.358 | 12.373 | 171 | 15 | 14.748 | 14.614 | 226 | 16.875 | 16.716 | 17.042 |
| 117 | 12.136 | 12.358 | 12.373 | 172 | 15 | 14.748 | 14.614 | 227 | 16.875 | 16.716 | 17.042 |
| 118 | 12.136 | 12.358 | 12.373 | 173 | 15 | 14.748 | 14.614 | 228 | 16.875 | 16.716 | 17.042 |
| 119 | 12.136 | 12.533 | 12.373 | 174 | 15 | 14.748 | 14.614 | 229 | 16.875 | 16.716 | 17.042 |
| 120 | 12.136 | 12.533 | 12.373 | 175 | 15 | 14.893 | 15.048 | 230 | 16.875 | 16.716 | 17.042 |
| 121 | 12.136 | 12.533 | 12.548 | 176 | 15 | 14.893 | 15.048 | 231 | 16.875 | 17.094 | 17.042 |
| 122 | 13 | 12.533 | 12.548 | 177 | 15 | 14.893 | 15.048 | 232 | 16.875 | 17.094 | 17.166 |
| 123 | 13 | 12.533 | 12.548 | 178 | 15 | 14.893 | 15.048 | 233 | 16.875 | 17.094 | 17.166 |
| 124 | 13 | 12.533 | 12.719 | 179 | 15 | 15.107 | 15.048 | 234 | 16.875 | 17.094 | 17.166 |
| 125 | 13 | 12.533 | 12.719 | 180 | 15 | 15.107 | 15.048 | 235 | 16.875 | 17.094 | 17.166 |
| 126 | 13 | 12.533 | 12.719 | 181 | 15 | 15.107 | 15.190 | 236 | 17 | 17.094 | 17.166 |
| 127 | 13 | 12.790 | 12.719 | 182 | 15 | 15.107 | 15.190 | 237 | 17 | 17.094 | 17.166 |
| 128 | 13.166 | 12.790 | 12.719 | 183 | 15 | 15.178 | 15.190 | 238 | 17 | 17.094 | 17.166 |
| 129 | 13.166 | 12.790 | 12.719 | 184 | 15 | 15.178 | 15.190 | 239 | 17 | 17.463 | 17.166 |
| 130 | 13.166 | 12.790 | 13.056 | 185 | 15 | 15.178 | 15.190 | 240 | 17 | 17.463 | 17.166 |
| 131 | 13.166 | 13.125 | 13.056 | 186 | 15 | 15.178 | 15.190 | 241 | 17 | 17.463 | 17.290 |
| 132 | 13.166 | 13.125 | 13.056 | 187 | 15 | 15.526 | 15.469 | 242 | 17.371 | 17.463 | 17.290 |
| 133 | 13.166 | 13.125 | 13.056 | 188 | 15.423 | 15.526 | 15.469 | 243 | 17.371 | 17.523 | 17.290 |
| 134 | 13.166 | 13.125 | 13.056 | 189 | 15.423 | 15.526 | 15.469 | 244 | 17.371 | 17.523 | 17.290 |
| 135 | 13.166 | 13.125 | 13.056 | 190 | 15.423 | 15.526 | 15.469 | 245 | 17.371 | 17.523 | 17.290 |
| 136 | 13.166 | 13.125 | 13.221 | 191 | 15.423 | 15.731 | 15.469 | 246 | 17.371 | 17.523 | 17.290 |
| 137 | 13.166 | 13.289 | 13.221 | 192 | 15.423 | 15.731 | 15.469 | 247 | 17.371 | 17.523 | 17.654 |
| 138 | 13.166 | 13.289 | 13.221 | 193 | 15.423 | 15.731 | 15.743 | 248 | 17.371 | 17.523 | 17.654 |
| 139 | 13.166 | 13.289 | 13.221 | 194 | 15.423 | 15.731 | 15.743 | 249 | 17.371 | 17.523 | 17.654 |
| 140 | 13.490 | 13.289 | 13.221 | 195 | 15.423 | 15.731 | 15.743 | 250 | 17.371 | 17.523 | 17.654 |
| 141 | 13.490 | 13.530 | 13.221 | 196 | 15.423 | 15.731 | 15.743 | 251 | 17.371 | 17.644 | 17.654 |
| 142 | 13.490 | 13.530 | 13.702 | 197 | 15.423 | 15.731 | 15.743 | 252 | 17.371 | 17.644 | 17.654 |
| 143 | 13.490 | 13.530 | 13.702 | 198 | 15.423 | 15.731 | 15.743 | 253 | 17.371 | 17.644 | 17.773 |
| 144 | 13.490 | 13.530 | 13.702 | 199 | 15.423 | 15.799 | 16.012 | 254 | 18.089 | 17.644 | 17.773 |
| 145 | 13.490 | 13.768 | 13.859 | 200 | 16.100 | 15.799 | 16.012 | 255 | 18.089 | 17.704 | 17.773 |
| 146 | 13.490 | 13.768 | 13.859 | 201 | 16.100 | 15.799 | 16.012 | 256 | 18.089 | 17.704 | 17.773 |
| 147 | 13.490 | 13.768 | 13.859 | 202 | 16.100 | 15.799 | 16.012 | 257 | 18.089 | 17.704 | 17.773 |
| 148 | 13.490 | 13.768 | 13.859 | 203 | 16.100 | 15.934 | 16.012 | 258 | 18.089 | 17.704 | 17.773 |
| 149 | 13.490 | 14 | 13.859 | 204 | 16.100 | 15.934 | 16.012 | 259 | 18.089 | 17.823 | 18.010 |
| 150 | 13.490 | 14 | 13.859 | 205 | 16.100 | 15.934 | 16.012 | 260 | 18.089 | 17.823 | 18.010 |
| 151 | 13.490 | 14 | 14.013 | 206 | 16.100 | 15.934 | 16.012 | 261 | 18.089 | 17.823 | 18.010 |
| 152 | 14.115 | 14 | 14.013 | 207 | 16.100 | 16 | 16.012 | 262 | 18.089 | 17.823 | 18.010 |

The diameter $D$ of the enclosing circle is equal to the diameter factor, $K$, multiplied by $d$, the diameter of the enclosed circles, or $D=K \times d$. For example, if the number of circles to be enclosed, $N$, is 12 , and the center circle arrangement is " C ," then for $d=1 \frac{1}{2}$ inches, $\mathrm{D}=4.056 \times 1 \frac{1}{2}=6.084$ inches. If $d=50$ millimeters, then $D=4.056 \times 50=202.9$ millimeters.

Approximate Formula When Number of Enclosed Circles Is Large: When a large number of circles are to be enclosed, the arrangement of the center circles has little effect on the diameter of the enclosing circle. For numbers of circles greater than 10,000 , the diameter of the enclosing circle may be calculated within 2 per cent from the formula $D=d(1+\sqrt{N \div 0.907})$. In this formula, $D=$ diameter of the enclosing circle; $d=$ diameter of the enclosed circles; and $N$ is the number of enclosed circles.

An alternative approach relates the area of each of the same-sized circles to be enclosed to the area of the enclosing circle (or container), as shown in Figs. 1 through 27. The table shows efficient ways for packing various numbers of circles $N$, from 2 up to 97 .

In the table, $D=$ the diameter of each circle to be enclosed, $d=$ the diameter of the enclosing circle or container, and $\Phi=N D^{2} / d^{2}=$ ratio of the area of the $N$ circles to the area of the enclosing circle or container, which is the packing efficiency. Cross-hatching in the diagrams indicates loose circles that may need packing constraints.

Data for Numbers of Circles in Circles

| $N$ | $d / D$ | $\Phi$ | Fig. | $N$ | $d / D$ | $\Phi$ | Fig. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 | 2.0000 | 0.500 | 1 | 17 | 4.7920 | 0.740 | 15 |
| 3 | 2.1547 | 0.646 | 2 | 18 | 4.8637 | 0.761 | 16 |
| 4 | 2.4142 | 0.686 | 3 | 19 | 4.8637 | 0.803 | 16 |
| 5 | 2.7013 | 0.685 | 4 | 20 | 5.1223 | 0.762 | 17 |
| 6 | 3.0000 | 0.667 | 5 | 21 | 5.2523 | 0.761 | 18 |
| 7 | 3.0000 | 0.778 | 5 | 22 | 5.4397 | 0.743 | 19 |
| 8 | 3.3048 | 0.733 | 6 | 23 | 5.5452 | 9.748 | 20 |
| 9 | 3.6131 | 0.689 | 7 | 24 | 5.6517 | 0.751 | 21 |
| 10 | 3.8130 | 0.688 | 8 | 25 | 5.7608 | 0.753 | 22 |
| 11 | 3.9238 | 0.714 | 9 | 31 | 6.2915 | 0.783 | 23 |
| 12 | 4.0296 | 0.739 | 10 | 37 | 6.7588 | 0.810 | 24 |
| 13 | 4.2361 | 0.724 | 11 | 55 | 8.2111 | 0.816 | 25 |
| 14 | 4.3284 | 0.747 | 12 | 61 | 8.6613 | 0.813 | 26 |
| 15 | 4.5214 | 0.734 | 13 | 97 | 11.1587 | 0.779 | 27 |
| 16 | 4.6154 | 0.751 | 14 | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |

Packing of large numbers of circles, such as the 97 in Fig. 27, may be approached by drawing a triangular pattern of circles, as shown in Fig. 28, which represents three circles near the center of the array. The point of a compass is then placed at $A, B$, or $C$, or anywhere within triangle $A B C$, and the radius of the compass is gradually enlarged until it encompasses the number of circles to be enclosed. As a first approximation of the diameter,
$1.14 D \sqrt{N}$ may be tried.


Fig. 1. $N=2$


Fig. 2. $N=3$


Fig. 3. $N=4$


Fig. 4. $N=5$


Fig. 5. $N=7$


Fig. 9. $N=11$


Fig. 13. $N=15$


Fig. 17. $N=20$


Fig. 21. $N=24$


Fig. 25. $N=55$


Fig. 6. $N=8$


Fig. 10. $N=12$


Fig. 14. $N=16$


Fig. 18. $N=21$


Fig. 22. $N=25$


Fig. 26. $N=61$


Fig. 7. $N=9$


Fig. 11. $N=13$


Fig. 15. $N=17$


Fig. 19. $N=22$


Fig. 23. $N=31$


Fig. 27. $N=97$


Fig. 8. $N=10$


Fig. 12. $N=14$


Fig. 16. $N=19$


Fig. 20. $N=23$


Fig. 24. $N=37$


Fig. 28.

Circles within Rectangles.-For small numbers $N$ of circles, packing (for instance, of cans) is less vital than for larger numbers and the number will usually govern the decision whether to use a rectangular or a triangular pattern, examples of which are seen in Figs. 29 and 30 .



Fig. 30. Triangular Pattern $(r=3, c=7)$

Fig. 29. Rectangular Pattern $(r=4, c=5)$
If $D$ is the can diameter and $H$ its height, the arrangement in Fig. 29 will hold 20 circles or cans in a volume of $5 D \times 4 D \times H=20 D^{2} H$. The arrangement in Fig. 30 will pack the same 20 cans into a volume of $7 D \times 2.732 D \times H=19.124 D^{2} H$, a reduction of 4.4 per cent. When the ratio of $H / D$ is less than $1.196: 1$, the rectangular pattern requires less surface area (therefore less material) for the six sides of the box, but for greater ratios, the triangular pattern is better. Some numbers, such as 19 , can be accommodated only in a triangular pattern.
The following table shows possible patterns for 3 to 25 cans, where $N=$ number of circles, $P=$ pattern ( $R$ rectangular or $T$ triangular), and $r$ and $c=$ numbers of rows and columns, respectively. The final table column shows the most economical application, where $V=$ best volume, $S=$ best surface area (sometimes followed by a condition on $H / D$ ). For the rectangular pattern, dimensions of the container are $r D \times c D$, and for the triangular pattern, the dimensions are $) \times[1+(r+70(-1)) \sqrt{3} / 2]$, or $c D^{2}[1+0.866(r-1)]$.

Numbers of Circles in Rectangular Arrangements

| $N$ | $P$ | $r$ | $c$ | Application | $N$ | $P$ | $r$ | $c$ | Application |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | $T$ | 2 | 2 | $V, S$ | 15 | $R$ | 3 | 5 | $(S, H / D>0.038)$ |
|  |  |  |  | $V, S$ | 16 | $R$ | 4 | 4 | $V,(S, H / D<0.038)$ |
| 4 | $R$ | 2 | 2 | $V, S$ | 17 | $T$ | 3 | 6 | $V, S$ |
| 5 | $T$ | 3 | 2 | $V, S$ | 18 | $T$ | 5 | 4 | $V, S$ |
| 6 | $R$ | 2 | 3 | $V$ | 19 | $T$ | 2 | 10 | $V, S$ |
| 7 | $T$ | 2 | 4 | $V, S$ |  | $V, S$ |  |  |  |
| 8 | $R$ | 4 | 2 | $V,(S, H / D<0.732)$ | 20 | $R$ | 4 | 5 | $(S, H / D>1.196)$ |
|  | $T$ | 3 | 3 | $(S, H / D>0.732)$ |  | $T$ | 3 | 7 | $V,(S, H / D<1.196)$ |
| 9 | $R$ | 3 | 3 | $V, S$ |  | $R$ | 3 | 7 | $(S, 0.165<H / D<0.479)$ |
| 10 | $R$ | 5 | 2 | $V,(S, H / D>1.976)$ | 21 | $T$ | 6 | 4 | $(S, H / D>0.479)$ |
|  | $T$ | 4 | 3 | $(S, H / D>1.976)$ |  | $T$ | 2 | 11 | $V,(S, H / D<0.165)$ |
| 11 | $T$ | 3 | 4 | $V, S$ | 22 | $T$ | 4 | 6 | $V, S$ |
| 12 | $R$ | 3 | 4 | $V, S$ | 23 | $T$ | 5 | 5 | $(S, H / D>0.366)$ |
| 13 | $T$ | 5 | 3 | $(S, H / D>0.236)$ |  | $T$ | 3 | 8 | $V,(S, H / D<0.366)$ |
|  | $T$ | 2 | 7 | $V,(S, H / D<0.236)$ | 24 | $R$ | 4 | 6 | $V, S$ |
| 14 | $T$ | 4 | 4 | $(S, H / D>5.464)$ |  | $R$ | 5 | 5 | $(S, H / D>1.10)$ |
|  | $T$ | 3 | 5 | $V,(S, H / D<5.464)$ | 25 | $T$ | 7 | 4 | $(S, 0.113<H / D<1.10)$ |
|  |  |  |  |  |  | $T$ | 2 | 13 | $V,(S, H / D<0.133)$ |

Formulas and Table for Regular Polygons.-The following formulas and table can be used to calculate the area, length of side, and radii of the inscribed and circumscribed circles of regular polygons (equal sided).

$$
\begin{aligned}
A & =N S^{2} \cot \alpha \div 4=N R^{2} \sin \alpha \cos \alpha=N r^{2} \tan \alpha \\
r & =R \cos \alpha=(S \cot \alpha) \div 2=\sqrt{(A \times \cot \alpha) \div N} \\
R & =S \div(2 \sin \alpha)=r \div \cos \alpha=\sqrt{A \div(N \sin \alpha \cos \alpha)} \\
S & =2 R \sin \alpha=2 r \tan \alpha=2 \sqrt{(A \times \tan \alpha) \div N}
\end{aligned}
$$

where $N=$ number of sides; $S=$ length of side; $R=$ radius of circumscribed circle; $r=$ radius of inscribed circle; $A=$ area of polygon; and, $\alpha=180^{\circ} \div \mathrm{N}=$ one-half center angle of one side (see Regular Polygon on page 62) .

Area, Length of Side, and Inscribed and Circumscribed Radii of Regular Polygons

| No. <br> of <br> Sides | $\frac{A}{S^{2}}$ | $\frac{A}{R^{2}}$ | $\frac{A}{r^{2}}$ | $\frac{R}{S}$ | $\frac{R}{r}$ | $\frac{S}{R}$ | $\frac{S}{r}$ | $\frac{r}{R}$ | $\frac{r}{S}$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 3 | 0.4330 | 1.2990 | 5.1962 | 0.5774 | 2.0000 | 1.7321 | 3.4641 | 0.5000 | 0.2887 |
| 4 | 1.0000 | 2.0000 | 4.0000 | 0.7071 | 1.4142 | 1.4142 | 2.0000 | 0.7071 | 0.5000 |
| 5 | 1.7205 | 2.3776 | 3.6327 | 0.8507 | 1.2361 | 1.1756 | 1.4531 | 0.8090 | 0.6882 |
| 6 | 2.5981 | 2.5981 | 3.4641 | 1.0000 | 1.1547 | 1.0000 | 1.1547 | 0.8660 | 0.8660 |
| 7 | 3.6339 | 2.7364 | 3.3710 | 1.1524 | 1.1099 | 0.8678 | 0.9631 | 0.9010 | 1.0383 |
| 8 | 4.8284 | 2.8284 | 3.3137 | 1.3066 | 1.0824 | 0.7654 | 0.8284 | 0.9239 | 1.2071 |
| 9 | 6.1818 | 2.8925 | 3.2757 | 1.4619 | 1.0642 | 0.6840 | 0.7279 | 0.9397 | 1.3737 |
| 10 | 7.6942 | 2.9389 | 3.2492 | 1.6180 | 1.0515 | 0.6180 | 0.6498 | 0.9511 | 1.5388 |
| 12 | 11.196 | 3.0000 | 3.2154 | 1.9319 | 1.0353 | 0.5176 | 0.5359 | 0.9659 | 1.8660 |
| 16 | 20.109 | 3.0615 | 3.1826 | 2.5629 | 1.0196 | 0.3902 | 0.3978 | 0.9808 | 2.5137 |
| 20 | 31.569 | 3.0902 | 3.1677 | 3.1962 | 1.0125 | 0.3129 | 0.3168 | 0.9877 | 3.1569 |
| 24 | 45.575 | 3.1058 | 3.1597 | 3.8306 | 1.0086 | 0.2611 | 0.2633 | 0.9914 | 3.7979 |
| 32 | 81.225 | 3.1214 | 3.1517 | 5.1011 | 1.0048 | 0.1960 | 0.1970 | 0.9952 | 5.0766 |
| 48 | 183.08 | 3.1326 | 3.1461 | 7.6449 | 1.0021 | 0.1308 | 0.1311 | 0.9979 | 7.6285 |
| 64 | 325.69 | 3.1365 | 3.1441 | 10.190 | 1.0012 | 0.0981 | 0.0983 | 0.9988 | 10.178 |

Example 1: A regular hexagon is inscribed in a circle of 6 inches diameter. Find the area and the radius of an inscribed circle. Here $R=3$. From the table, area $A=2.5981 R^{2}=2.5981$ $\times 9=23.3829$ square inches. Radius of inscribed circle, $r=0.866 R=0.866 \times 3=2.598$ inches.

Example 2: An octagon is inscribed in a circle of 100 millimeters diameter. Thus $R=50$. Find the area and radius of an inscribed circle. $A=2.8284 R^{2}=2.8284 \times 2500=7071 \mathrm{~mm}^{2}$ $=70.7 \mathrm{~cm}^{2}$. Radius of inscribed circle, $r=0.9239 R=09239 \times 50=46.195 \mathrm{~mm}$.

Example 3:Thirty-two bolts are to be equally spaced on the periphery of a bolt-circle, 16 inches in diameter. Find the chordal distance between the bolts. Chordal distance equals the side $S$ of a polygon with 32 sides. $R=8$. Hence, $S=0.196 R=0.196 \times 8=1.568$ inch.

Example 4: Sixteen bolts are to be equally spaced on the periphery of a bolt-circle, 250 millimeters diameter. Find the chordal distance between the bolts. Chordal distance equals the side $S$ of a polygon with 16 sides. $R=125$. Thus, $S=0.3902 R=0.3902 \times 125=48.775$ millimeters.

## Tabulated Dimensions Of Geometric Shapes

Diameters of Circles and Sides of Squares of Equal Area

|  |  |  | (Th] | The table below will be found useful for determining the diameter of a circle of an area equal to that of a square, the side of which is known, or for determining the side of a square which has an area equal to that of a circle, the area or diameter of which is known. For example, if the diameter of a circle is $17 \frac{1}{2}$ inches, it is found from the table that the side of a square of the same area is 15.51 inches. |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Diam. of Circle, $D$ | Side of Square, $S$ | Area of Circle or Square | Diam. of Circle, $D$ | Side of Square, $S$ | Area of Circle or Square | Diam. of Circle, $D$ | Side of Square, $S$ | Area of Circle or Square |
| 1/2 | 0.44 | 0.196 | 201/2 | 18.17 | 330.06 | 401/2 | 35.89 | 1288.25 |
| 1 | 0.89 | 0.785 | 21 | 18.61 | 346.36 | 41 | 36.34 | 1320.25 |
| 11/2 | 1.33 | 1.767 | 211/2 | 19.05 | 363.05 | 411/2 | 36.78 | 1352.65 |
| 2 | 1.77 | 3.142 | 22 | 19.50 | 380.13 | 42 | 37.22 | 1385.44 |
| 21/2 | 2.22 | 4.909 | $221 / 2$ | 19.94 | 397.61 | $421 / 2$ | 37.66 | 1418.63 |
| 3 | 2.66 | 7.069 | 23 | 20.38 | 415.48 | 43 | 38.11 | 1452.20 |
| $31 / 2$ | 3.10 | 9.621 | 231/2 | 20.83 | 433.74 | $431 / 2$ | 38.55 | 1486.17 |
| 4 | 3.54 | 12.566 | 24 | 21.27 | 452.39 | 44 | 38.99 | 1520.53 |
| $41 / 2$ | 3.99 | 15.904 | $241 / 2$ | 21.71 | 471.44 | 441/2 | 39.44 | 1555.28 |
| 5 | 4.43 | 19.635 | 25 | 22.16 | 490.87 | 45 | 39.88 | 1590.43 |
| 51/2 | 4.87 | 23.758 | $251 / 2$ | 22.60 | 510.71 | 451/2 | 40.32 | 1625.97 |
| 6 | 5.32 | 28.274 | 26 | 23.04 | 530.93 | 46 | 40.77 | 1661.90 |
| $61 / 2$ | 5.76 | 33.183 | 261/2 | 23.49 | 551.55 | $461 / 2$ | 41.21 | 1698.23 |
| 7 | 6.20 | 38.485 | 27 | 23.93 | 572.56 | 47 | 41.65 | 1734.94 |
| 71/2 | 6.65 | 44.179 | 271/2 | 24.37 | 593.96 | 471/2 | 42.10 | 1772.05 |
| 8 | 7.09 | 50.265 | 28 | 24.81 | 615.75 | 48 | 42.54 | 1809.56 |
| 81/2 | 7.53 | 56.745 | $281 / 2$ | 25.26 | 637.94 | $481 / 2$ | 42.98 | 1847.45 |
| 9 | 7.98 | 63.617 | 29 | 25.70 | 660.52 | 49 | 43.43 | 1885.74 |
| 91/2 | 8.42 | 70.882 | 291/2 | 26.14 | 683.49 | 491/2 | 43.87 | 1924.42 |
| 10 | 8.86 | 78.540 | 30 | 26.59 | 706.86 | 50 | 44.31 | 1963.50 |
| 101/2 | 9.31 | 86.590 | $301 / 2$ | 27.03 | 730.62 | 501/2 | 44.75 | 2002.96 |
| 11 | 9.75 | 95.033 | 31 | 27.47 | 754.77 | 51 | 45.20 | 2042.82 |
| 11/2 | 10.19 | 103.87 | $311 / 2$ | 27.92 | 779.31 | 511/2 | 45.64 | 2083.07 |
| 12 | 10.63 | 113.10 | 32 | 28.36 | 804.25 | 52 | 46.08 | 2123.72 |
| $121 / 2$ | 11.08 | 122.72 | $321 / 2$ | 28.80 | 829.58 | $521 / 2$ | 46.53 | 2164.75 |
| 13 | 11.52 | 132.73 | 33 | 29.25 | 855.30 | 53 | 46.97 | 2206.18 |
| $131 / 2$ | 11.96 | 143.14 | $331 / 2$ | 29.69 | 881.41 | $531 / 2$ | 47.41 | 2248.01 |
| 14 | 12.41 | 153.94 | 34 | 30.13 | 907.92 | 54 | 47.86 | 2290.22 |
| $141 / 2$ | 12.85 | 165.13 | $341 / 2$ | 30.57 | 934.82 | $541 / 2$ | 48.30 | 2332.83 |
| 15 | 13.29 | 176.71 | 35 | 31.02 | 962.11 | 55 | 48.74 | 2375.83 |
| 151/2 | 13.74 | 188.69 | $351 / 2$ | 31.46 | 989.80 | 551/2 | 49.19 | 2419.22 |
| 16 | 14.18 | 201.06 | 36 | 31.90 | 1017.88 | 56 | 49.63 | 2463.01 |
| $161 / 2$ | 14.62 | 213.82 | $361 / 2$ | 32.35 | 1046.35 | $561 / 2$ | 50.07 | 2507.19 |
| 17 | 15.07 | 226.98 | 37 | 32.79 | 1075.21 | 57 | 50.51 | 2551.76 |
| 171/2 | 15.51 | 240.53 | $371 / 2$ | 33.23 | 1104.47 | 571/2 | 50.96 | 2596.72 |
| 18 | 15.95 | 254.47 | 38 | 33.68 | 1134.11 | 58 | 51.40 | 2642.08 |
| 181/2 | 16.40 | 268.80 | $381 / 2$ | 34.12 | 1164.16 | $581 / 2$ | 51.84 | 2687.83 |
| 19 | 16.84 | 283.53 | 39 | 34.56 | 1194.59 | 59 | 52.29 | 2733.97 |
| 191/2 | 17.28 | 298.65 | $391 / 2$ | 35.01 | 1225.42 | 591/2 | 52.73 | 2780.51 |
| 20 | 17.72 | 314.16 | 40 | 35.45 | 1256.64 | 60 | 53.17 | 2827.43 |

Segments of Circles for Radius $=\mathbf{1}$ (English or metric units)

|  | $\bar{\nu}$ |  |  |  | Formulas for segments of circles are given on page 63. When the central angle $\alpha$ and radius $r$ are known, the tables on these pages can be used to find the length of arc $l$, height of segment $h$, chord length $c$, and segment area $A$. When angle $\alpha$ and radius $r$ are not known, but segment height $h$ and chord length $c$ are known or can be measured, the ratio $h / c$ can be used to enter the table and find $\alpha, l$, and $A$ by linear interpolation. Radius $r$ is found by the formula on page 63. The value of $l$ is then multiplied by the radius $r$ and the area $A$ by $r^{2}$, the square of the radius. <br> Angle $\alpha$ can be found thus with an accuracy of about 0.001 degree; arc length $l$ with an error of about 0.02 per cent; and area $A$ with an error ranging from about 0.02 per cent for the highest entry value of $h / c$ to about 1 per cent for values of $h / c$ of about 0.050 . For lower values of $h / c$, and where greater accuracy is required, area $A$ should be found by the formula on page 63 . |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \begin{array}{c} \theta, \\ \text { Deg } \end{array} \end{gathered}$ |  | $h$ |  | Area A | h/c | $\\| \begin{gathered} \theta, \\ \text { Deg. } \end{gathered}$ | 1 | $h$ | ${ }_{c}$ | rea A | h/c |
|  | 0.01745 | 0.00004 | 0.01745 | 0.0000 | 0.00218 | 41 | 0.71558 | 0.06333 | 0.70041 | 0.0298 | 0.09041 |
| 2 | 0.034 | 0.000 | 0.03490 | 0.0000 | 004 | 42 | 0.7330 | 0.066 | 16 | 0.0320 | 0.09267 |
| 3 | 0.05 | 0.00034 | 0.05235 | 0.0000 | 06.5 | 43 | 0.75049 | 0.069 | 0.73300 | 0.0342 | 93 |
| 4 | 0.06981 | 0.00061 | 0.06980 | 0.0000 | 0.00873 | 44 | 0.76794 | 0.07282 | 0.7492 | 0.03 | 0.097 |
| 5 | 0.08727 | 0.00093 | 087 | 0.0001 | ${ }^{0} .0109$ | 45 | 0.7854 | 0.07612 | 0.76537 | 0.0391 | 0.0994 |
| 6 | 0.10472 | 0.0013 | 0.1046 | 0.000 | 0.013 | 46 | 0.80285 | 0.079 | 0.7814 | 0.04 | 0.10 |
| 7 | 0.12217 | 0.00187 | 0.12210 | 0002 | 0.01528 | 47 | 0.82030 | 0.0 | 9750 | 0.0445 | 0.10400 |
| 8 | 0.13963 | 0.00244 | 0.13951 | 0.0002 | 0.01746 | 48 | 0.83776 | 0.0864 | 0.81347 | 0.0473 | 0.10628 |
|  | 0.15708 | 0.00308 | 0.15692 | 0.0003 | 0.01965 | 49 | 0.85521 | 0.09004 | 0.82939 | 0.0503 | 0.10856 |
| 10 | 0.17453 | 0.00381 | 0.17431 | 0.0004 | 0.02183 | 50 | 0.87266 | 0.09369 | 0.84524 | 0.053 | 0.11085 |
| 11 | 0.19199 | 0.00460 | 0.19169 | 0.0006 | 0.02402 | 51 | 0.89012 | 0.0974 | 0.86102 | 0.0565 | 0.11314 |
| 12 | 0.20944 | 0.005 | 0.20906 | 0.000 | 0.02620 | 52 | 0.90757 | 0.1012 | 0.8767 | 0.059 | 0.11543 |
| 13 | 0.22689 | 0.00643 | 0.22641 | 0.0010 | 0.02839 | 53 | 0.92502 | 0.1050 | 0.89240 | 0.0632 | 0.11773 |
| 14 | 0.24435 | 0.007 | 0.24374 | 0.0012 | 0.03058 | 54 | 0.94248 | 0.1089 | 0.907 | 0.066 | 0.12004 |
| 15 | 0.26180 | 0.00856 | 0.26105 | 0.0015 | 0.03277 | 55 | 0.95993 | 0.11299 | 0.92350 | 0.070 | 0.12235 |
| 16 | 0.27 | 0.00973 | 0.27835 | 0.0018 | 0.03496 | 56 | 0.9 | 0.11705 | 0.93894 | 0.0742 | 0.12466 |
| 17 | 0.29671 | 0.01098 | 0.29562 | 0.0022 | 0.03716 | 57 | 0.99484 | 0.12118 | 0.95432 | 0.078 | 0.12698 |
| 18 | 0.31 | 0.01231 | 0.31287 | 0.0026 | 0.03935 | 58 | 1.01229 | 0.12538 | 0.96962 | 0.0821 | 0.1 |
| 19 | 0.33161 | 0.01371 | 0.33010 | 0.0030 | 0.04155 | 59 | 1.02974 | 0.12964 | 0.98485 | 0.086 | 0.13164 |
| 20 | 0.34907 | 0.01519 | 0.34730 | 0.0035 | 0.04374 | 60 | 1.0472 | 0.1339 | 1.000 | 0.09 | 0.133 |
| 21 | 0.36652 | 0.01675 | 0.36447 | 0.0041 | 0.04594 | 61 | 1.06465 | 0.1383 | 1.01508 | 0.0950 | 0.13632 |
| 22 | 0.38397 | 0.01837 | 0.38162 | 0.0047 | 0.04814 | 62 | 1.08210 | 0.14283 | 1.03008 | 0.0996 | 0.13866 |
| 23 | 0.40143 | 0.02008 | 0.39874 | 0.0053 | 0.05035 | 63 | 1.09956 | 0.14736 | 1.04500 | 0.104 | 0.14101 |
| 24 | 0.41888 | 0.02185 | 0.41582 | 0.0061 | 0.05255 | 64 | 1.11701 | 0.15195 | 1.05984 | 0.1091 | 0.14337 |
| 25 | 0.43633 | 0.02370 | 0.43288 | 0.0069 | 0.05476 | 65 | 1.13446 | 0.15661 | 1.07460 | 0.1141 | 0.145 |
| 26 | 0.45379 | 0.02563 | 0.44990 | 0.0077 | 0.05697 | 66 | 1.15192 | 0.16133 | 1.08928 | 0.1192 | 0.14811 |
| 27 | 0.47124 | 0.02763 | 0.46689 | 0.0086 | 0.05918 | 67 | 1.16937 | 0.16611 | 1.1038 | 0.124 | 0.1504 |
| 28 | 0.48869 | 0.02970 | 0.48384 | 0.0096 | 0.06139 | 68 | 1.18682 | 0.17096 | 1.1183 | 0.1298 | 0.15287 |
| 29 | 0.50615 | 0.03185 | 0.50076 | 0.0107 | 0.06361 | 69 | 1.20428 | 0.17587 | 1.1328 | 0.135 | 0.15525 |
| 30 | 0.52360 | 0.03407 | 0.5176 | 0.011 | 0.06583 | 70 | 1.22173 | 0.1808 | 1.1471 | 0.14 | 0.1576 |
| 31 | 0.54105 | 0.03637 | 0.53448 | 0.0130 | 0.06805 | 71 | 1.23918 | 0.18588 | 1.16141 | 0.1468 | 0.16005 |
| 32 | 0.558 | 0.03874 | 0.55 | 0.0143 | 0.07027 | 72 | 1.2566 | 0.19 | 1.17557 | 0.1528 | 0.162 |
| 33 | 0.57596 | 0.04118 | 0.56803 | 0.0157 | 0.07250 | 73 | 1.27409 | 0.19614 | 1.18965 | 0.158 | 0.16488 |
| 34 | 0.59341 | 0.04370 | 0.58474 | 0.0 | 0.07473 | 74 | 1.291 | 0.201 | 1.2036 | 0.16 | 0.16 |
| 35 | 0.61087 | 0.04628 | 0.60141 | 0.0186 | 0.07696 | 75 | 1.30900 | 0.20665 | 1.21752 | 0.1715 | 0.16973 |
| 36 | 0.62832 | 0.04894 | 0.61803 | 0.020 | 0.07919 | 76 | 1.326 | 0.211 | 1.231 | 0.17 | 0.172 |
| 37 | 0.64577 | 0.05168 | 0.63461 | 0.0220 | 0.08143 | 77 | 1.34390 | 0.21739 | 1.24503 | 0.1848 | 0.1746 |
| 38 | 0.66323 | 0.05448 | 0.65114 | 0.0238 | 0.08367 | 78 | 1.36136 | 0.22285 | 1.2586 | 0.191 | 0.17706 |
| 39 | 0.68068 | 0.05736 | 0.6676 | 0.0257 | 0.08592 | 79 | 1.37881 | 0.22838 | 1.27216 | 0.1986 | 0.17952 |
| 40 | 0.69813 | 0.06031 | 0.68404 | 0.0277 | 0.08816 | 80 | 1.39626 | 0.23396 | 1.28558 | 0.2057 | 0.18199 |

Segments of Circles for Radius =1 (English or metric units)

| $\begin{gathered} \theta, \\ \text { Deg. } \end{gathered}$ | $l$ | $h$ | $c$ | Area A | $h / c$ | $\begin{gathered} \theta, \\ \text { Deg. } \end{gathered}$ | $l$ | $h$ | c | Area A | $h / \mathrm{c}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 81 | 1.41372 | 0.23959 | 1.29890 | 0.2130 | 0.18446 | 131 | 2.28638 | 0.58531 | 1.81992 | 0.7658 | 0.32161 |
| 82 | 1.43117 | 0.24529 | 1.31212 | 0.2205 | 0.18694 | 132 | 2.30383 | 0.59326 | 1.82709 | 0.7803 | 0.32470 |
| 83 | 1.44862 | 0.25104 | 1.32524 | 0.2280 | 0.18943 | 133 | 2.32129 | 0.60125 | 1.83412 | 0.7950 | 0.32781 |
| 84 | 1.46608 | 0.25686 | 1.33826 | 0.2358 | 0.19193 | 134 | 2.33874 | 0.60927 | 1.84101 | 0.8097 | 0.33094 |
| 85 | 1.48353 | 0.26272 | 1.35118 | 0.2437 | 0.19444 | 135 | 2.35619 | 0.61732 | 1.84776 | 0.8245 | 0.33409 |
| 86 | 1.50098 | 0.26865 | 1.36400 | 0.2517 | 0.19696 | 136 | 2.37365 | 0.62539 | 1.85437 | 0.8395 | 0.33725 |
| 87 | 1.51844 | 0.27463 | 1.37671 | 0.2599 | 0.19948 | 137 | 2.39110 | 0.63350 | 1.86084 | 0.8546 | 0.34044 |
| 88 | 1.53589 | 0.28066 | 1.38932 | 0.2682 | 0.20201 | 138 | 2.40855 | 0.64163 | 1.86716 | 0.8697 | 0.34364 |
| 89 | 1.55334 | 0.28675 | 1.40182 | 0.2767 | 0.20456 | 139 | 2.42601 | 0.64979 | 1.87334 | 0.8850 | 0.34686 |
| 90 | 1.57080 | 0.29289 | 1.41421 | 0.2854 | 0.20711 | 140 | 2.44346 | 0.65798 | 1.87939 | 0.9003 | 0.35010 |
| 91 | 1.58825 | 0.29909 | 1.42650 | 0.2942 | 0.20967 | 141 | 2.46091 | 0.66619 | 1.88528 | 0.9158 | 0.35337 |
| 92 | 1.60570 | 0.30534 | 1.43868 | 0.3032 | 0.21224 | 142 | 2.47837 | 0.67443 | 1.89104 | 0.9314 | 0.35665 |
| 93 | 1.62316 | 0.31165 | 1.45075 | 0.3123 | 0.21482 | 143 | 2.49582 | 0.68270 | 1.89665 | 0.9470 | 0.35995 |
| 94 | 1.64061 | 0.31800 | 1.46271 | 0.3215 | 0.21741 | 144 | 2.51327 | 0.69098 | 1.90211 | 0.9627 | 0.36327 |
| 95 | 1.65806 | 0.32441 | 1.47455 | 0.330 | 0.2 | 145 | 2.53073 | 0.69929 | 1.90743 | 0.9786 | 0.36662 |
| 96 | 1.67552 | 0.33087 | 1.48629 | 0.3405 | 0.22261 | 146 | 2.54818 | 0.70763 | 1.91261 | 0.9945 | 0.36998 |
| 97 | 1.69297 | 0.33738 | 1.49791 | 0.3502 | 0.22523 | 147 | 2.56563 | 0.71598 | 1.91764 | 1.0105 | 0.37337 |
| 98 | 1.71042 | 0.34394 | 1.50942 | 0.3601 | 0.22786 | 148 | 2.58309 | 0.72436 | 1.92252 | 1.0266 | 0.37678 |
| 99 | 1.72788 | 0.35055 | 1.52081 | 0.3701 | 0.23050 | 149 | 2.60054 | 0.73276 | 1.92726 | 1.0428 | 0.38021 |
| 100 | 1.74533 | 0.35721 | 1.53209 | 0.3803 | 0.23315 | 150 | 2.61799 | 0.74118 | 1.93185 | 1.0590 | 0.38366 |
| 101 | 1.76278 | 0.36392 | 1.54325 | 0.3906 | 0.23582 | 151 | 2.63545 | 0.74962 | 1.93630 | 1.0753 | 0.38714 |
| 102 | 1.78024 | 0.37068 | 1.55429 | 0.401 | 0.23849 | 152 | 2.65290 | 0.75808 | 1.94059 | 1.0917 | 0.39064 |
| 103 | 1.79769 | 0.37749 | 1.56522 | 0.4117 | 0.24117 | 153 | 2.67035 | 0.76655 | 1.94474 | 1.1082 | 0.39417 |
| 104 | 1.81514 | 0.3843 | 1.57602 | 0.422 | 0.2438 | 154 | 2.68781 | 0.77505 | 1.94874 | 1.1247 | 0.39772 |
| 105 | 1.83260 | 0.39124 | 1.58671 | 0.4333 | 0.24657 | 155 | 2.70526 | 0.78356 | 1.95259 | 1.1413 | 0.40129 |
| 106 | 1.85005 | 0.39818 | 1.59727 | 0.444 | 0.24929 | 156 | 2.7227 | 0.79209 | 1.95630 | 1.1580 | 0.40489 |
| 107 | 1.86750 | 0.40518 | 1.60771 | 0.4556 | 0.25202 | 157 | 2.74017 | 0.80063 | 1.95985 | 1.1747 | 0.40852 |
| 108 | 1.88496 | 0.4122 | 1.61803 | 0.466 | 0.25476 | 158 | 2.75762 | 0.80919 | 1.96325 | 1.1915 | 0.41217 |
| 109 | 1.90241 | 0.41930 | 1.62823 | 0.4784 | 0.25752 | 159 | 2.77507 | 0.81776 | 1.96651 | 1.2084 | 0.41585 |
| 110 | 1.91986 | 0.42642 | 1.63830 | 0.490 | 0.26028 | 160 | 2.79253 | 0.82635 | 1.96962 | 1.2253 | 0.41955 |
| 111 | 1.93732 | 0.43359 | 1.64825 | 0.5019 | 0.26306 | 161 | 2.80998 | 0.83495 | 1.97257 | 1.2422 | 0.42328 |
| 112 | 1.95477 | 0.44081 | 1.65808 | 0.5138 | 0.26585 | 162 | 2.82743 | 0.84357 | 1.97538 | 1.2592 | 0.42704 |
| 113 | 1.97222 | 0.44806 | 1.66777 | 0.5259 | 0.26866 | 163 | 2.84489 | 0.85219 | 1.97803 | 1.2763 | 0.43083 |
| 11 | 1.98968 | 0.45536 | 1.67734 | 0.5381 | 0.27148 | 164 | 2.86234 | 0.86083 | 1.98054 | 1.2934 | 0.43464 |
| 115 | 2.00713 | 0.46270 | 1.68678 | 0.5504 | 0.27431 | 165 | 2.87979 | 0.86947 | 1.98289 | 1.3105 | 0.43849 |
| 116 | 2.02458 | 0.47008 | 1.69610 | 0.5629 | 0.27715 | 166 | 2.89725 | 0.87813 | 1.98509 | 1.3277 | 0.44236 |
| 117 | 2.04204 | 0.47750 | 1.70528 | 0.5755 | 0.28001 | 167 | 2.91470 | 0.88680 | 1.98714 | 1.3449 | 0.44627 |
| 118 | 2.05949 | 0.48496 | 1.71433 | 0.5883 | 0.28289 | 168 | 2.93215 | 0.89547 | 1.98904 | 1.3621 | 0.45020 |
| 119 | 2.07694 | 0.49246 | 1.72326 | 0.6012 | 0.28577 | 169 | 2.94961 | 0.90415 | 1.99079 | 1.3794 | 0.45417 |
| 120 | 2.09440 | 0.50000 | 1.73205 | 0.6142 | 0.28868 | 170 | 2.96706 | 0.91284 | 1.99239 | 1.3967 | 0.45817 |
| 121 | 2.11185 | 0.50758 | 1.74071 | 0.6273 | 0.29159 | 171 | 2.98451 | 0.92154 | 1.99383 | 1.4140 | 0.46220 |
| 122 | 2.12930 | 0.51519 | 1.74924 | 0.6406 | 0.29452 | 172 | 3.00197 | 0.93024 | 1.99513 | 1.4314 | 0.46626 |
| 123 | 2.14675 | 0.52284 | 1.75763 | 0.6540 | 0.29747 | 173 | 3.01942 | 0.93895 | 1.99627 | 1.4488 | 0.47035 |
| 124 | 2.16421 | 0.53053 | 1.76590 | 0.6676 | 0.30043 | 174 | 3.03687 | 0.94766 | 1.99726 | 1.4662 | 0.47448 |
| 125 | 2.18166 | 0.53825 | 1.77402 | 0.6813 | 0.30341 | 175 | 3.05433 | 0.95638 | 1.99810 | 1.4836 | 0.47865 |
| 126 | 2.19911 | 0.54601 | 1.78201 | 0.6950 | 0.30640 | 176 | 3.07178 | 0.96510 | 1.99878 | 1.5010 | 0.48284 |
| 127 | 2.21657 | 0.55380 | 1.78987 | 0.7090 | 0.30941 | 177 | 3.08923 | 0.97382 | 1.99931 | 1.5184 | 0.48708 |
| 128 | 2.23402 | 0.56163 | 1.79759 | 0.7230 | 0.31243 | 178 | 3.10669 | 0.98255 | 1.99970 | 1.5359 | 0.49135 |
| 129 | 2.25147 | 0.56949 | 1.80517 | 0.7372 | 0.31548 | 179 | 3.12414 | 0.99127 | 1.99992 | 1.5533 | 0.49566 |
| 130 | 2.26893 | 0.57738 | 1.81262 | 0.7514 | 0.31854 | 180 | 3.14159 | 1.00000 | 2.00000 | 1.5708 | 0.50000 |

## Distance Across Corners of Squares and Hexagons (English and metric units)

|  | D <br> E | ? |  |  | A desired value not given directly in the table can be obtained by the simple addition of two or more values taken directly from the table. Further values can be obtained by shifting the decimal point. <br> Example 1: Find $D$ when $d=25 / 16$ inches. From the table, $2=2.3094$, and $5 / 16$ $=0.3608$. Therefore, $\mathrm{D}=2.3094+0.3608=2.6702$ inches. <br> Example 2: Find $E$ when $d=20.25$ millimeters. From the table, $20=$ $28.2843 ; 0.2=0.2828$; and $0.05=0.0707$ (obtained by shifting the decimal point one place to the left at $d=0.5$ ). Thus, $E=28.2843+0.2828+0.0707=$ 28.6378 millimeters. |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $d$ | D | E | $d$ | D | E | $d$ | D | E | $d$ | D | E |
| 1/32 | 0.0361 | 0.0442 | 0.9 | 1.0392 | 1.2728 | 32 | 36.9504 | 45.2548 | 67 | 77.3650 | 94.7523 |
| 1/16 | 0.0722 | 0.0884 | 29/32 | 1.0464 | 1.2816 | 33 | 38.1051 | 46.6691 | 68 | 78.5197 | 96.1666 |
| $3 / 32$ | 0.1083 | 0.1326 | 15/16 | 1.0825 | 1.3258 | 34 | 39.2598 | 48.0833 | 69 | 79.6744 | 97.5808 |
| 0.1 | 0.1155 | 0.1414 | $31 / 32$ | 1.1186 | 1.3700 | 35 | 40.4145 | 49.4975 | 70 | 80.8291 | 98.9950 |
| 1/8 | 0.1443 | 0.1768 | 1.0 | 1.1547 | 1.4142 | 36 | 41.5692 | 50.9117 | 71 | 81.9838 | 100.409 |
| 5/32 | 0.1804 | 0.2210 | 2.0 | 2.3094 | 2.8284 | 37 | 42.7239 | 52.3259 | 72 | 83.1385 | 101.823 |
| 3/16 | 0.2165 | 0.2652 | 3.0 | 3.4641 | 4.2426 | 38 | 43.8786 | 53.7401 | 73 | 84.2932 | 103.238 |
| 0.2 | 0.2309 | 0.2828 | 4.0 | 4.6188 | 5.6569 | 39 | 45.0333 | 55.1543 | 74 | 85.4479 | 104.652 |
| 7/32 | 0.2526 | 0.3094 | 5.0 | 5.7735 | 7.0711 | 40 | 46.1880 | 56.5686 | 75 | 86.6026 | 106.066 |
| 1/4 | 0.2887 | 0.3536 | 6.0 | 6.9282 | 8.4853 | 41 | 47.3427 | 57.9828 | 76 | 87.7573 | 107.480 |
| $9 / 32$ | 0.3248 | 0.3977 | 7.0 | 8.0829 | 9.8995 | 42 | 48.4974 | 59.3970 | 77 | 88.9120 | 108.894 |
| 0.3 | 0.3464 | 0.4243 | 8.0 | 9.2376 | 11.3137 | 43 | 49.6521 | 60.8112 | 78 | 90.0667 | 110.309 |
| 5/16 | 0.3608 | 0.4419 | 9.0 | 10.3923 | 12.7279 | 44 | 50.8068 | 62.2254 | 79 | 91.2214 | 111.723 |
| $11 / 32$ | 0.3969 | 0.4861 | 10 | 11.5470 | 14.1421 | 45 | 51.9615 | 63.6396 | 80 | 92.3761 | 113.137 |
| 3/8 | 0.4330 | 0.5303 | 11 | 12.7017 | 15.5564 | 46 | 53.1162 | 65.0538 | 81 | 93.5308 | 114.551 |
| 0.4 | 0.4619 | 0.5657 | 12 | 13.8564 | 16.9706 | 47 | 54.2709 | 66.4681 | 82 | 94.6855 | 115.966 |
| $13 / 32$ | 0.4691 | 0.5745 | 13 | 15.0111 | 18.3848 | 48 | 55.4256 | 67.8823 | 83 | 95.8402 | 117.380 |
| 7/16 | 0.5052 | 0.6187 | 14 | 16.1658 | 19.7990 | 49 | 56.5803 | 69.2965 | 84 | 96.9949 | 118.794 |
| 15/32 | 0.5413 | 0.6629 | 15 | 17.3205 | 21.2132 | 50 | 57.7351 | 70.7107 | 85 | 98.1496 | 120.208 |
| 0.5 | 0.5774 | 0.7071 | 16 | 18.4752 | 22.6274 | 51 | 58.8898 | 72.1249 | 86 | 99.3043 | 121.622 |
| 17/32 | 0.6134 | 0.7513 | 17 | 19.6299 | 24.0416 | 52 | 60.0445 | 73.5391 | 87 | 100.459 | 123.037 |
| 9/16 | 0.6495 | 0.7955 | 18 | 20.7846 | 25.4559 | 53 | 61.1992 | 74.9533 | 88 | 101.614 | 124.451 |
| 19/32 | 0.6856 | 0.8397 | 19 | 21.9393 | 26.8701 | 54 | 62.3539 | 76.3676 | 89 | 102.768 | 125.865 |
| 0.6 | 0.6928 | 0.8485 | 20 | 23.0940 | 28.2843 | 55 | 63.5086 | 77.7818 | 90 | 103.923 | 127.279 |
| 5/8 | 0.7217 | 0.8839 | 21 | 24.2487 | 29.6985 | 56 | 64.6633 | 79.1960 | 91 | 105.078 | 128.693 |
| $21 / 32$ | 0.7578 | 0.9281 | 22 | 25.4034 | 31.1127 | 57 | 65.8180 | 80.6102 | 92 | 106.232 | 130.108 |
| 11/16 | 0.7939 | 0.9723 | 23 | 26.5581 | 32.5269 | 58 | 66.9727 | 82.0244 | 93 | 107.387 | 131.522 |
| 0.7 | 0.8083 | 0.9899 | 24 | 27.7128 | 33.9411 | 59 | 68.1274 | 83.4386 | 94 | 108.542 | 132.936 |
| 23/32 | 0.8299 | 1.0165 | 25 | 28.8675 | 35.3554 | 60 | 69.2821 | 84.8528 | 95 | 109.697 | 134.350 |
| 3/4 | 0.8660 | 1.0607 | 26 | 30.0222 | 36.7696 | 61 | 70.4368 | 86.2671 | 96 | 110.851 | 135.765 |
| 25/32 | 0.9021 | 1.1049 | 27 | 31.1769 | 38.1838 | 62 | 71.5915 | 87.6813 | 97 | 112.006 | 137.179 |
| 0.8 | 0.9238 | 1.1314 | 28 | 32.3316 | 39.5980 | 63 | 72.7462 | 89.0955 | 98 | 113.161 | 138.593 |
| 13/16 | 0.9382 | 1.1490 | 29 | 33.4863 | 41.0122 | 64 | 73.9009 | 90.5097 | 99 | 114.315 | 140.007 |
| $27 / 32$ | 0.9743 | 1.1932 | 30 | 34.6410 | 42.4264 | 65 | 75.0556 | 91.9239 | 100 | 115.470 | 141.421 |
| 7/8 | 1.0104 | 1.2374 | 31 | 35.7957 | 43.8406 | 66 | 76.2103 | 93.3381 | $\ldots$ | $\ldots$ | $\ldots$ |

## SOLUTION OF TRIANGLES

Any figure bounded by three straight lines is called a triangle. Any one of the three lines may be called the base, and the line drawn from the angle opposite the base at right angles to it is called the height or altitude of the triangle.
If all three sides of a triangle are of equal length, the triangle is called equilateral. Each of the three angles in an equilateral triangle equals 60 degrees. If two sides are of equal length, the triangle is an isosceles triangle. If one angle is a right or 90 -degree angle, the triangle is a right or right-angled triangle. The side opposite the right angle is called the hypotenuse.
If all the angles are less than 90 degrees, the triangle is called an acute or acute-angled triangle. If one of the angles is larger than 90 degrees, the triangle is called an obtuseangled triangle. Both acute and obtuse-angled triangles are known under the common name of oblique-angled triangles. The sum of the three angles in every triangle is 180 degrees.
The sides and angles of any triangle that are not known can be found when: 1) all the three sides; 2) two sides and one angle; and 3) one side and two angles are given.
In other words, if a triangle is considered as consisting of six parts, three angles and three sides, the unknown parts can be determined when any three parts are given, provided at least one of the given parts is a side.

## Functions of Angles

For every right triangle, a set of six ratios is defined; each is the length of one side of the triangle divided by the length of another side. The six ratios are the trigonometric (trig) functions sine, cosine, tangent, cosecant, secant, and cotangent (abbreviated sin, cos, tan, csc , sec, and cot). Trig functions are usually expressed in terms of an angle in degree or radian measure, as in $\cos 60^{\circ}=0.5$. "Arc" in front of a trig function name, as in arcsin or $\arccos$, means find the angle whose function value is given. For example, $\arcsin 0.5=30^{\circ}$ means that $30^{\circ}$ is the angle whose $\sin$ is equal to 0.5 . Electronic calculators frequently use $\sin ^{-1}, \cos ^{-1}$, and $\tan ^{-1}$ to represent the arc functions.

$$
\text { Example: } \tan 53.1^{\circ}=1.332 ; \arctan 1.332=\tan ^{-1} 1.332=53.1^{\circ}=53^{\circ} 6^{\prime}
$$

The sine of an angle equals the opposite side divided by the hypotenuse. Hence, $\sin B=b$ $\div c$, and $\sin A=a \div c$.


The cosine of an angle equals the adjacent side divided by the hypotenuse. Hence, $\cos B=a \div c$, and $\cos A=b \div c$.
The tangent of an angle equals the opposite side divided by the adjacent side. Hence, $\tan B=b \div a$, and $\tan A=a \div b$.
The cotangent of an angle equals the adjacent side divided by the opposite side. Hence, $\cot B=a \div b$, and $\cot A=b \div a$.
The secant of an angle equals the hypotenuse divided by the adjacent side. Hence, sec $B$ $=c \div a$, and $\sec A=c \div b$.
The cosecant of an angle equals the hypotenuse divided by the opposite side. Hence, csc $B=c \div b$, and $\csc A=c \div a$.
It should be noted that the functions of the angles can be found in this manner only when the triangle is right-angled.
If in a right-angled triangle (see preceding illustration), the lengths of the three sides are represented by $a, b$, and $c$, and the angles opposite each of these sides by $A, B$, and $C$, then the side $c$ opposite the right angle is the hypotenuse; side $b$ is called the side adjacent to angle $A$ and is also the side opposite to angle $B$; side $a$ is the side adjacent to angle $B$ and the
side opposite to angle $A$. The meanings of the various functions of angles can be explained with the aid of a right-angled triangle. Note that the cosecant, secant, and cotangent are the reciprocals of, respectively, the sine, cosine, and tangent.
The following relation exists between the angular functions of the two acute angles in a right-angled triangle: The sine of angle $B$ equals the cosine of angle $A$; the tangent of angle $B$ equals the cotangent of angle $A$, and vice versa. The sum of the two acute angles in a right-angled triangle always equals 90 degrees; hence, when one angle is known, the other can easily be found. When any two angles together make 90 degrees, one is called the complement of the other, and the sine of the one angle equals the cosine of the other, and the tangent of the one equals the cotangent of the other.
The Law of Sines.-In any triangle, any side is to the sine of the angle opposite that side as any other side is to the sine of the angle opposite that side. If $a, b$, and $c$ are the sides, and $A, B$, and $C$ their opposite angles, respectively, then:

$$
\begin{array}{rlrlrl}
\frac{a}{\sin A} & =\frac{b}{\sin B}=\frac{c}{\sin C}, & & \text { so that: } \\
a & =\frac{b \sin A}{\sin B} & \text { or } & & a=\frac{c \sin A}{\sin C} \\
b & =\frac{a \sin B}{\sin A} & \text { or } & b & =\frac{c \sin B}{\sin C} \\
c & =\frac{a \sin C}{\sin A} & \text { or } & c & =\frac{b \sin C}{\sin B}
\end{array}
$$

The Law of Cosines.-In any triangle, the square of any side is equal to the sum of the squares of the other two sides minus twice their product times the cosine of the included angle; or if $a, b$ and $c$ are the sides and $A, B$, and $C$ are the opposite angles, respectively, then:

$$
\begin{aligned}
& a^{2}=b^{2}+c^{2}-2 b c \cos A \\
& b^{2}=a^{2}+c^{2}-2 a c \cos B \\
& c^{2}=a^{2}+b^{2}-2 a b \cos C
\end{aligned}
$$

These two laws, together with the proposition that the sum of the three angles equals 180 degrees, are the basis of all formulas relating to the solution of triangles.
Formulas for the solution of right-angled and oblique-angled triangles, arranged in tabular form, are given on the following pages.
Signs of Trigonometric Functions.-The diagram, Signs of Trigonometric Functions, Fractions of $\pi$, and Degree-Radian Conversion on page 92, shows the proper sign ( + or ) for the trigonometric functions of angles in each of the four quadrants, 0 to 90,90 to 180 , 180 to 270 , and 270 to 360 degrees. Thus, the cosine of an angle between 90 and 180 degrees is negative; the sine of the same angle is positive.
Trigonometric Identities.-Trigonometric identities are formulas that show the relationship between different trigonometric functions. They may be used to change the form of some trigonometric expressions to simplify calculations. For example, if a formula has a term, $2 \sin A \cos A$, the equivalent but simpler term $\sin 2 A$ may be substituted. The identities that follow may themselves be combined or rearranged in various ways to form new identities.

## Basic

$$
\tan A=\frac{\sin A}{\cos A}=\frac{1}{\cot A} \quad \sec A=\frac{1}{\cos A} \quad \csc A=\frac{1}{\sin A}
$$

## Negative Angle

$$
\sin (-A)=-\sin A \quad \cos (-A)=\cos A \quad \tan (-A)=-\tan A
$$

## Pythagorean

$$
\sin ^{2} A+\cos ^{2} A=1 \quad 1+\tan ^{2} A=\sec ^{2} A \quad 1+\cot ^{2} A=\csc ^{2} A
$$

## Sum and Difference of Angles

$$
\begin{aligned}
& \tan (A+B)=\frac{\tan A+\tan B}{1-\tan A \tan B} \quad \tan (A-B)=\frac{\tan A-\tan B}{1+\tan A \tan B} \\
& \cot (A+B)=\frac{\cot A \cot B-1}{\cot B+\cot A} \quad \cot (A-B)=\frac{\cot A \cot B+1}{\cot B-\cot A} \\
& \sin (A+B)=\sin A \cos B+\cos A \sin B \quad \sin (A-B)=\sin A \cos B-\cos A \sin B \\
& \cos (A+B)=\cos A \cos B-\sin A \sin B \quad \cos (A-B)=\cos A \cos B-\sin A \sin B
\end{aligned}
$$

## Double-Angle

$$
\begin{aligned}
& \cos 2 A=\cos ^{2} A-\sin ^{2} A=2 \cos ^{2} A-1=1-2 \sin ^{2} A \\
& \sin 2 A=2 \sin A \cos A \quad \tan 2 A=\frac{2 \tan A}{1-\tan ^{2} A}=\frac{2}{\cot A-\tan A}
\end{aligned}
$$

## Half-Angle

$$
\begin{aligned}
& \sin 1 / 2 A=\sqrt{1 / 2(1-\cos A)} \quad \cos 1 / 2 A=\sqrt{1 / 2(1+\cos A)} \\
& \tan 1 / 2 A=\sqrt{\frac{1-\cos A}{1+\cos A}}=\frac{1-\cos A}{\sin A}=\frac{\sin A}{1+\cos A}
\end{aligned}
$$

## Product-to-Sum

$$
\begin{aligned}
& \sin A \cos B=\frac{1}{2}[\sin (A+B)+\sin (A-B)] \\
& \cos A \cos B=1 / 2[\cos (A+B)+\cos (A-B)] \\
& \sin A \sin B=1 / 2[\cos (A-B)-\cos (A+B)] \\
& \tan A \tan B=\frac{\tan A+\tan B}{\cot A+\cot B}
\end{aligned}
$$

## Sum and Difference of Functions

$$
\begin{aligned}
& \sin A+\sin B=2\left[\sin \frac{1}{2}(A+B) \cos 1 / 2(A-B)\right] \\
& \sin A-\sin B=2\left[\sin 1 / 2(A-B) \cos \frac{1}{2}(A+B)\right] \\
& \cos A+\cos B=2[\cos 1 / 2(A+B) \cos 1 / 2(A-B)] \\
& \cos A-\cos B=-2\left[\cos \frac{1}{2}(A+B) \cos 1 / 2(A-B)\right] \\
& \tan A+\tan B=\frac{\sin (A+B)}{\cos A \cos B} \quad \tan A-\tan B=\frac{\sin (A-B)}{\cos A \cos B} \\
& \cot A+\cot B=\frac{\sin (B+A)}{\sin A \sin B} \quad \cot A-\cot B=\frac{\sin (B-A)}{\sin A \sin B}
\end{aligned}
$$

## Solution of Right-Angled Triangles

|  | As shown in the illustration, the sides of the right- <br> angled triangle are designated $a$ and $b$ and the hypote- <br> nuse, $c$ The angles opposite each of these sides are des- <br> ignated $A$ and $B$, respectively. |
| :--- | :--- | :--- | :--- |
| Angle $C$, opposite the hypotenuse $c$ is the right angle, |  |
| and is therefore always one of the known quantities. |  |, | Formulas for Sides and Angles to be Found |
| :--- |

Examples of the Solution of Right-Angled Triangles (English and metric units)

| Hypotenuse and one angle known |  |
| :---: | :---: |
| Hypotenuse and one side known | $\begin{aligned} & \begin{aligned} c=25 \text { centimeters; } a & =20 \text { centimeters. } \\ b=\sqrt{c^{2}-a^{2}} & =\sqrt{25^{2}-20^{2}}=\sqrt{625-400} \\ & =\sqrt{225}=15 \text { centimeters } \end{aligned} \\ & \qquad \begin{aligned} \sin A & =\frac{a}{c}=\frac{20}{25}=0.8 \end{aligned} \\ & \text { Hence, } \quad \begin{aligned} A & =53^{\circ} 8^{\prime} \\ B & =90^{\circ}-A=90^{\circ}-53^{\circ} 8^{\prime}=36^{\circ} 52^{\prime} \end{aligned} \end{aligned}$ |
| Two sides known | $a=36$ inches; $b=15$ inches. $\begin{aligned} c=\sqrt{a^{2}+b^{2}} & =\sqrt{36^{2}+15^{2}}=\sqrt{1296+225} \\ & =\sqrt{1521}=39 \text { inches } \\ \tan A & =\frac{a}{b}=\frac{36}{15}=2.4 \end{aligned}$ <br> Hence, $\begin{aligned} & A=67^{\circ} 23^{\prime} \\ & B=90^{\circ}-A=90^{\circ}-67^{\circ} 23^{\prime}=22^{\circ} 37^{\prime} \end{aligned}$ |
| One side and one angle known | $\begin{aligned} & a=12 \text { meters; } A=65^{\circ} . \\ & \begin{aligned} c & =\frac{a}{\sin A}=\frac{12}{\sin 65^{\circ}}=\frac{12}{0.90631}=13.2405 \text { meters } \\ b & =a \times \cot A \end{aligned}=12 \times \cot 65^{\circ}=12 \times 0.46631 \\ & \\ & =5.5957 \text { meters } \\ & B \end{aligned} \quad \begin{aligned} & 90^{\circ}-A=90^{\circ}-65^{\circ}=25^{\circ} \end{aligned}$ |

## Solution of Oblique-Angled Triangles

| (KNOWN) <br> One side and one angle known | Call the known side $a$, the angle opposite it $A$, and the other known angle $B$. Then: <br> $C=180^{\circ}-(A+B)$; or if angles $B$ and $C$ are given, but not $A$, then $A=180^{\circ}-(B+C)$. $\begin{gathered} C=180^{\circ}-(A+B) \\ b=\frac{a \times \sin B}{\sin A} \quad c=\frac{a \times \sin C}{\sin A} \\ \text { Area }=\frac{a \times b \times \sin C}{2} \end{gathered}$ |
| :---: | :---: |
| Two sides and the angle between them known | Call the known sides $a$ and $b$, and the known angle between them $C$. Then: $\begin{gathered} \tan A=\frac{a \times \sin C}{b-(a \times \cos C)} \\ B=180^{\circ}-(A+C) \quad c=\frac{a \times \sin C}{\sin A} \end{gathered}$ <br> Side $c$ may also be found directly as below: $\begin{gathered} c=\sqrt{a^{2}+b^{2}-(2 a b \times \cos C)} \\ \text { Area }=\frac{a \times b \times \sin C}{2} \end{gathered}$ |
| Two sides and the angle opposite one of the sides known | Call the known angle $A$, the side opposite it $a$, and the other known side $b$. Then: $\begin{aligned} \sin B & =\frac{b \times \sin A}{a} & C & =180^{\circ}-(A+B) \\ c & =\frac{a \times \sin C}{\sin A} & \text { Area } & =\frac{a \times b \times \sin C}{2} \end{aligned}$ <br> If, in the above, angle $B>$ angle $A$ but $<90^{\circ}$, then a second solution $B_{2}, C_{2}, c_{2}$ exists for which: $B_{2}=180^{\circ}-B ; C_{2}=180^{\circ}$ $-\left(A+B_{2}\right) ; c_{2}=\left(a \times \sin C_{2}\right) \div \sin A$; area $=\left(a \times b \times \sin C_{2}\right) \div$ 2. If $a \geq b$, then the first solution only exists. If $a<b \times \sin A$, then no solution exists. |
|  | Call the sides $a, b$, and $c$, and the angles opposite them, $A, B$, and $C$. Then: $\begin{aligned} \cos A & =\frac{b^{2}+c^{2}-a^{2}}{2 b c} & & \sin B \end{aligned}=\frac{b \times \sin A}{a}, ~ A r e a ~=\frac{a \times b \times \sin }{2}$ |

Examples of the Solution of Oblique-Angled Triangles (English and metric units)

| Side and angles known: | $\begin{aligned} a & =5 \text { centimeters; } A=80^{\circ} ; B=62^{\circ} \\ C & =180^{\circ}-\left(80^{\circ}+62^{\circ}\right)=180^{\circ}-142^{\circ}=38^{\circ} \\ b & =\frac{a \times \sin B}{\sin A}=\frac{5 \times \sin 62^{\circ}}{\sin 80^{\circ}}=\frac{5 \times 0.88295}{0.98481}=4.483 \end{aligned}$ <br> centimeters $c=\frac{a \times \sin C}{\sin A}=\frac{5 \times \sin 38^{\circ}}{\sin 80^{\circ}}=\frac{5 \times 0.61566}{0.98481}=3.126$ <br> centimeters |
| :---: | :---: |
| Sides and angle known: | $a=9 \text { inches; } b=8 \text { inches; } C=35^{\circ} \text {. }$ $\begin{aligned} \tan A & =\frac{a \times \sin C}{b-(a \times \cos C)}=\frac{9 \times \sin 35^{\circ}}{8-\left(9 \times \cos 35^{\circ}\right)} \\ & =\frac{9 \times 0.57358}{8-(9 \times 0.81915)}=\frac{5.16222}{0.62765}=8.22466 \end{aligned}$ <br> Hence, $A=83^{\circ} 4^{\prime}$ $\begin{aligned} B & =180^{\circ}-(A+C)=180^{\circ}-118^{\circ} 4^{\prime}=61^{\circ} \\ c & =\frac{a \times \sin C}{\sin A}=\frac{9 \times 0.57358}{0.99269}=5.2 \text { inches } \end{aligned}$ |
| Sides and angle known: | $a=20$ centimeters; $b=17$ centimeters; $A=61^{\circ}$. $\begin{aligned} \sin B & =\frac{b \times \sin A}{a}=\frac{17 \times \sin 61^{\circ}}{20} \\ & =\frac{17 \times 0.87462}{20}=0.74343 \end{aligned}$ <br> Hence, $B=48^{\circ} 1^{\prime}$ $\begin{aligned} C & =180^{\circ}-(A+B)=180^{\circ}-109^{\circ} 1^{\prime}=70^{\circ} 59^{\prime} \\ c & =\frac{a \times \sin C}{\sin A}=\frac{20 \times \sin 70^{\circ} 59^{\prime}}{\sin 61^{\circ}}=\frac{20 \times 0.94542}{0.87462} \\ & =21.62 \text { centimeters } \end{aligned}$ |
| Sides and angle known: | $a=8$ inches; $b=9$ inches; $c=10$ inches. $\begin{aligned} \cos A & =\frac{b^{2}+c^{2}-a^{2}}{2 b c}=\frac{9^{2}+10^{2}-8^{2}}{2 \times 9 \times 10} \\ & =\frac{81+100-64}{180}=\frac{117}{180}=0.65000 \end{aligned}$ <br> Hence, $\quad A=49^{\circ} 27^{\prime}$ $\sin B=\frac{b \times \sin A}{a}=\frac{9 \times 0.75984}{8}=0.85482$ <br> Hence, $\quad B=58^{\circ} 44^{\prime}$ $C=180^{\circ}-(A+B)=180^{\circ}-108^{\circ} 11^{\prime}=71^{\circ} 49^{\prime}$ |

Conversion Tables of Angular Measure.-The accompanying tables of degrees, minutes, and seconds into radians; radians into degrees, minutes, and seconds; radians into degrees and decimals of a degree; and minutes and seconds into decimals of a degree and vice versa facilitate the conversion of measurements.
Example: The Degrees, Minutes, and Seconds into Radians table is used to find the number of radians in 324 degrees, 25 minutes, 13 seconds as follows:

| 300 degrees | $=5.235988$ radians |
| ---: | :--- |
| 20 degrees | $=0.349066$ radian |
| 4 degrees | $=0.069813$ radian |
| 25 minutes | $=0.007272$ radian |
| $\frac{13 \text { seconds }}{324^{\circ} 25^{\prime} 13^{\prime \prime}}$ | $=\frac{0.000063 \text { radian }}{5.662202 \text { radians }}$ |

Example: The Radians into Degrees and Decimals of a Degree, and Radians into Degrees, Minutes and Seconds tables are used to find the number of decimal degrees or degrees, minutes and seconds in 0.734 radian as follows:

$$
\begin{array}{lll}
0.7 \text { radian }=40.1070 \text { degrees } & 0.7 \text { radian }=40^{\circ} 6^{\prime} 25^{\prime \prime} \\
0.03 \text { radian }=1.7189 \text { degrees } & 0.03 \text { radian }=1^{\circ} 43^{\prime} 8^{\prime \prime} \\
0.004 \text { radian }=0.2292 \text { degree } & 0.004 \text { radian }=0^{\circ} 10^{\circ} 13^{\prime} 45^{\prime \prime} \\
\overline{0.734} \text { radian }=\overline{42.0551} \text { degrees } & \overline{0.734} \text { radian }=41^{\circ} 62^{\prime} 78^{\prime \prime} \text { or } 42^{\circ} 3^{\prime} 18^{\prime \prime}
\end{array}
$$

Degrees, Minutes, and Seconds into Radians (Based on 180 degrees $=\pi$ radians)

| Degrees into Radians |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Deg. | Rad. | Deg. | Rad. | Deg. | Rad. | Deg. | Rad. | Deg. | Rad. | Deg. | Rad. |
| 1000 | 17.453293 | 100 | 1.745329 | 10 | 0.174533 | 1 | 0.017453 | 0.1 | 0.001745 | 0.01 | 0.000175 |
| 2000 | 34.906585 | 200 | 3.490659 | 20 | 0.349066 | 2 | 0.034907 | 0.2 | 0.003491 | 0.02 | 0.000349 |
| 3000 | 52.359878 | 300 | 5.235988 | 30 | 0.523599 | 3 | 0.052360 | 0.3 | 0.005236 | 0.03 | 0.000524 |
| 4000 | 69.813170 | 400 | 6.981317 | 40 | 0.698132 | 4 | 0.069813 | 0.4 | 0.006981 | 0.04 | 0.000698 |
| 5000 | 87.266463 | 500 | 8.726646 | 50 | 0.872665 | 5 | 0.087266 | 0.5 | 0.008727 | 0.05 | 0.000873 |
| 6000 | 104.719755 | 600 | 10.471976 | 60 | 1.047198 | 6 | 0.104720 | 0.6 | 0.010472 | 0.06 | 0.001047 |
| 7000 | 122.173048 | 700 | 12.217305 | 70 | 1.221730 | 7 | 0.122173 | 0.7 | 0.012217 | 0.07 | 0.001222 |
| 8000 | 139.626340 | 800 | 13.962634 | 80 | 1.396263 | 8 | 0.139626 | 0.8 | 0.013963 | 0.08 | 0.001396 |
| 9000 | 157.079633 | 900 | 15.707963 | 90 | 1.570796 | 9 | 0.157080 | 0.9 | 0.015708 | 0.09 | 0.001571 |
| 10000 | 174.532925 | 1000 | 17.453293 | 100 | 1.745329 | 10 | 0.174533 | 1.0 | 0.017453 | 0.10 | 0.001745 |
| Minutes into Radians |  |  |  |  |  |  |  |  |  |  |  |
| Min. | Rad. | Min. | Rad. | Min. | Rad. | Min. | Rad. | Min. | Rad. | Min. | Rad. |
| 1 | 0.000291 | 11 | 0.003200 | 21 | 0.006109 | 31 | 0.009018 | 41 | 0.011926 | 51 | 0.014835 |
| 2 | 0.000582 | 12 | 0.003491 | 22 | 0.006400 | 32 | 0.009308 | 42 | 0.012217 | 52 | 0.015126 |
| 3 | 0.000873 | 13 | 0.003782 | 23 | 0.006690 | 33 | 0.009599 | 43 | 0.012508 | 53 | 0.015417 |
| 4 | 0.001164 | 14 | 0.004072 | 24 | 0.006981 | 34 | 0.009890 | 44 | 0.012799 | 54 | 0.015708 |
| 5 | 0.001454 | 15 | 0.004363 | 25 | 0.007272 | 35 | 0.010181 | 45 | 0.013090 | 55 | 0.015999 |
| 6 | 0.001745 | 16 | 0.004654 | 26 | 0.007563 | 36 | 0.010472 | 46 | 0.013381 | 56 | 0.016290 |
| 7 | 0.002036 | 17 | 0.004945 | 27 | 0.007854 | 37 | 0.010763 | 47 | 0.013672 | 57 | 0.016581 |
| 8 | 0.002327 | 18 | 0.005236 | 28 | 0.008145 | 38 | 0.011054 | 48 | 0.013963 | 58 | 0.016872 |
| 9 | 0.002618 | 19 | 0.005527 | 29 | 0.008436 | 39 | 0.011345 | 49 | 0.014254 | 59 | 0.017162 |
| 10 | 0.002909 | 20 | 0.005818 | 30 | 0.008727 | 40 | 0.011636 | 50 | 0.014544 | 60 | 0.017453 |
| Seconds into Radians |  |  |  |  |  |  |  |  |  |  |  |
| Sec. | Rad. | Sec. | Rad. | Sec. | Rad. | Sec. | Rad. | Sec. | Rad. | Sec. | Rad. |
| 1 | 0.000005 | 11 | 0.000053 | 21 | 0.000102 | 31 | 0.000150 | 41 | 0.000199 | 51 | 0.000247 |
| 2 | 0.000010 | 12 | 0.000058 | 22 | 0.000107 | 32 | 0.000155 | 42 | 0.000204 | 52 | 0.000252 |
| 3 | 0.000015 | 13 | 0.000063 | 23 | 0.000112 | 33 | 0.000160 | 43 | 0.000208 | 53 | 0.000257 |
| 4 | 0.000019 | 14 | 0.000068 | 24 | 0.000116 | 34 | 0.000165 | 44 | 0.000213 | 54 | 0.000262 |
| 5 | 0.000024 | 15 | 0.000073 | 25 | 0.000121 | 35 | 0.000170 | 45 | 0.000218 | 55 | 0.000267 |
| 6 | 0.000029 | 16 | 0.000078 | 26 | 0.000126 | 36 | 0.000175 | 46 | 0.000223 | 56 | 0.000271 |
| 7 | 0.000034 | 17 | 0.000082 | 27 | 0.000131 | 37 | 0.000179 | 47 | 0.000228 | 57 | 0.000276 |
| 8 | 0.000039 | 18 | 0.000087 | 28 | 0.000136 | 38 | 0.000184 | 48 | 0.000233 | 58 | 0.000281 |
| 9 | 0.000044 | 19 | 0.000092 | 29 | 0.000141 | 39 | 0.000189 | 49 | 0.000238 | 59 | 0.000286 |
| 10 | 0.000048 | 20 | 0.000097 | 30 | 0.000145 | 40 | 0.000194 | 50 | 0.000242 | 60 | 0.000291 |

## Radians into Degrees and Decimals of a Degree (Based on $\pi$ radians $=180$ degrees)

| Rad. | Deg. | Rad. | Deg. | Rad. | Deg. | Rad. | Deg. | Rad. | Deg. | Rad. | Deg. |
| :---: | ---: | :---: | ---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 572.9578 | 1 | 57.2958 | 0.1 | 5.7296 | 0.01 | 0.5730 | 0.001 | 0.0573 | 0.0001 | 0.0057 |
| 20 | 1145.9156 | 2 | 114.5916 | 0.2 | 11.4592 | 0.02 | 1.1459 | 0.002 | 0.1146 | 0.0002 | 0.0115 |
| 30 | 1718.8734 | 3 | 171.8873 | 0.3 | 17.1887 | 0.03 | 1.7189 | 0.003 | 0.1719 | 0.0003 | 0.0172 |
| 40 | 2291.8312 | 4 | 229.1831 | 0.4 | 22.9183 | 0.04 | 2.2918 | 0.004 | 0.2292 | 0.0004 | 0.0229 |
| 50 | 2864.7890 | 5 | 286.4789 | 0.5 | 28.6479 | 0.05 | 2.8648 | 0.005 | 0.2865 | 0.0005 | 0.0286 |
| 60 | 3437.7468 | 6 | 343.7747 | 0.6 | 34.3775 | 0.06 | 3.4377 | 0.006 | 0.3438 | 0.0006 | 0.0344 |
| 70 | 4010.7046 | 7 | 401.0705 | 0.7 | 40.1070 | 0.07 | 4.0107 | 0.007 | 0.4011 | 0.0007 | 0.0401 |
| 80 | 4583.6624 | 8 | 458.3662 | 0.8 | 45.8366 | 0.08 | 4.5837 | 0.008 | 0.4584 | 0.0008 | 0.0458 |
| 90 | 5156.6202 | 9 | 515.6620 | 0.9 | 51.5662 | 0.09 | 5.1566 | 0.009 | 0.5157 | 0.0009 | 0.0516 |
| 100 | 5729.5780 | 10 | 572.9578 | 1.0 | 57.2958 | 0.10 | 5.7296 | 0.010 | 0.5730 | 0.0010 | 0.0573 |

## Radians into Degrees, Minutes, and Seconds (Based on $\pi$ radians $=180$ degrees)

| Rad. | Angle | Rad. | Angle | Rad. | Angle | Rad. | Angle | Rad. | Angle | Rad. | Angle |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 572 ${ }^{\circ} 57^{\prime} 28^{\prime \prime}$ | 1 | $57^{\circ} 17^{\prime} 45^{\prime \prime}$ | 0.1 | $5^{\circ} 43^{\prime} 46^{\prime \prime}$ | 0.01 | $0^{\circ} 34^{\prime} 23^{\prime \prime}$ | 0.001 | $0^{\circ} 3^{\prime} 26^{\prime \prime}$ | 0.0001 | $0^{\circ} 0^{\prime} 21^{\prime \prime}$ |
| 20 | $1145^{\circ} 54^{\prime} 56^{\prime \prime}$ | 2 | $114^{\circ} 35^{\prime} 30^{\prime \prime}$ | 0.2 | $11^{\circ} 27^{\prime} 33^{\prime \prime}$ | 0.02 | $1^{\circ} 8^{\prime} 45^{\prime \prime}$ | 0.002 | $0^{\circ} 6^{\prime} 53^{\prime \prime}$ | 0.0002 | $0^{\circ} 0^{\prime} 41^{\prime \prime}$ |
| 30 | $1718^{\circ} 52^{\prime} 24^{\prime \prime}$ | 3 | $171^{\circ} 53^{\prime} 14^{\prime \prime}$ | 0.3 | $17^{\circ} 11^{\prime} 19^{\prime \prime}$ | 0.03 | $1^{\circ} 43^{\prime} 8^{\prime \prime}$ | 0.003 | $0^{\circ} 10^{\prime} 19^{\prime \prime}$ | 0.0003 | $0^{\circ} 1^{\prime} 2^{\prime \prime}$ |
| 40 | $2291^{\circ} 49^{\prime} 52^{\prime \prime}$ | 4 | $229^{\circ} 10^{\prime} 59^{\prime \prime}$ | 0.4 | $22^{\circ} 55^{\prime} 6^{\prime \prime}$ | 0.04 | $2^{\circ} 17^{\prime} 31^{\prime \prime}$ | 0.004 | $0^{\circ} 13^{\prime} 45^{\prime \prime}$ | 0.0004 | $0^{\circ} 1^{\prime} 23^{\prime \prime}$ |
| 50 | $2864^{\circ} 47^{\prime} 20^{\prime \prime}$ | 5 | $286^{\circ} 28^{\prime} 44^{\prime \prime}$ | 0.5 | $28^{\circ} 38^{\prime} 52^{\prime \prime}$ | 0.05 | $2^{\circ} 51^{\prime} 53^{\prime \prime}$ | 0.005 | $0^{\circ} 17^{\prime} 11^{\prime \prime}$ | 0.0005 | $0^{\circ} 1^{\prime} 43^{\prime \prime}$ |
| 60 | $3437^{\circ} 44^{\prime} 48^{\prime \prime}$ | 6 | $343^{\circ} 46^{\prime} 29^{\prime \prime}$ | 0.6 | $34^{\circ} 22^{\prime} 39^{\prime \prime}$ | 0.06 | $3^{\circ} 26^{\prime} 16^{\prime \prime}$ | 0.006 | $0^{\circ} 20^{\prime} 38^{\prime \prime}$ | 0.0006 | $0^{\circ} 2^{\prime} 4^{\prime \prime}$ |
| 70 | $4010^{\circ} 42^{\prime} 16^{\prime \prime}$ | 7 | $401^{\circ} 4^{\prime} 14^{\prime \prime}$ | 0.7 | $40^{\circ} 6^{\prime} 25^{\prime \prime}$ | 0.07 | $4^{\circ} 0^{\prime} 39^{\prime \prime}$ | 0.007 | $0^{\circ} 24^{\prime} 4^{\prime \prime}$ | 0.0007 | $0^{\circ} 2^{\prime} 24^{\prime \prime}$ |
| 80 | $4583{ }^{\circ} 39^{\prime} 44^{\prime \prime}$ | 8 | $458^{\circ} 21^{\prime} 58^{\prime \prime}$ | 0.8 | $45^{\circ} 50^{\prime} 12^{\prime \prime}$ | 0.08 | $4^{\circ} 35^{\prime} 1^{\prime \prime}$ | 0.008 | $0^{\circ} 27^{\prime} 30^{\prime \prime}$ | 0.0008 | $0^{\circ} 2^{\prime} 45^{\prime \prime}$ |
| 90 | $5156^{\circ} 37^{\prime} 13^{\prime \prime}$ | 9 | $515^{\circ} 39^{\prime} 43^{\prime \prime}$ | 0.9 | $51^{\circ} 33^{\prime} 58^{\prime \prime}$ | 0.09 | $5^{\circ} 9^{\prime} 24^{\prime \prime}$ | 0.009 | $0^{\circ} 30^{\prime} 56^{\prime \prime}$ | 0.0009 | $0^{\circ} 3^{\prime} 6^{\prime \prime}$ |
| 100 | $5729^{\circ} 34^{\prime} 41^{\prime \prime}$ | 10 | $572^{\circ} 57^{\prime} 28^{\prime \prime}$ | 1.0 | $57^{\circ} 17^{\prime} 45^{\prime \prime}$ | 0.10 | $5^{\circ} 43^{\prime} 46^{\prime \prime}$ | 0.010 | $0^{\circ} 34^{\prime} 23^{\prime \prime}$ | 0.0010 | $0^{\circ} 3^{\prime} 26^{\prime \prime}$ |

Minutes and Seconds into Decimal of a Degree and Vice Versa (Based on 1 second $=\mathbf{0 . 0 0 0 2 7 7 7 8}$ degree)

| Minutes into Decimals of a Degree |  |  |  |  |  |  |  | Seconds into Decimals of a Degree |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :--- | :---: | :--- | :---: |
| Min. | Deg. | Min. | Deg. | Min. | Deg. | Sec. | Deg. | Sec. | Deg. | Sec. | Deg. |
| 1 | 0.0167 | 21 | 0.3500 | 41 | 0.6833 | 1 | 0.0003 | 21 | 0.0058 | 41 | 0.0114 |
| 2 | 0.0333 | 22 | 0.3667 | 42 | 0.7000 | 2 | 0.0006 | 22 | 0.0061 | 42 | 0.0117 |
| 3 | 0.0500 | 23 | 0.3833 | 43 | 0.7167 | 3 | 0.0008 | 23 | 0.0064 | 43 | 0.0119 |
| 4 | 0.0667 | 24 | 0.4000 | 44 | 0.7333 | 4 | 0.0011 | 24 | 0.0067 | 44 | 0.0122 |
| 5 | 0.0833 | 25 | 0.4167 | 45 | 0.7500 | 5 | 0.0014 | 25 | 0.0069 | 45 | 0.0125 |
| 6 | 0.1000 | 26 | 0.4333 | 46 | 0.7667 | 6 | 0.0017 | 26 | 0.0072 | 46 | 0.0128 |
| 7 | 0.1167 | 27 | 0.4500 | 47 | 0.7833 | 7 | 0.0019 | 27 | 0.0075 | 47 | 0.0131 |
| 8 | 0.1333 | 28 | 0.4667 | 48 | 0.8000 | 8 | 0.0022 | 28 | 0.0078 | 48 | 0.0133 |
| 9 | 0.1500 | 29 | 0.4833 | 49 | 0.8167 | 9 | 0.0025 | 29 | 0.0081 | 49 | 0.0136 |
| 10 | 0.1667 | 30 | 0.5000 | 50 | 0.8333 | 10 | 0.0028 | 30 | 0.0083 | 50 | 0.0139 |
| 11 | 0.1833 | 31 | 0.5167 | 51 | 0.8500 | 11 | 0.0031 | 31 | 0.0086 | 51 | 0.0142 |
| 12 | 0.2000 | 32 | 0.5333 | 52 | 0.8667 | 12 | 0.0033 | 32 | 0.0089 | 52 | 0.0144 |
| 13 | 0.2167 | 33 | 0.5500 | 53 | 0.8833 | 13 | 0.0036 | 33 | 0.0092 | 53 | 0.0147 |
| 14 | 0.2333 | 34 | 0.5667 | 54 | 0.9000 | 14 | 0.0039 | 34 | 0.0094 | 54 | 0.0150 |
| 15 | 0.2500 | 35 | 0.5833 | 55 | 0.9167 | 15 | 0.0042 | 35 | 0.0097 | 55 | 0.0153 |
| 16 | 0.2667 | 36 | 0.6000 | 56 | 0.9333 | 16 | 0.0044 | 36 | 0.0100 | 56 | 0.0156 |
| 17 | 0.2833 | 37 | 0.6167 | 57 | 0.9500 | 17 | 0.0047 | 37 | 0.0103 | 57 | 0.0158 |
| 18 | 0.3000 | 38 | 0.6333 | 58 | 0.9667 | 18 | 0.0050 | 38 | 0.0106 | 58 | 0.0161 |
| 19 | 0.3167 | 39 | 0.6500 | 59 | 0.9833 | 19 | 0.0053 | 39 | 0.0108 | 59 | 0.0164 |
| 20 | 0.3333 | 40 | 0.6667 | 60 | 1.0000 | 20 | 0.0056 | 40 | 0.0111 | 60 | 0.0167 |

Example 1: Convert 11'37" to decimals of a degree. From the left table, $11^{\prime}=0.1833$ degree. From the right table, $37^{\prime \prime}=0.0103$ degree. Adding, $11^{\prime} 37^{\prime \prime}=0.1833+0.0103=0.1936$ degree.
Example 2: Convert 0.1234 degree to minutes and seconds. From the left table, 0.1167 degree $=7^{\prime}$. Subtracting 0.1167 from 0.1234 gives 0.0067 . From the right table, $0.0067=24^{\prime \prime}$ so that $0.1234=$ 7'24".


Signs of Trigonometric Functions, Fractions of $\pi$, and Degree-Radian Conversion
Graphic Illustrations of the Functions of Angles.-In graphically illustrating the functions of angles, it is assumed that all distances measured in the horizontal direction to the right of line $A B$ are positive. Those measured horizontally to the left of $A B$ are negative. All distances measured vertically, are positive above line $C D$ and negative below it. It can then be readily seen that the sine is positive for all angles less than 180 degrees. For angles larger than 180 degrees, the sine would be measured below $C D$, and is negative. The cosine is positive up to 90 degrees, but for angles larger than 90 but less than 270 degrees, the cosine is measured to the left of line $A B$ and is negative.
The table Useful Relationships Among Angles that follows is arranged to show directly whether the function of any given angle is positive or negative. It also gives the limits between which the numerical values of the function vary. For example, it will be seen from the table that the cosine of an angle between 90 and 180 degrees is negative, and that its value will be somewhere between 0 and - 1 . In the same way, the cotangent of an angle between 180 and 270 degrees is positive and has a value between infinity and 0 ; in other words, the cotangent for 180 degrees is infinitely large and then the cotangent gradually decreases for increasing angles, so that the cotangent for 270 degrees equals 0 .
The sine is positive for all angles up to 180 degrees. The cosine, tangent and cotangent for angles between 90 and 180 degrees, while they have the same numerical values as for angles from 0 to 90 degrees, are negative. These should be preceded by a minus sign; thus $\tan 123$ degrees 20 minutes $=-1.5204$.


Tables of Trigonometric Functions.- The trigonometric (trig) tables on the following pages give numerical values for sine, cosine, tangent, and cotangent functions of angles from 0 to 90 degrees. Function values for all other angles can be obtained from the tables by applying the rules for signs of trigonometric functions and the useful relationships among angles given in the following. Secant and cosecant functions can be found from sec $A=1 / \cos A$ and $\csc A=1 / \sin A$.

The trig tables are divided in half by a double line. The body of each half table consists of four labeled columns of data between columns listing angles. The angles listed to the left of the data increase, moving down the table, and angles listed to the right of the data increase, moving up the table. Labels above the data identify the trig functions corresponding to angles listed in the left column of each half table. Labels below the data correspond to angles listed in the right column of each half table. To find the value of a function for a particular angle, first locate the angle in the table, then find the appropriate function label across the top or bottom row of the table, and find the function value at the intersection of the angle row and label column. Angles opposite each other are complementary angles (i.e., their sum equals $90^{\circ}$ ) and are related. For example, $\sin 10^{\circ}=\cos 80^{\circ}$ and $\cos 10^{\circ}=\sin$ $80^{\circ}$.
All the trig functions of angles between $0^{\circ}$ and $90^{\circ}$ have positive values. For other angles, consult the chart below to find the sign of the function in the quadrant where the angle is located. To determine trig functions of angles greater than $90^{\circ}$ subtract $90,180,270$, or 360 from the angle to get an angle less than $90^{\circ}$ and use Table 1 to find the equivalent firstquadrant function and angle to look up in the trig tables.

Table 1. Useful Relationships Among Angles

| Angle Function | $\theta$ | $-\theta$ | $90^{\circ} \pm \theta$ | $180^{\circ} \pm \theta$ | $270^{\circ} \pm \theta$ | $360^{\circ} \pm \theta$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\sin$ | $\sin \theta$ | $-\sin \theta$ | $+\cos \theta$ | $\mp \sin \theta$ | $-\cos \theta$ | $\pm \sin \theta$ |
| $\cos$ | $\cos \theta$ | $+\cos \theta$ | $\mp \sin \theta$ | $-\cos \theta$ | $\pm \sin \theta$ | $+\cos \theta$ |
| $\tan$ | $\tan \theta$ | $-\tan \theta$ | $\mp \cot \theta$ | $\pm \tan \theta$ | $\mp \cot \theta$ | $\pm \tan \theta$ |
| $\cot$ | $\cot \theta$ | $-\cot \theta$ | $\mp \tan \theta$ | $\pm \cot \theta$ | $\mp \tan \theta$ | $\pm \cot \theta$ |
| $\sec$ | $\sec \theta$ | $+\sec \theta$ | $\mp \csc \theta$ | $-\sec \theta$ | $\pm \csc \theta$ | $+\sec \theta$ |
| $\csc$ | $\csc \theta$ | $-\csc \theta$ | $+\sec \theta$ | $\mp \csc \theta$ | $-\sec \theta$ | $\pm \csc \theta$ |

Examples: $\cos \left(270^{\circ}-\theta\right)=-\sin \theta ; \tan \left(90^{\circ}+\theta\right)=-\cot \theta$.
Example: Find the cosine of $336^{\circ} 40^{\prime}$. The diagram in Signs of Trigonometric Functions, Fractions of $\pi$, and Degree-Radian Conversion shows that the cosine of every angle in Quadrant IV $\left(270^{\circ}\right.$ to $\left.360^{\circ}\right)$ is positive. To find the angle and trig function to use when entering the trig table, subtract 270 from 336 to get $\cos 336^{\circ} 40^{\prime}=\cos \left(270^{\circ}+66^{\circ} 40^{\prime}\right)$ and then find the intersection of the cos row and the $270 \pm \theta$ column in Table 1. Because cos $(270 \pm \theta)$ in the fourth quadrant is equal to $\pm \sin \theta$ in the first quadrant, find $\sin 66^{\circ} 40^{\prime}$ in the trig table. Therefore, $\cos 336^{\circ} 40^{\prime}=\sin 66^{\circ} 40^{\prime}=0.918216$.

Trigonometric Functions of Angles from $0^{\circ}$ to $15^{\circ}$ and $75^{\circ}$ to $90^{\circ}$

| Angle | $\sin$ | cos | $\tan$ | cot |  | Angle | $\sin$ | cos | $\tan$ | cot |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $0^{\circ} 0^{\prime}$ | 0.000000 | 1.000000 | 0.000000 | - | $90^{\circ} 0^{\prime}$ | $7^{\circ} 30^{\prime}$ | 0.130526 | 0.991445 | 0.131652 | 7.595754 | $82^{\circ} 30^{\prime}$ |
| 10 | 0.002909 | 0.999996 | 0.002909 | 343.7737 | 50 | 40 | 0.133410 | 0.991061 | 0.134613 | 7.428706 | 20 |
| 20 | 0.005818 | 0.999983 | 0.005818 | 171.8854 | 40 | 50 | 0.136292 | 0.990669 | 0.137576 | 7.268725 | 10 |
| 30 | 0.008727 | 0.999962 | 0.008727 | 114.5887 | 30 | $8^{\circ} 0^{\prime}$ | 0.139173 | 0.990268 | 0.140541 | 7.115370 | $82^{\circ} 0^{\prime}$ |
| 40 | 0.011635 | 0.999932 | 0.011636 | 85.93979 | 20 | 10 | 0.142053 | 0.989859 | 0.143508 | 6.968234 | 50 |
| 50 | 0.014544 | 0.999894 | 0.014545 | 68.75009 | 10 | 20 | 0.144932 | 0.989442 | 0.146478 | 6.826944 | 40 |
| $1^{\circ} 0^{\prime}$ | 0.017452 | 0.999848 | 0.017455 | 57.28996 | $89^{\circ} 0^{\prime}$ | 30 | 0.147809 | 0.989016 | 0.149451 | 6.691156 | 30 |
| 10 | 0.020361 | 0.999793 | 0.020365 | 49.10388 | 50 | 40 | 0.150686 | 0.988582 | 0.152426 | 6.560554 | 20 |
| 20 | 0.023269 | 0.999729 | 0.023275 | 42.96408 | 40 | 50 | 0.153561 | 0.988139 | 0.155404 | 6.434843 | 10 |
| 30 | 0.026177 | 0.999657 | 0.026186 | 38.18846 | 30 | $9^{\circ} 0^{\prime}$ | 0.156434 | 0.987688 | 0.158384 | 6.313752 | $81^{\circ} 0^{\prime}$ |
| 40 | 0.029085 | 0.999577 | 0.029097 | 34.36777 | 20 | 10 | 0.159307 | 0.987229 | 0.161368 | 6.197028 | 50 |
| 50 | 0.031992 | 0.999488 | 0.032009 | 31.24158 | 10 | 20 | 0.162178 | 0.986762 | 0.164354 | 6.084438 | 40 |
| $2^{\circ} 0^{\prime}$ | 0.034899 | 0.999391 | 0.034921 | 28.63625 | $88^{\circ} 0^{\prime}$ | 30 | 0.165048 | 0.986286 | 0.167343 | 5.975764 | 30 |
| 10 | 0.037806 | 0.99928 | 0.037834 | 26.43 | 50 | 40 | 0.167916 | 0.985801 | 0.170334 | 5.870804 | 20 |
| 20 | 0.040713 | 0.999171 | 0.040747 | 24.54176 | 40 | 50 | 0.170783 | 0.985309 | 0.173329 | 5.769369 | 10 |
| 30 | 0.04361 | 0.99904 | 0.043661 | 22. | 30 | $10^{\circ} 0^{\prime}$ | 0.173648 | 0.984808 | 0.176327 | 5.671282 | $80^{\circ} 0^{\prime}$ |
| 40 | 0.046525 | 0.998917 | 0.046576 | 21.47040 | 20 | 10 | 0.176512 | 0.984298 | 0.179328 | 5.576379 | 50 |
| 50 | 0.049431 | 0.99877 | 0.049491 | 20.2055 | 10 | 20 | 0.179375 | 0.983781 | 0.182332 | 5.484505 | 40 |
| $3^{\circ} 0^{\prime}$ | 0.052336 | 0.998630 | 0.052408 | 19.0811 | $87^{\circ} 0^{\prime}$ | 30 | 0.182236 | 0.983255 | 0.185339 | 5.395517 | 30 |
| 10 | 0.055241 | 0.998473 | 0.055325 | 18.07498 | 50 | 40 | 0.185095 | 0.982721 | 0.188349 | 5.309279 | 20 |
| 20 | 0.058145 | 0.998308 | 0.058243 | 17.16934 | 40 | 50 | 0.187953 | 0.982178 | 0.191363 | 5.225665 | 10 |
| 30 | 0.061049 | 0.998135 | 0.061163 | 16.3498 | 30 | $11^{\circ} 0^{\prime}$ | 0.190809 | 0.981627 | 0.194380 | 5.144554 | $79^{\circ} 0^{\prime}$ |
| 40 | 0.063952 | 0.99795 | 0.064083 | 15.60478 | 20 | 10 | 0.193664 | 0.981068 | 0.197401 | 5.065835 | 50 |
| 50 | 0.066854 | 0.997763 | 0.067004 | 14.92442 | 10 | 20 | 0.196517 | 0.980500 | 0.200425 | 4.989403 | 40 |
| $4^{\circ} 0^{\prime}$ | 0.069756 | 0.99756 | 0.069927 | 14.30067 | $86^{\circ} 0^{\prime}$ | 30 | 0.199368 | 0.979925 | 0.203452 | 4.915157 | 30 |
| 10 | 0.072658 | 0.997357 | 0.072851 | 13.72674 | 50 | 40 | 0.202218 | 0.979341 | 0.206483 | 4.843005 | 20 |
| 20 | 0.075559 | 0.997141 | 0.075775 | 13.19688 | 40 | 50 | 0.205065 | 0.978748 | 0.209518 | 4.772857 | 10 |
| 30 | 0.078459 | 0.996917 | 0.078702 | 12.70621 | 30 | $12^{\circ} 0^{\prime}$ | 0.207912 | 0.978148 | 0.212557 | 4.704630 | $78^{\circ} 0^{\prime}$ |
| 40 | 0.081359 | 0.996685 | 0.081629 | 12.25051 | 20 | 10 | 0.210756 | 0.977539 | 0.215599 | 4.638246 | 50 |
| 50 | 0.084258 | 0.996444 | 0.084558 | 11.82617 | 10 | 20 | 0.213599 | 0.976921 | 0.218645 | 4.573629 | 40 |
| $5^{\circ} 0^{\prime}$ | 0.087156 | 0.996195 | 0.087489 | 11.43005 | $85^{\circ} 0^{\prime}$ | 30 | 0.216440 | 0.976296 | 0.221695 | 4.510709 | 30 |
| 10 | 0.090053 | 0.995937 | 0.090421 | 11.05943 | 50 | 40 | 0.219279 | 0.975662 | 0.224748 | 4.449418 | 20 |
| 20 | 0.092950 | 0.995671 | 0.093354 | 10.71191 | 40 | 50 | 0.222116 | 0.975020 | 0.227806 | 4.389694 | 10 |
| 30 | 0.095846 | 0.995396 | 0.096289 | 10.38540 | 30 | $13^{\circ} 0^{\prime}$ | 0.224951 | 0.974370 | 0.230868 | 4.331476 | $77^{\circ} 0^{\prime}$ |
| 40 | 0.098741 | 0.995113 | 0.099226 | 10.07803 | 20 | 10 | 0.227784 | 0.973712 | 0.233934 | 4.274707 | 50 |
| 50 | 0.101635 | 0.994822 | 0.102164 | 9.788173 | 10 | 20 | 0.230616 | 0.973045 | 0.237004 | 4.219332 | 40 |
| $6^{\circ} 0^{\prime}$ | 0.104528 | 0.994522 | 0.105104 | 9.514364 | $84^{\circ} 0^{\prime}$ | 30 | 0.233445 | 0.972370 | 0.240079 | 4.165300 | 30 |
| 10 | 0.107421 | 0.994214 | 0.108046 | 9.255304 | 50 | 40 | 0.236273 | 0.971687 | 0.243157 | 4.112561 | 20 |
| 20 | 0.110313 | 0.993897 | 0.110990 | 9.009826 | 40 | 50 | 0.239098 | 0.970995 | 0.246241 | 4.061070 | 10 |
| 30 | 0.113203 | 0.993572 | 0.113936 | 8.776887 | 30 | $14^{\circ} 0^{\prime}$ | 0.241922 | 0.970296 | 0.249328 | 4.010781 | $76^{\circ} 0^{\prime}$ |
| 40 | 0.116093 | 0.993238 | 0.116883 | 8.555547 | 20 | 10 | 0.244743 | 0.969588 | 0.252420 | 3.961652 | 50 |
| 50 | 0.118982 | 0.992896 | 0.119833 | 8.344956 | 10 | 20 | 0.247563 | 0.968872 | 0.255516 | 3.913642 | 40 |
| $7^{\circ} 0^{\prime}$ | 0.121869 | 0.992546 | 0.122785 | 8.144346 | $83^{\circ} 0^{\prime}$ | 30 | 0.250380 | 0.968148 | 0.258618 | 3.866713 | 30 |
| 10 | 0.124756 | 0.992187 | 0.125738 | 7.953022 | 50 | 40 | 0.253195 | 0.967415 | 0.261723 | 3.820828 | 20 |
| 20 | 0.127642 | 0.991820 | 0.128694 | 7.770351 | 40 | 50 | 0.256008 | 0.966675 | 0.264834 | 3.775952 | 10 |
| $7^{\circ} 30^{\prime}$ | 0.130526 | 0.991445 | 0.131652 | 7.595754 | $82^{\circ} 30$ | $15^{\circ} 0^{\prime}$ | 0.258819 | 0.965926 | 0.267949 | 3.732051 | $75^{\circ} 0^{\prime}$ |
|  | $\cos$ | $\sin$ | $\cot$ | $\tan$ |  | Angle | $\cos$ | sin | cot | tan | Angle |

For angles $0^{\circ}$ to $15^{\circ} 0^{\prime}$ (angles found in a column to the left of the data), use the column labels at the top of the table; for angles $75^{\circ}$ to $90^{\circ} 0^{\prime}$ (angles found in a column to the right of the data), use the column labels at the bottom of the table.

Trigonometric Functions of Angles from $15^{\circ}$ to $30^{\circ}$ and $60^{\circ}$ to $\mathbf{7 5}^{\circ}$

| Angle | sin | cos | $\tan$ | cot |  | Angle | sin | cos | $\tan$ | cot |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $15^{\circ} 0^{\prime}$ | 0.258819 | 0.965926 | 0.267949 | 3.732051 | $75^{\circ} 0^{\prime}$ | $22^{\circ} 30^{\prime}$ | 0.382683 | 0.923880 | 0.414214 | 2.414214 | $67^{\circ} 30$ |
| 10 | 0.261628 | 0.965169 | 0.271069 | 3.689093 | 50 | 40 | 0.385369 | 0.922762 | 0.417626 | 2.394489 | 20 |
| 20 | 0.264434 | 0.964404 | 0.274194 | 3.647047 | 40 | 50 | 0.388052 | 0.921638 | 0.421046 | 2.375037 | 10 |
| 30 | 0.267238 | 0.963630 | 0.277325 | 3.605884 | 30 | $23^{\circ} 0^{\prime}$ | 0.390731 | 0.920505 | 0.424475 | 2.355852 | $67^{\circ} 0^{\prime}$ |
| 40 | 0.270040 | 0.962849 | 0.280460 | 3.565575 | 20 | 10 | 0.393407 | 0.919364 | 0.427912 | 2.336929 | 50 |
| 50 | 0.272840 | 0.962059 | 0.283600 | 3.526094 | 10 | 20 | 0.396080 | 0.918216 | 0.431358 | 2.318261 | 40 |
| $16^{\circ} 0^{\prime}$ | 0.275637 | 0.961262 | 0.286745 | 3.487414 | $74^{\circ} 0^{\prime}$ | 30 | 0.398749 | 0.917060 | 0.434812 | 2.299843 | 30 |
| 10 | 0.278432 | 0.960456 | 0.289896 | 3.449512 | 50 | 40 | 0.401415 | 0.915896 | 0.438276 | 2.281669 | 20 |
| 20 | 0.281225 | 0.959642 | 0.293052 | 3.412363 | 40 | 50 | 0.404078 | 0.914725 | 0.441748 | 2.263736 | 10 |
| 30 | 0.284015 | 0.958820 | 0.296213 | 3.375943 | 30 | $24^{\circ} 0^{\prime}$ | 0.406737 | 0.913545 | 0.445229 | 2.246037 | $66^{\circ} 0^{\prime}$ |
| 40 | 0.286803 | 0.957990 | 0.299380 | 3.340233 | 20 | 10 | 0.409392 | 0.912358 | 0.448719 | 2.228568 | 50 |
| 50 | 0.289589 | 0.957151 | 0.302553 | 3.305209 | 10 | 20 | 0.412045 | 0.911164 | 0.452218 | 2.211323 | 40 |
| $17^{\circ} 0^{\prime}$ | 0.292372 | 0.956305 | 0.305731 | 3.270853 | $73^{\circ} 0^{\prime}$ | 30 | 0.414693 | 0.909961 | 0.455726 | 2.194300 | 30 |
| 10 | 0.295152 | 0.955450 | 0.308914 | 3.237144 | 50 | 40 | 0.417338 | 0.908751 | 0.459244 | 2.177492 | 20 |
| 20 | 0.297930 | 0.954588 | 0.312104 | 3.204064 | 40 | 50 | 0.419980 | 0.907533 | 0.462771 | 2.160896 | 10 |
| 30 | 0.300706 | 0.953717 | 0.315299 | 3.171595 | 30 | $25^{\circ} 0^{\prime}$ | 0.422618 | 0.906308 | 0.466308 | 2.144507 | $65^{\circ} 0^{\prime}$ |
| 40 | 0.303479 | 0.952838 | 0.318500 | 3.13971 | 20 | 10 | 0.425253 | 0.905075 | 0.469854 | 2.128321 | 50 |
| 50 | 0.306249 | 0.951951 | 0.321707 | 3.108421 | 10 | 20 | 0.427884 | 0.903834 | 0.473410 | 2.112335 | 40 |
| $18^{\circ} 0^{\prime}$ | 0.309017 | 0.95105 | 0.324920 | 3.07768 | $72^{\circ} 0$ | 30 | 0.430511 | 0.902585 | 0.476976 | 2.096544 | 30 |
| 10 | 0.311782 | 0.950154 | 0.328139 | 3.047492 | 50 | 40 | 0.433135 | 0.901329 | 0.480551 | 2.080944 | 20 |
| 20 | 0.314545 | 0.949243 | 0.33136 | 3.017830 | 40 | 50 | 0.435755 | 0.900065 | 0.484137 | 2.065532 | 10 |
| 30 | 0.317305 | 0.948324 | 0.334595 | 2.988685 | 30 | $26^{\circ} 0^{\prime}$ | 0.438371 | 0.898794 | 0.487733 | 2.050304 | $64^{\circ} 0^{\prime}$ |
| 40 | 0.320062 | 0.94739 | 0.337833 | 2.960042 | 20 | 10 | 0.44098 | 0.897515 | 0.491339 | 2.035256 | 50 |
| 50 | 0.322816 | 0.946462 | 0.341077 | 2.931888 | 10 | 20 | 0.443593 | 0.896229 | 0.494955 | 2.020386 | 40 |
| $19^{\circ} 0^{\prime}$ | 0.325568 | 0.945519 | 0.344328 | 2.904211 | $71^{\circ} 0^{\prime}$ | 30 | 0.446198 | 0.894934 | 0.498582 | 2.005690 | 30 |
| 10 | 0.328317 | 0.944568 | 0.347585 | 2.876997 | 50 | 40 | 0.448799 | 0.893633 | 0.502219 | 1.991164 | 20 |
| 20 | 0.331063 | 0.943609 | 0.350848 | 2.850235 | 40 | 50 | 0.451397 | 0.892323 | 0.505867 | 1.976805 | 10 |
| 30 | 0.333807 | 0.942641 | 0.354119 | 2.823913 | 30 | $27^{\circ} 0^{\prime}$ | 0.453990 | 0.891007 | 0.509525 | 1.962611 | $63^{\circ} 0^{\prime}$ |
| 40 | 0.336547 | 0.941666 | 0.357396 | 2.798020 | 20 | 10 | 0.456580 | 0.889682 | 0.513195 | 1.948577 | 50 |
| 50 | 0.339285 | 0.94068 | 0.360679 | 2.772545 | 10 | 20 | 0.459166 | 0.888350 | 0.516875 | 1.934702 | 40 |
| $20^{\circ} 0^{\prime}$ | 0.342020 | 0.939693 | 0.363970 | 2.747477 | $70^{\circ} 0^{\prime}$ | 30 | 0.461749 | 0.887011 | 0.520567 | 1.920982 | 30 |
| 10 | 0.344752 | 0.93869 | 0.367268 | 2.722808 | 50 | 40 | 0.464327 | 0.885664 | 0.524270 | 1.907415 | 20 |
| 20 | 0.347481 | 0.937687 | 0.370573 | 2.698525 | 40 | 50 | 0.466901 | 0.884309 | 0.527984 | 1.893997 | 10 |
| 30 | 0.350207 | 0.93667 | 0.373885 | 2.674621 | 30 | $28^{\circ} 0^{\prime}$ | 0.469472 | 0.882948 | 0.531709 | 1.880726 | $62^{\circ} 0^{\prime}$ |
| 40 | 0.352931 | 0.935650 | 0.377204 | 2.651087 | 20 | 10 | 0.472038 | 0.881578 | 0.535446 | 1.867600 | 50 |
| 50 | 0.355651 | 0.934619 | 0.380530 | 2.627912 | 10 | 20 | 0.474600 | 0.880201 | 0.539195 | 1.854616 | 40 |
| $21^{\circ} 0^{\prime}$ | 0.358368 | 0.933580 | 0.383864 | 2.605089 | $69^{\circ} 0^{\prime}$ | 30 | 0.477159 | 0.878817 | 0.542956 | 1.841771 | 30 |
| 10 | 0.361082 | 0.932534 | 0.387205 | 2.582609 | 50 | 40 | 0.479713 | 0.877425 | 0.546728 | 1.829063 | 20 |
| 20 | 0.363793 | 0.931480 | 0.390554 | 2.560465 | 40 | 50 | 0.482263 | 0.876026 | 0.550513 | 1.816489 | 10 |
| 30 | 0.366501 | 0.930418 | 0.393910 | 2.538648 | 30 | $29^{\circ} 0^{\prime}$ | 0.484810 | 0.874620 | 0.554309 | 1.804048 | $61^{\circ} 0^{\prime}$ |
| 40 | 0.369206 | 0.929348 | 0.397275 | 2.517151 | 20 | 10 | 0.487352 | 0.873206 | 0.558118 | 1.791736 | 50 |
| 50 | 0.371908 | 0.928270 | 0.400646 | 2.495966 | 10 | 20 | 0.489890 | 0.871784 | 0.561939 | 1.779552 | 40 |
| $22^{\circ} 0^{\prime}$ | 0.374607 | 0.927184 | 0.404026 | 2.475087 | $68^{\circ} 0^{\prime}$ | 30 | 0.492424 | 0.870356 | 0.565773 | 1.767494 | 30 |
| 10 | 0.377302 | 0.926090 | 0.407414 | 2.454506 | 50 | 40 | 0.494953 | 0.868920 | 0.569619 | 1.755559 | 20 |
| 20 | 0.379994 | 0.924989 | 0.410810 | 2.434217 | 40 | 50 | 0.497479 | 0.867476 | 0.573478 | 1.743745 | 10 |
| $22^{\circ} 30$ | 0.382683 | 0.923880 | 0.414214 | 2.414214 | $67^{\circ} 30$ | $30^{\circ} 0^{\prime}$ | 0.500000 | 0.866025 | 0.577350 | 1.732051 | $60^{\circ} 0^{\prime}$ |
|  | cos | sin | cot | $\tan$ | Angle |  | $\cos$ | $\sin$ | cot | $\tan$ | Angle |

For angles $15^{\circ}$ to $30^{\circ} 0^{\prime}$ (angles found in a column to the left of the data), use the column labels at the top of the table; for angles $60^{\circ}$ to $75^{\circ} 0^{\prime}$ (angles found in a column to the right of the data), use the column labels at the bottom of the table.

Trigonometric Functions of Angles from $30^{\circ}$ to $60^{\circ}$

| Angle | $\sin$ | cos | $\tan$ | cot |  | Angle | sin | cos | $\tan$ | cot |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $30^{\circ} 0^{\prime}$ | 0.500000 | 0.866025 | 0.577350 | 1.732051 | $60^{\circ} 0^{\prime}$ | $37^{\circ} 30^{\prime}$ | 0.608761 | 0.793353 | 0.767327 | 1.303225 | $52^{\circ} 30^{\prime}$ |
| 10 | 0.502517 | 0.864567 | 0.581235 | 1.720474 | 50 | 40 | 0.611067 | 0.791579 | 0.771959 | 1.295406 | 20 |
| 20 | 0.505030 | 0.863102 | 0.585134 | 1.709012 | 40 | 50 | 0.613367 | 0.789798 | 0.776612 | 1.287645 | 10 |
| 30 | 0.507538 | 0.861629 | 0.589045 | 1.697663 | 30 | $38^{\circ} 0^{\prime}$ | 0.615661 | 0.788011 | 0.781286 | 1.279942 | $52^{\circ} 0^{\prime}$ |
| 40 | 0.510043 | 0.860149 | 0.592970 | 1.686426 | 20 | 10 | 0.617951 | 0.786217 | 0.785981 | 1.272296 | 50 |
| 50 | 0.512543 | 0.858662 | 0.596908 | 1.675299 | 10 | 20 | 0.620235 | 0.784416 | 0.790697 | 1.264706 | 40 |
| $31{ }^{\circ} 0^{\prime}$ | 0.515038 | 0.857167 | 0.600861 | 1.664279 | $59^{\circ} 0^{\prime}$ | 30 | 0.622515 | 0.782608 | 0.795436 | 1.257172 | 30 |
| 10 | 0.517529 | 0.855665 | 0.604827 | 1.653366 | 50 | 40 | 0.624789 | 0.780794 | 0.800196 | 1.249693 | 20 |
| 20 | 0.520016 | 0.854156 | 0.608807 | 1.642558 | 40 | 50 | 0.627057 | 0.778973 | 0.804979 | 1.242268 | 10 |
| 30 | 0.522499 | 0.852640 | 0.612801 | 1.631852 | 30 | $39^{\circ} 0^{\prime}$ | 0.629320 | 0.777146 | 0.809784 | 1.234897 | $51^{\circ} 0^{\prime}$ |
| 40 | 0.524977 | 0.851117 | 0.616809 | 1.621247 | 20 | 10 | 0.631578 | 0.775312 | 0.814612 | 1.227579 | 50 |
| 50 | 0.527450 | 0.849586 | 0.620832 | 1.610742 | 10 | 20 | 0.633831 | 0.773472 | 0.819463 | 1.220312 | 40 |
| $32^{\circ} 0^{\prime}$ | 0.529919 | 0.848048 | 0.624869 | 1.600335 | $58^{\circ} 0^{\prime}$ | 30 | 0.636078 | 0.771625 | 0.824336 | 1.213097 | 30 |
| 10 | 0.532384 | 0.846503 | 0.628921 | 1.59002 | 50 | 40 | 0.638320 | 0.769771 | 0.829234 | 1.205933 | 20 |
| 20 | 0.534844 | 0.844951 | 0.632988 | 1.579808 | 40 | 50 | 0.640557 | 0.767911 | 0.834155 | 1.198818 | 10 |
| 30 | 0.537300 | 0.84339 | 0.637070 | 1.56968 | 30 | $40^{\circ} 0^{\prime}$ | 0.642788 | 0.766044 | 0.839100 | 1.191754 | $50^{\circ} 0^{\prime}$ |
| 40 | 0.539751 | 0.841825 | 0.641167 | 1.559655 | 20 | 10 | 0.645013 | 0.764171 | 0.844069 | 1.184738 | 50 |
| 50 | 0.542197 | 0.84025 | 0.645280 | 1.54971 | 10 | 20 | 0.647233 | 0.762292 | 0.849062 | 1.177770 | 40 |
| $33^{\circ} 0^{\prime}$ | 0.544639 | 0.838671 | 0.649408 | 1.539865 | $57^{\circ} 0^{\prime}$ | 30 | 0.649448 | 0.760406 | 0.854081 | 1.170850 | 30 |
| 10 | 0.547076 | 0.837083 | 0.653551 | 1.530102 | 50 | 40 | 0.651657 | 0.758514 | 0.859124 | 1.163976 | 20 |
| 20 | 0.549509 | 0.835488 | 0.657710 | 1.520426 | 40 | 50 | 0.653861 | 0.756615 | 0.864193 | 1.157149 | 10 |
| 30 | 0.551937 | 0.833886 | 0.661886 | 1.510835 | 30 | $41^{\circ} 0^{\prime}$ | 0.656059 | 0.754710 | 0.869287 | 1.150368 | $49^{\circ} 0^{\prime}$ |
| 40 | 0.554360 | 0.832277 | 0.666077 | 1.501328 | 20 | 10 | 0.658252 | 0.752798 | 0.874407 | 1.143633 | 50 |
| 50 | 0.556779 | 0.830661 | 0.670284 | 1.491904 | 10 | 20 | 0.660439 | 0.750880 | 0.879553 | 1.136941 | 40 |
| $34^{\circ} 0^{\prime}$ | 0.559193 | 0.829038 | 0.674509 | 1.482561 | $56^{\circ} 0^{\prime}$ | 30 | 0.662620 | 0.748956 | 0.884725 | 1.130294 | 30 |
| 10 | 0.561602 | 0.827407 | 0.678749 | 1.473298 | 50 | 40 | 0.664796 | 0.747025 | 0.889924 | 1.123691 | 20 |
| 20 | 0.564007 | 0.825770 | 0.683007 | 1.464115 | 40 | 50 | 0.666966 | 0.745088 | 0.895151 | 1.117130 | 10 |
| 30 | 0.566406 | 0.824126 | 0.687281 | 1.455009 | 30 | $42^{\circ} 0^{\prime}$ | 0.669131 | 0.743145 | 0.900404 | 1.110613 | $48^{\circ} 0^{\prime}$ |
| 40 | 0.568801 | 0.822475 | 0.691572 | 1.445980 | 20 | 10 | 0.671289 | 0.741195 | 0.905685 | 1.104137 | 50 |
| 50 | 0.571191 | 0.820817 | 0.695881 | 1.437027 | 10 | 20 | 0.673443 | 0.739239 | 0.910994 | 1.097702 | 40 |
| $35^{\circ} 0^{\prime}$ | 0.573576 | 0.819152 | 0.700208 | 1.428148 | $55^{\circ} 0^{\prime}$ | 30 | 0.675590 | 0.737277 | 0.916331 | 1.091309 | 30 |
| 10 | 0.575957 | 0.817480 | 0.704551 | 1.419343 | 50 | 40 | 0.677732 | 0.735309 | 0.921697 | 1.084955 | 20 |
| 20 | 0.578332 | 0.815801 | 0.708913 | 1.410610 | 40 | 50 | 0.679868 | 0.733334 | 0.927091 | 1.078642 | 10 |
| 30 | 0.580703 | 0.814116 | 0.713293 | 1.401948 | 30 | $43^{\circ} 0^{\prime}$ | 0.681998 | 0.731354 | 0.932515 | 1.072369 | $47^{\circ} 0^{\prime}$ |
| 40 | 0.583069 | 0.812423 | 0.717691 | 1.393357 | 20 | 10 | 0.684123 | 0.729367 | 0.937968 | 1.066134 | 50 |
| 50 | 0.585429 | 0.810723 | 0.722108 | 1.384835 | 10 | 20 | 0.686242 | 0.727374 | 0.943451 | 1.059938 | 40 |
| $36^{\circ} 0^{\prime}$ | 0.587785 | 0.809017 | 0.726543 | 1.376382 | $54^{\circ} 0^{\prime}$ | 30 | 0.688355 | 0.725374 | 0.948965 | 1.053780 | 30 |
| 10 | 0.590136 | 0.807304 | 0.730996 | 1.367996 | 50 | 40 | 0.690462 | 0.723369 | 0.954508 | 1.047660 | 20 |
| 20 | 0.592482 | 0.805584 | 0.735469 | 1.359676 | 40 | 50 | 0.692563 | 0.721357 | 0.960083 | 1.041577 | 10 |
| 30 | 0.594823 | 0.803857 | 0.739961 | 1.351422 | 30 | $44^{\circ} 0^{\prime}$ | 0.694658 | 0.719340 | 0.965689 | 1.035530 | $46^{\circ} 0^{\prime}$ |
| 40 | 0.597159 | 0.802123 | 0.744472 | 1.343233 | 20 | 10 | 0.696748 | 0.717316 | 0.971326 | 1.029520 | 50 |
| 50 | 0.599489 | 0.800383 | 0.749003 | 1.335108 | 10 | 20 | 0.698832 | 0.715286 | 0.976996 | 1.023546 | 40 |
| $37^{\circ} 0^{\prime}$ | 0.601815 | 0.798636 | 0.753554 | 1.327045 | $53^{\circ} 0^{\prime}$ | 30 | 0.700909 | 0.713250 | 0.982697 | 1.017607 | 30 |
| 10 | 0.604136 | 0.796882 | 0.758125 | 1.319044 | 50 | 40 | 0.702981 | 0.711209 | 0.988432 | 1.011704 | 20 |
| 20 | 0.606451 | 0.795121 | 0.762716 | 1.311105 | 40 | 50 | 0.705047 | 0.709161 | 0.994199 | 1.005835 | 10 |
| $37^{\circ} 30$ | 0.608761 | 0.793353 | 0.767327 | 1.303225 | $52^{\circ} 30$ | $45^{\circ} 0^{\prime}$ | 0.707107 | 0.707107 | 1.000000 | 1.000000 | $45^{\circ} 0^{\prime}$ |
|  | $\cos$ | sin | $\cot$ | $\tan$ | Angle |  | $\cos$ | $\sin$ | cot | $\tan$ | Angle |

For angles $30^{\circ}$ to $45^{\circ} 0^{\prime}$ (angles found in a column to the left of the data), use the column labels at the top of the table; for angles $45^{\circ}$ to $60^{\circ} 0^{\prime}$ (angles found in a column to the right of the data), use the column labels at the bottom of the table.

Using a Calculator to Find Trig Functions.-A scientific calculator is quicker and more accurate than tables for finding trig functions and angles corresponding to trig functions. On scientific calculators, the keys labeled $\sin$, $\boldsymbol{\operatorname { c o s }}$, and $\boldsymbol{\operatorname { t a n }}$ are used to find the common trig functions. The other functions can be found by using the same keys and the $1 / x$ key, noting that $\csc A=1 / \sin A, \sec A=1 / \cos A$, and $\cot A=1 / \tan A$. The specific keystrokes used will vary slightly from one calculator to another. To find the angle corresponding to a given trig function use the keys labeled $\boldsymbol{\operatorname { s i n }}^{-1}, \boldsymbol{\operatorname { c o s }}^{-1}$, and $\boldsymbol{t a n}^{-1}$. On some other calculators, the $\sin , \cos$, and $\boldsymbol{t a n}$ are used in combination with the INV, or inverse, key to find the number corresponding to a given trig function.

If a scientific calculator or computer is not available, tables are the easiest way to find trig values. However, trig function values can be calculated very accurately without a scientific calculator by using the following formulas:

$$
\begin{aligned}
\sin A & =A-\frac{A^{3}}{3!}+\frac{A^{5}}{5!}-\frac{A^{7}}{7!} \pm \cdots & \cos A & =1-\frac{A^{2}}{2!}+\frac{A^{4}}{4!}-\frac{A^{6}}{6!} \pm \cdots \\
\sin ^{-1} A & =\frac{1}{2} \times \frac{A^{3}}{3}+\frac{1}{2} \times \frac{3}{4} \times \frac{A^{5}}{5}+\cdots & \tan ^{-1} A & =A-\frac{A^{3}}{3}+\frac{A^{5}}{5}-\frac{A^{7}}{7} \pm \cdots
\end{aligned}
$$

where the angle $A$ is expressed in radians (convert degrees to radians by multiplying degrees by $\pi / 180=0.0174533$ ). The three dots at the ends of the formulas indicate that the expression continues with more terms following the sequence established by the first few terms. Generally, calculating just three or four terms of the expression is sufficient for accuracy. In these formulas, a number followed by the symbol ! is called a factorial (for example, 3 ! is three factorial). Except for 0 !, which is defined as 1 , a factorial is found by multiplying together all the integers greater than zero and less than or equal to the factorial number wanted. For example: $3!=1 \times 2 \times 3=6 ; 4!=1 \times 2 \times 3 \times 4=24 ; 7!=1 \times 2 \times 3 \times 4 \times$ $5 \times 6 \times 7=5040$; etc.

Versed Sine and Versed Cosine.-These functions are sometimes used in formulas for segments of a circle and may be obtained using the relationships:

$$
\text { versed } \sin \theta=1-\cos \theta ; \text { versed } \cos \theta=1-\sin \theta \text {. }
$$

Sevolute Functions.-Sevolute functions are used in calculating the form diameter of involute splines. They are computed by subtracting the involute function of an angle from the secant of the angle $(1 /$ cosine $=$ secant $)$. Thus, sevolute of 20 degrees $=$ secant of 20 degrees - involute function of 20 degrees $=1.064178-0.014904=1.049274$.

Involute Functions.-Involute functions are used in certain formulas relating to the design and measurement of gear teeth as well as measurement of threads over wires. See, for example, pages 1867 through 1870, 2080, and 2147.

The tables on the following pages provide values of involute functions for angles from 14 to 51 degrees in increments of 1 minute. These involute functions were calculated from the following formulas: Involute of $\theta=\tan \theta-\theta$, for $\theta$ in radians, and involute of $\theta=\tan \theta-\pi$ $\times \theta / 180$, for $\theta$ in degrees.

Example: For an angle of 14 degrees and 10 minutes, the involute function is found as follows: 10 minutes $=10 / 60=0.166666$ degrees, $14+0.166666=14.166666$ degree, so that the involute of 14.166666 degrees $=\tan 14.166666-\pi \times 14.166666 / 180=0.252420-$ $0.247255=0.005165$. This value is the same as that in the table Involute Functions for Angles from 14 to 23 Degrees for 14 degrees and 10 minutes. The same result would be obtained from using the conversion tables beginning on page 90 to convert 14 degrees and 10 minutes to radians and then applying the first of the formulas given above.

Involute Functions for Angles from 14 to 23 Degrees

| Minutes | Degrees |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 |
|  | Involute Functions |  |  |  |  |  |  |  |  |
| 0 | 0.004982 | 0.006150 | 0.007493 | 0.009025 | 0.010760 | 0.012715 | 0.014904 | 0.017345 | 0.020054 |
| 1 | 0.005000 | 0.006171 | 0.007517 | 0.009052 | 0.010791 | 0.012750 | 0.014943 | 0.017388 | 0.020101 |
| 2 | 0.005018 | 0.006192 | 0.007541 | 0.009079 | 0.010822 | 0.012784 | 0.014982 | 0.017431 | 0.020149 |
| 3 | 0.005036 | 0.006213 | 0.007565 | 0.009107 | 0.010853 | 0.012819 | 0.015020 | 0.017474 | 0.020197 |
| 4 | 0.005055 | 0.006234 | 0.007589 | 0.009134 | 0.010884 | 0.012854 | 0.015059 | 0.017517 | 0.020244 |
| 5 | 0.005073 | 0.006255 | 0.007613 | 0.009161 | 0.010915 | 0.012888 | 0.015098 | 0.017560 | 0.020292 |
| 6 | 0.005091 | 0.006276 | 0.007637 | 0.009189 | 0.010946 | 0.012923 | 0.015137 | 0.017603 | 0.020340 |
| 7 | 0.005110 | 0.006297 | 0.007661 | 0.009216 | 0.010977 | 0.012958 | 0.015176 | 0.017647 | 0.020388 |
| 8 | 0.005128 | 0.006318 | 0.007686 | 0.009244 | 0.011008 | 0.012993 | 0.015215 | 0.017690 | 0.020436 |
| 9 | 0.005146 | 0.006340 | 0.007710 | 0.009272 | 0.011039 | 0.013028 | 0.015254 | 0.017734 | 0.020484 |
| 10 | 0.005165 | 0.006361 | 0.007735 | 0.009299 | 0.011071 | 0.013063 | 0.015293 | 0.017777 | 0.020533 |
| 11 | 0.005184 | 0.006382 | 0.007759 | 0.009327 | 0.011102 | 0.013098 | 0.015333 | 0.017821 | 0.020581 |
| 12 | 0.005202 | 0.006404 | 0.007784 | 0.009355 | 0.011133 | 0.013134 | 0.015372 | 0.017865 | 0.020629 |
| 13 | 0.005221 | 0.006425 | 0.007808 | 0.009383 | 0.011165 | 0.013169 | 0.015411 | 0.017908 | 0.020678 |
| 14 | 0.005239 | 0.006447 | 0.007833 | 0.009411 | 0.011196 | 0.013204 | 0.015451 | 0.017952 | 0.020726 |
| 15 | 0.005258 | 0.006469 | 0.007857 | 0.009439 | 0.011228 | 0.013240 | 0.015490 | 0.017996 | 0.020775 |
| 16 | 0.005277 | 0.006490 | 0.007882 | 0.009467 | 0.011260 | 0.013275 | 0.015530 | 0.018040 | 0.020824 |
| 17 | 0.005296 | 0.006512 | 0.007907 | 0.009495 | 0.011291 | 0.013311 | 0.015570 | 0.018084 | 0.020873 |
| 18 | 0.005315 | 0.006534 | 0.007932 | 0.009523 | 0.011323 | 0.013346 | 0.015609 | 0.018129 | 0.020921 |
| 19 | 0.005334 | 0.006555 | 0.007957 | 0.009552 | 0.011355 | 0.013382 | 0.015649 | 0.018173 | 0.020970 |
| 20 | 0.005353 | 0.006577 | 0.007982 | 0.009580 | 0.011387 | 0.013418 | 0.015689 | 0.018217 | 0.021019 |
| 21 | 0.005372 | 0.006599 | 0.008007 | 0.009608 | 0.011419 | 0.013454 | 0.015729 | 0.018262 | 0.021069 |
| 22 | 0.005391 | 0.006621 | 0.008032 | 0.009637 | 0.011451 | 0.013490 | 0.015769 | 0.018306 | 0.021118 |
| 23 | 0.005410 | 0.006643 | 0.008057 | 0.009665 | 0.011483 | 0.013526 | 0.015809 | 0.018351 | 0.021167 |
| 24 | 0.005429 | 0.006665 | 0.008082 | 0.009694 | 0.011515 | 0.013562 | 0.015850 | 0.018395 | 0.021217 |
| 25 | 0.005448 | 0.006687 | 0.008107 | 0.009722 | 0.011547 | 0.013598 | 0.015890 | 0.018440 | 0.021266 |
| 26 | 0.005467 | 0.006709 | 0.008133 | 0.009751 | 0.011580 | 0.013634 | 0.015930 | 0.018485 | 0.021316 |
| 27 | 0.005487 | 0.006732 | 0.008158 | 0.009780 | 0.011612 | 0.013670 | 0.015971 | 0.018530 | 0.021365 |
| 28 | 0.005506 | 0.006754 | 0.008183 | 0.009808 | 0.011644 | 0.013707 | 0.016011 | 0.018575 | 0.021415 |
| 29 | 0.005525 | 0.006776 | 0.008209 | 0.009837 | 0.011677 | 0.013743 | 0.016052 | 0.018620 | 0.021465 |
| 30 | 0.005545 | 0.006799 | 0.008234 | 0.009866 | 0.011709 | 0.013779 | 0.016092 | 0.018665 | 0.021514 |
| 31 | 0.005564 | 0.006821 | 0.008260 | 0.009895 | 0.011742 | 0.013816 | 0.016133 | 0.018710 | 0.021564 |
| 32 | 0.005584 | 0.006843 | 0.008285 | 0.009924 | 0.011775 | 0.013852 | 0.016174 | 0.018755 | 0.021614 |
| 33 | 0.005603 | 0.006866 | 0.008311 | 0.009953 | 0.011807 | 0.013889 | 0.016215 | 0.018800 | 0.021665 |
| 34 | 0.005623 | 0.006888 | 0.008337 | 0.009982 | 0.011840 | 0.013926 | 0.016255 | 0.018846 | 0.021715 |
| 35 | 0.005643 | 0.006911 | 0.008362 | 0.010011 | 0.011873 | 0.013963 | 0.016296 | 0.018891 | 0.021765 |
| 36 | 0.005662 | 0.006934 | 0.008388 | 0.010041 | 0.011906 | 0.013999 | 0.016337 | 0.018937 | 0.021815 |
| 37 | 0.005682 | 0.006956 | 0.008414 | 0.010070 | 0.011939 | 0.014036 | 0.016379 | 0.018983 | 0.021866 |
| 38 | 0.005702 | 0.006979 | 0.008440 | 0.010099 | 0.011972 | 0.014073 | 0.016420 | 0.019028 | 0.021916 |
| 39 | 0.005722 | 0.007002 | 0.008466 | 0.010129 | 0.012005 | 0.014110 | 0.016461 | 0.019074 | 0.021967 |
| 40 | 0.005742 | 0.007025 | 0.008492 | 0.010158 | 0.012038 | 0.014148 | 0.016502 | 0.019120 | 0.022018 |
| 41 | 0.005762 | 0.007048 | 0.008518 | 0.010188 | 0.012071 | 0.014185 | 0.016544 | 0.019166 | 0.022068 |
| 42 | 0.005782 | 0.007071 | 0.008544 | 0.010217 | 0.012105 | 0.014222 | 0.016585 | 0.019212 | 0.022119 |
| 43 | 0.005802 | 0.007094 | 0.008571 | 0.010247 | 0.012138 | 0.014259 | 0.016627 | 0.019258 | 0.022170 |
| 44 | 0.005822 | 0.007117 | 0.008597 | 0.010277 | 0.012172 | 0.014297 | 0.016669 | 0.019304 | 0.022221 |
| 45 | 0.005842 | 0.007140 | 0.008623 | 0.010307 | 0.012205 | 0.014334 | 0.016710 | 0.019350 | 0.022272 |
| 46 | 0.005862 | 0.007163 | 0.008650 | 0.010336 | 0.012239 | 0.014372 | 0.016752 | 0.019397 | 0.022324 |
| 47 | 0.005882 | 0.007186 | 0.008676 | 0.010366 | 0.012272 | 0.014409 | 0.016794 | 0.019443 | 0.022375 |
| 48 | 0.005903 | 0.007209 | 0.008702 | 0.010396 | 0.012306 | 0.014447 | 0.016836 | 0.019490 | 0.022426 |
| 49 | 0.005923 | 0.007233 | 0.008729 | 0.010426 | 0.012340 | 0.014485 | 0.016878 | 0.019536 | 0.022478 |
| 50 | 0.005943 | 0.007256 | 0.008756 | 0.010456 | 0.012373 | 0.014523 | 0.016920 | 0.019583 | 0.022529 |
| 51 | 0.005964 | 0.007280 | 0.008782 | 0.010486 | 0.012407 | 0.014560 | 0.016962 | 0.019630 | 0.022581 |
| 52 | 0.005984 | 0.007303 | 0.008809 | 0.010517 | 0.012441 | 0.014598 | 0.017004 | 0.019676 | 0.022633 |
| 53 | 0.006005 | 0.007327 | 0.008836 | 0.010547 | 0.012475 | 0.014636 | 0.017047 | 0.019723 | 0.022684 |
| 54 | 0.006025 | 0.007350 | 0.008863 | 0.010577 | 0.012509 | 0.014674 | 0.017089 | 0.019770 | 0.022736 |
| 55 | 0.006046 | 0.007374 | 0.008889 | 0.010608 | 0.012543 | 0.014713 | 0.017132 | 0.019817 | 0.022788 |
| 56 | 0.006067 | 0.007397 | 0.008916 | 0.010638 | 0.012578 | 0.014751 | 0.017174 | 0.019864 | 0.022840 |
| 57 | 0.006087 | 0.007421 | 0.008943 | 0.010669 | 0.012612 | 0.014789 | 0.017217 | 0.019912 | 0.022892 |
| 58 | 0.006108 | 0.007445 | 0.008970 | 0.010699 | 0.012646 | 0.014827 | 0.017259 | 0.019959 | 0.022944 |
| 59 | 0.006129 | 0.007469 | 0.008998 | 0.010730 | 0.012681 | 0.014866 | 0.017302 | 0.020006 | 0.022997 |
| 60 | 0.006150 | 0.007493 | 0.009025 | 0.010760 | 0.012715 | 0.014904 | 0.017345 | 0.020054 | 0.023049 |

Involute Functions for Angles from 23 to 32 Degrees

| Minutes | Degrees |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | 31 |
|  | Involute Functions |  |  |  |  |  |  |  |  |
| 0 | 0.023049 | 0.026350 | 0.029975 | 0.033947 | 0.038287 | 0.043017 | 0.048164 | 0.053752 | 0.059809 |
| 1 | 0.023102 | 0.026407 | 0.030039 | 0.034016 | 0.038362 | 0.043100 | 0.048253 | 0.053849 | 0.059914 |
| 2 | 0.023154 | 0.026465 | 0.030102 | 0.034086 | 0.038438 | 0.043182 | 0.048343 | 0.053946 | 0.060019 |
| 3 | 0.023207 | 0.026523 | 0.030166 | 0.034155 | 0.038514 | 0.043264 | 0.048432 | 0.054043 | 0.060124 |
| 4 | 0.023259 | 0.026581 | 0.030229 | 0.034225 | 0.038590 | 0.043347 | 0.048522 | 0.054140 | 0.060230 |
| 5 | 0.023312 | 0.026639 | 0.030293 | 0.034294 | 0.038666 | 0.043430 | 0.048612 | 0.054238 | 0.060335 |
| 6 | 0.023365 | 0.026697 | 0.030357 | 0.034364 | 0.038742 | 0.043513 | 0.048702 | 0.054336 | 0.060441 |
| 7 | 0.023418 | 0.026756 | 0.030420 | 0.034434 | 0.038818 | 0.043596 | 0.048792 | 0.054433 | 0.060547 |
| 8 | 0.023471 | 0.026814 | 0.030484 | 0.034504 | 0.038894 | 0.043679 | 0.048883 | 0.054531 | 0.060653 |
| 9 | 0.023524 | 0.026872 | 0.030549 | 0.034574 | 0.038971 | 0.043762 | 0.048973 | 0.054629 | 0.060759 |
| 10 | 0.023577 | 0.026931 | 0.030613 | 0.034644 | 0.039047 | 0.043845 | 0.049064 | 0.054728 | 0.060866 |
| 11 | 0.023631 | 0.026989 | 0.030677 | 0.034714 | 0.039124 | 0.043929 | 0.049154 | 0.054826 | 0.060972 |
| 12 | 0.023684 | 0.027048 | 0.030741 | 0.034785 | 0.039201 | 0.044012 | 0.049245 | 0.054924 | 0.061079 |
| 13 | 0.023738 | 0.027107 | 0.030806 | 0.034855 | 0.039278 | 0.044096 | 0.049336 | 0.055023 | 0.061186 |
| 14 | 0.023791 | 0.027166 | 0.030870 | 0.034926 | 0.039355 | 0.044180 | 0.049427 | 0.055122 | 0.061292 |
| 15 | 0.023845 | 0.027225 | 0.030935 | 0.034997 | 0.039432 | 0.044264 | 0.049518 | 0.055221 | 0.061400 |
| 16 | 0.023899 | 0.027284 | 0.031000 | 0.035067 | 0.039509 | 0.044348 | 0.049609 | 0.055320 | 0.061507 |
| 17 | 0.023952 | 0.027343 | 0.031065 | 0.035138 | 0.039586 | 0.044432 | 0.049701 | 0.055419 | 0.061614 |
| 18 | 0.024006 | 0.027402 | 0.031130 | 0.035209 | 0.039664 | 0.044516 | 0.049792 | 0.055518 | 0.061721 |
| 19 | 0.024060 | 0.027462 | 0.031195 | 0.035280 | 0.039741 | 0.044601 | 0.049884 | 0.055617 | 0.061829 |
| 20 | 0.024114 | 0.027521 | 0.031260 | 0.035352 | 0.039819 | 0.044685 | 0.049976 | 0.055717 | 0.061937 |
| 21 | 0.024169 | 0.027581 | 0.031325 | 0.035423 | 0.039897 | 0.044770 | 0.050068 | 0.055817 | 0.062045 |
| 22 | 0.024223 | 0.027640 | 0.031390 | 0.035494 | 0.039974 | 0.044855 | 0.050160 | 0.055916 | 0.062153 |
| 23 | 0.024277 | 0.027700 | 0.031456 | 0.035566 | 0.040052 | 0.044940 | 0.050252 | 0.056016 | 0.062261 |
| 24 | 0.024332 | 0.027760 | 0.031521 | 0.035637 | 0.040131 | 0.045024 | 0.050344 | 0.056116 | 0.062369 |
| 25 | 0.024386 | 0.027820 | 0.031587 | 0.035709 | 0.040209 | 0.045110 | 0.050437 | 0.056217 | 0.062478 |
| 26 | 0.024441 | 0.027880 | 0.031653 | 0.035781 | 0.040287 | 0.045195 | 0.050529 | 0.056317 | 0.062586 |
| 27 | 0.024495 | 0.027940 | 0.031718 | 0.035853 | 0.040366 | 0.045280 | 0.050622 | 0.056417 | 0.062695 |
| 28 | 0.024550 | 0.028000 | 0.031784 | 0.035925 | 0.040444 | 0.045366 | 0.050715 | 0.056518 | 0.062804 |
| 29 | 0.024605 | 0.028060 | 0.031850 | 0.035997 | 0.040523 | 0.045451 | 0.050808 | 0.056619 | 0.062913 |
| 30 | 0.024660 | 0.028121 | 0.031917 | 0.036069 | 0.040602 | 0.045537 | 0.050901 | 0.056720 | 0.063022 |
| 31 | 0.024715 | 0.028181 | 0.031983 | 0.036142 | 0.040680 | 0.045623 | 0.050994 | 0.056821 | 0.063131 |
| 32 | 0.024770 | 0.028242 | 0.032049 | 0.036214 | 0.040759 | 0.045709 | 0.051087 | 0.056922 | 0.063241 |
| 33 | 0.024825 | 0.028302 | 0.032116 | 0.036287 | 0.040839 | 0.045795 | 0.051181 | 0.057023 | 0.063350 |
| 34 | 0.024881 | 0.028363 | 0.032182 | 0.036359 | 0.040918 | 0.045881 | 0.051274 | 0.057124 | 0.063460 |
| 35 | 0.024936 | 0.028424 | 0.032249 | 0.036432 | 0.040997 | 0.045967 | 0.051368 | 0.057226 | 0.063570 |
| 36 | 0.024992 | 0.028485 | 0.032315 | 0.036505 | 0.041077 | 0.046054 | 0.051462 | 0.057328 | 0.063680 |
| 37 | 0.025047 | 0.028546 | 0.032382 | 0.036578 | 0.041156 | 0.046140 | 0.051556 | 0.057429 | 0.063790 |
| 38 | 0.025103 | 0.028607 | 0.032449 | 0.036651 | 0.041236 | 0.046227 | 0.051650 | 0.057531 | 0.063901 |
| 39 | 0.025159 | 0.028668 | 0.032516 | 0.036724 | 0.041316 | 0.046313 | 0.051744 | 0.057633 | 0.064011 |
| 40 | 0.025214 | 0.028729 | 0.032583 | 0.036798 | 0.041395 | 0.046400 | 0.051838 | 0.057736 | 0.064122 |
| 41 | 0.025270 | 0.028791 | 0.032651 | 0.036871 | 0.041475 | 0.046487 | 0.051933 | 0.057838 | 0.064232 |
| 42 | 0.025326 | 0.028852 | 0.032718 | 0.036945 | 0.041556 | 0.046575 | 0.052027 | 0.057940 | 0.064343 |
| 43 | 0.025382 | 0.028914 | 0.032785 | 0.037018 | 0.041636 | 0.046662 | 0.052122 | 0.058043 | 0.064454 |
| 44 | 0.025439 | 0.028976 | 0.032853 | 0.037092 | 0.041716 | 0.046749 | 0.052217 | 0.058146 | 0.064565 |
| 45 | 0.025495 | 0.029037 | 0.032920 | 0.037166 | 0.041797 | 0.046837 | 0.052312 | 0.058249 | 0.064677 |
| 46 | 0.025551 | 0.029099 | 0.032988 | 0.037240 | 0.041877 | 0.046924 | 0.052407 | 0.058352 | 0.064788 |
| 47 | 0.025608 | 0.029161 | 0.033056 | 0.037314 | 0.041958 | 0.047012 | 0.052502 | 0.058455 | 0.064900 |
| 48 | 0.025664 | 0.029223 | 0.033124 | 0.037388 | 0.042039 | 0.047100 | 0.052597 | 0.058558 | 0.065012 |
| 49 | 0.025721 | 0.029285 | 0.033192 | 0.037462 | 0.042120 | 0.047188 | 0.052693 | 0.058662 | 0.065123 |
| 50 | 0.025778 | 0.029348 | 0.033260 | 0.037537 | 0.042201 | 0.047276 | 0.052788 | 0.058765 | 0.065236 |
| 51 | 0.025834 | 0.029410 | 0.033328 | 0.037611 | 0.042282 | 0.047364 | 0.052884 | 0.058869 | 0.065348 |
| 52 | 0.025891 | 0.029472 | 0.033397 | 0.037686 | 0.042363 | 0.047452 | 0.052980 | . 058973 | 0.065460 |
| 53 | 0.025948 | 0.029535 | 0.033465 | 0.037761 | 0.042444 | 0.047541 | 0.053076 | 0.059077 | 0.065573 |
| 54 | 0.026005 | 0.029598 | 0.033534 | 0.037835 | 0.042526 | 0.047630 | 0.053172 | 0.059181 | 0.065685 |
| 55 | 0.026062 | 0.029660 | 0.033602 | 0.037910 | 0.042608 | 0.047718 | 0.053268 | 0.059285 | 0.065798 |
| 56 | 0.026120 | 0.029723 | 0.033671 | 0.037985 | 0.042689 | 0.047807 | 0.053365 | 0.059390 | 0.065911 |
| 57 | 0.026177 | 0.029786 | 0.033740 | 0.038060 | 0.042771 | 0.047896 | 0.053461 | 0.059494 | 0.066024 |
| 58 | 0.026235 | 0.029849 | 0.033809 | 0.038136 | 0.042853 | 0.047985 | 0.053558 | 0.059599 | 0.066137 |
| 59 | 0.026292 | 0.029912 | 0.033878 | 0.038211 | 0.042935 | 0.048074 | 0.053655 | 0.059704 | 0.066251 |
| 60 | 0.026350 | 0.029975 | 0.033947 | 0.038287 | 0.043017 | 0.048164 | 0.053752 | 0.059809 | 0.066364 |

Involute Functions for Angles from 32 to 41 Degrees

| Minutes | Degrees |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 32 | 33 | 34 | 35 | 36 | 37 | 38 | 39 | 40 |
|  | Involute Functions |  |  |  |  |  |  |  |  |
| 0 | 0.066364 | 0.073449 | 0.081097 | 0.089342 | 0.098224 | 0.107782 | 0.118061 | 0.129106 | 0.140968 |
| 1 | 0.066478 | 0.073572 | 0.081229 | 0.089485 | 0.098378 | 0.107948 | 0.118238 | 0.129297 | 0.141173 |
| 2 | 0.066591 | 0.073695 | 0.081362 | 0.089628 | 0.098532 | 0.108113 | 0.118416 | 0.129488 | 0.141378 |
| 3 | 0.066705 | 0.073818 | 0.081494 | 0.089771 | 0.098686 | 0.108279 | 0.118594 | 0.129679 | 0.141584 |
| 4 | 0.066820 | 0.073941 | 0.081627 | 0.089914 | 0.098840 | 0.108445 | 0.118773 | 0.129870 | 0.141789 |
| 5 | 0.066934 | 0.074064 | 0.081760 | 0.090058 | 0.098994 | 0.108611 | 0.118951 | 0.130062 | 0.141995 |
| 6 | 0.067048 | 0.074188 | 0.081894 | 0.090201 | 0.099149 | 0.108777 | 0.119130 | 0.130254 | 0.142201 |
| 7 | 0.067163 | 0.074312 | 0.082027 | 0.090345 | 0.099303 | 0.108943 | 0.119309 | 0.130446 | 0.142408 |
| 8 | 0.067277 | 0.074435 | 0.082161 | 0.090489 | 0.099458 | 0.109110 | 0.119488 | 0.130639 | 0.142614 |
| 9 | 0.067392 | 0.074559 | 0.082294 | 0.090633 | 0.099614 | 0.109277 | 0.119667 | 0.130832 | 0.142821 |
| 10 | 0.067507 | 0.074684 | 0.082428 | 0.090777 | 0.099769 | 0.109444 | 0.119847 | 0.131025 | 0.143028 |
| 11 | 0.067622 | 0.074808 | 0.082562 | 0.090922 | 0.099924 | 0.109611 | 0.120027 | 0.131218 | 0.143236 |
| 12 | 0.067738 | 0.074932 | 0.082697 | 0.091067 | 0.100080 | 0.109779 | 0.120207 | 0.131411 | 0.143443 |
| 13 | 0.067853 | 0.075057 | 0.082831 | 0.091211 | 0.100236 | 0.109947 | 0.120387 | 0.131605 | 0.143651 |
| 14 | 0.067969 | 0.075182 | 0.082966 | 0.091356 | 0.100392 | 0.110114 | 0.120567 | 0.131799 | 0.143859 |
| 15 | 0.068084 | 0.075307 | 0.083101 | 0.091502 | 0.100549 | 0.110283 | 0.120748 | 0.131993 | 0.144068 |
| 16 | 0.068200 | 0.075432 | 0.083235 | 0.091647 | 0.100705 | 0.110451 | 0.120929 | 0.132187 | 0.144276 |
| 17 | 0.068316 | 0.075557 | 0.083371 | 0.091793 | 0.100862 | 0.110619 | 0.121110 | 0.132381 | 0.144485 |
| 18 | 0.068432 | 0.075683 | 0.083506 | 0.091938 | 0.101019 | 0.110788 | 0.121291 | 0.132576 | 0.144694 |
| 19 | 0.068549 | 0.075808 | 0.083641 | 0.092084 | 0.101176 | 0.110957 | 0.121473 | 0.132771 | 0.144903 |
| 20 | 0.068665 | 0.075934 | 0.083777 | 0.092230 | 0.101333 | 0.111126 | 0.121655 | 0.132966 | 0.145113 |
| 21 | 0.068782 | 0.076060 | 0.083913 | 0.092377 | 0.101490 | 0.111295 | 0.121837 | 0.133162 | 0.145323 |
| 22 | 0.068899 | 0.076186 | 0.084049 | 0.092523 | 0.101648 | 0.111465 | 0.122019 | 0.133358 | 0.145533 |
| 23 | 0.069016 | 0.076312 | 0.084185 | 0.092670 | 0.101806 | 0.111635 | 0.122201 | 0.133553 | 0.145743 |
| 24 | 0.069133 | 0.076439 | 0.084321 | 0.092816 | 0.101964 | 0.111805 | 0.122384 | 0.133750 | 0.145954 |
| 25 | 0.069250 | 0.076565 | 0.084458 | 0.092963 | 0.102122 | 0.111975 | 0.122567 | 0.133946 | 0.146165 |
| 26 | 0.069367 | 0.076692 | 0.084594 | 0.093111 | 0.102280 | 0.112145 | 0.122750 | 0.134143 | 0.146376 |
| 27 | 0.069485 | 0.076819 | 0.084731 | 0.093258 | 0.102439 | 0.112316 | 0.122933 | 0.134339 | 0.146587 |
| 28 | 0.069602 | 0.076946 | 0.084868 | 0.093406 | 0.102598 | 0.112486 | 0.123117 | 0.134537 | 0.146799 |
| 29 | 0.069720 | 0.077073 | 0.085005 | 0.093553 | 0.102757 | 0.112657 | 0.123300 | 0.134734 | 0.147010 |
| 30 | 0.069838 | 0.077200 | 0.085142 | 0.093701 | 0.102916 | 0.112829 | 0.123484 | 0.134931 | 0.147222 |
| 31 | 0.069956 | 0.077328 | 0.085280 | 0.093849 | 0.103075 | 0.113000 | 0.123668 | 0.135129 | 0.147435 |
| 32 | 0.070075 | 0.077455 | 0.085418 | 0.093998 | 0.103235 | 0.113172 | 0.123853 | 0.135327 | 0.147647 |
| 33 | 0.070193 | 0.077583 | 0.085555 | 0.094146 | 0.103395 | 0.113343 | 0.124037 | 0.135525 | 0.147860 |
| 34 | 0.070312 | 0.077711 | 0.085693 | 0.094295 | 0.103555 | 0.113515 | 0.124222 | 0.135724 | 0.148073 |
| 35 | 0.070430 | 0.077839 | 0.085832 | 0.094443 | 0.103715 | 0.113688 | 0.124407 | 0.135923 | 0.148286 |
| 36 | 0.070549 | 0.077968 | 0.085970 | 0.094593 | 0.103875 | 0.113860 | 0.124592 | 0.136122 | 0.148500 |
| 37 | 0.070668 | 0.078096 | 0.086108 | 0.094742 | 0.104036 | 0.114033 | 0.124778 | 0.136321 | 0.148714 |
| 38 | 0.070788 | 0.078225 | 0.086247 | 0.094891 | 0.104196 | 0.114205 | 0.124964 | 0.136520 | 0.148928 |
| 39 | 0.070907 | 0.078354 | 0.086386 | 0.095041 | 0.104357 | 0.114378 | 0.125150 | 0.136720 | 0.149142 |
| 40 | 0.071026 | 0.078483 | 0.086525 | 0.095190 | 0.104518 | 0.114552 | 0.125336 | 0.136920 | 0.149357 |
| 41 | 0.071146 | 0.078612 | 0.086664 | 0.095340 | 0.104680 | 0.114725 | 0.125522 | 0.137120 | 0.149572 |
| 42 | 0.071266 | 0.078741 | 0.086804 | 0.095490 | 0.104841 | 0.114899 | 0.125709 | 0.137320 | 0.149787 |
| 43 | 0.071386 | 0.078871 | 0.086943 | 0.095641 | 0.105003 | 0.115073 | 0.125896 | 0.137521 | 0.150002 |
| 44 | 0.071506 | 0.079000 | 0.087083 | 0.095791 | 0.105165 | 0.115247 | 0.126083 | 0.137722 | 0.150218 |
| 45 | 0.071626 | 0.079130 | 0.087223 | 0.095942 | 0.105327 | 0.115421 | 0.126270 | 0.137923 | 0.150434 |
| 46 | 0.071747 | 0.079260 | 0.087363 | 0.096093 | 0.105489 | 0.115595 | 0.126457 | 0.138124 | 0.150650 |
| 47 | 0.071867 | 0.079390 | 0.087503 | 0.096244 | 0.105652 | 0.115770 | 0.126645 | 0.138326 | 0.150866 |
| 48 | 0.071988 | 0.079520 | 0.087644 | 0.096395 | 0.105814 | 0.115945 | 0.126833 | 0.138528 | 0.151083 |
| 49 | 0.072109 | 0.079651 | 0.087784 | 0.096546 | 0.105977 | 0.116120 | 0.127021 | 0.138730 | 0.151299 |
| 50 | 0.072230 | 0.079781 | 0.087925 | 0.096698 | 0.106140 | 0.116296 | 0.127209 | 0.138932 | 0.151517 |
| 51 | 0.072351 | 0.079912 | 0.088066 | 0.096850 | 0.106304 | 0.116471 | 0.127398 | 0.139134 | 0.151734 |
| 52 | 0.072473 | 0.080043 | 0.088207 | 0.097002 | 0.106467 | 0.116647 | 0.127587 | 0.139337 | 0.151952 |
| 53 | 0.072594 | 0.080174 | 0.088348 | 0.097154 | 0.106631 | 0.116823 | 0.127776 | 0.139540 | 0.152169 |
| 54 | 0.072716 | 0.080306 | 0.088490 | 0.097306 | 0.106795 | 0.116999 | 0.127965 | 0.139743 | 0.152388 |
| 55 | 0.072838 | 0.080437 | 0.088631 | 0.097459 | 0.106959 | 0.117175 | 0.128155 | 0.139947 | 0.152606 |
| 56 | 0.072960 | 0.080569 | 0.088773 | 0.097611 | 0.107123 | 0.117352 | 0.128344 | 0.140151 | 0.152825 |
| 57 | 0.073082 | 0.080700 | 0.088915 | 0.097764 | 0.107288 | 0.117529 | 0.128534 | 0.140355 | 0.153044 |
| 58 | 0.073204 | 0.080832 | 0.089057 | 0.097917 | 0.107452 | 0.117706 | 0.128725 | 0.140559 | 0.153263 |
| 59 | 0.073326 | 0.080964 | 0.089200 | 0.098071 | 0.107617 | 0.117883 | 0.128915 | 0.140763 | 0.153482 |
| 60 | 0.073449 | 0.081097 | 0.089342 | 0.098224 | 0.107782 | 0.118061 | 0.129106 | 0.140968 | 0.153702 |

Involute Functions for Angles from 41 to 50 Degrees

| Minutes | Degrees |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 41 | 42 | 43 | 44 | 45 | 46 | 47 | 48 | 49 |
|  | Involute Functions |  |  |  |  |  |  |  |  |
| 0 | 02 | 0.167366 | 182024 | 197744 | 0.214602 | 0.232679 | 0.252064 | 0.272855 | 157 |
| 1 | 153922 | 0.16 | 0.182277 | 0.198015 | 0.214893 | . 23 | 0.252399 | 0.273214 | 0.295542 |
| 2 | 0.154142 | 0.167838 | 0.182530 | 0.198287 | 0.215184 | 0.233304 | 0.25273 | 0.273573 | 5928 |
| 3 | 0.154362 | 0.168075 | 182784 | 0.198559 | 0.215476 | 0.233616 | 0.253069 | 0.273933 | 0.296314 |
| 4 | 0.154583 | 0.168311 | 0.183038 | 0.198832 | 0.215768 | 0.233930 | 0.253405 | 0.274293 | 0.296701 |
| 5 | 0.154804 | 0.168548 | 0.183292 | 0.199104 | 0.216061 | 0.234243 | 0.253742 | 0.274654 | 0.297088 |
| 6 | 0.155025 | 0.1687 | 183547 | 0.199377 | 0.216353 | 0.234557 | 0.254078 | 0.275015 | 0.297475 |
| 7 | 0.155247 | 0.1690 | 183801 | 0.199651 | 0.216646 | 0.234871 | 0.254415 | 0.275376 | 63 |
| 8 | 0.155469 | 0.169261 | 0.184057 | 0.199924 | 0.216940 | 0.235186 | 0.254753 | 0.275738 | 0.298251 |
| 9 | 0.155691 | 0.169500 | 0.184312 | 0.200198 | 0.217234 | 0.235501 | 0.255091 | 0.276101 | 0.298640 |
| 10 | 0.155913 | 0.169738 | 0.184568 | 0.200473 | 0.217528 | 0.235816 | 0.255429 | 0.276464 | 0.299029 |
| 11 | 0.156135 | 0.169977 | 0.184824 | 0.200747 | 0.217822 | 0.236132 | 0.255767 | 0.276827 | 0.299419 |
| 12 | 0.156358 | 0.170216 | 0.185080 | 0.201022 | 0.218117 | 0.236448 | 0.256106 | 0.277191 | 0.299809 |
| 13 | 0.156581 | 0.170455 | 0.185337 | 0.201297 | 0.218412 | 0.236765 | 0.256446 | 0.277555 | 0.300200 |
| 14 | 0.156805 | 0.170695 | 0.185594 | 0.201573 | 0.218708 | 0.237082 | 0.256786 | 0.277919 | 0.300591 |
| 15 | 0.157028 | 0.170935 | 0.185851 | 0.201849 | 0.219004 | 0.237399 | 0.257126 | 0.278284 | 0.300983 |
| 16 | 0.157252 | 175 | 109 | 0.202125 | 0.219300 | 0.237717 | 0.257467 | 0.278649 | 375 |
| 17 | 0.157476 | 0.171415 | 0.186367 | 0.202401 | 0.219596 | 0.238035 | 0.257808 | 0.279015 | 0.301767 |
| 18 | 0.157701 | 0.171656 | 0.186625 | 0.202678 | 0.219893 | 0.238353 | 0.258149 | 0.279381 | 0.302160 |
| 19 | 0.157925 | 0.171897 | 0.186883 | 0.202956 | 0.220190 | 0.238672 | 0.258491 | 0.279748 | 0.302553 |
| 20 | 0.158150 | 0.172138 | 0.187142 | 0.203233 | 0.220488 | 0.238991 | 0.258833 | 0.280115 | 0.302947 |
| 21 | 0.158375 | 0.1 | 187401 | 0.203511 | 0.220786 | 0.239310 | 0.259176 | 0.280483 | 342 |
| 22 | 0.158601 | 0.172621 | 0.187661 | 0.203789 | 0.221084 | 0.239630 | 0.259519 | 0.280851 | 0.303736 |
| 23 | 0.158826 | 0.172864 | 0.187920 | 0.204067 | 0.221383 | 0.239950 | 0.259862 | 0.281219 | 0.304132 |
| 24 | 0.159052 | 0.173106 | 0.188180 | 0.204346 | 0.221682 | 0.240271 | 0.260206 | 0.281588 | 0.304527 |
| 25 | 0.159279 | 0.173349 | 0.188440 | 0.204625 | 0.221981 | 0.240592 | 0.260550 | 0.281957 | 0.304924 |
| 26 | 0.1 | 0. | 0.188701 | 0.204905 | 0.222281 | 0.240913 | 0.260895 | 0.282327 | 320 |
| 27 | 0.159732 | 0.173835 | 0.188962 | 0.205185 | 0.222581 | 0.241235 | 0.261240 | 0.282697 | 0.305718 |
| 28 | 0.159959 | 0.174078 | 0.189223 | 0.205465 | 0.222881 | 0.241557 | 0.261585 | 0.283067 | 0.306115 |
| 29 | 0.160186 | 0.174322 | 0.189485 | 0.205745 | 0.223182 | 0.241879 | 0.261931 | 0.283438 | 0.306513 |
| 30 | 0.160414 | 0.174566 | 0.189746 | 0.206026 | 0.223483 | 0.242202 | 0.262277 | 0.283810 | 0.306912 |
| 31 | 0.1 | 0.174811 | 09 | 0.206307 | 0.223784 | 0.242525 | 0.262624 | 0.284182 | 311 |
| 32 | 0.160870 | 0.175055 | 0.190271 | 0.206588 | 0.224086 | 0.242849 | 0.262971 | 0.284554 | 0.307710 |
| 33 | 0.161098 | 0.175300 | 0.190534 | 0.206870 | 0.224388 | 0.243173 | 0.263318 | 0.284927 | 0.308110 |
| 34 | 0.161327 | 0.175546 | 0.190797 | 0.207152 | 0.224690 | 0.243497 | 0.263666 | 0.285300 | 0.308511 |
| 35 | 0.161555 | 0.175791 | 0.191060 | 0.207434 | 0.224993 | 0.243822 | 0.264014 | 0.285673 | 0.308911 |
| 36 | 0.161785 | 0.176037 | 0.191324 | 0.207717 | 0.225296 | 0.244147 | 0.264363 | 0.286047 | 0.309313 |
| 37 | 0.162014 | 0.176283 | 0.191588 | 0.208000 | 0.225600 | 0.244472 | 0.264712 | 0.286422 | 0.309715 |
| 38 | 0.162244 | 0.176529 | 0.191852 | 0.208284 | 0.225904 | 0.244798 | 0.265062 | 0.286797 | 0.310117 |
| 39 | 0.162474 | 0.176776 | 0.192116 | 0.208567 | 0.226208 | 0.245125 | 0.265412 | 0.287172 | 0.310520 |
| 40 | 0.162704 | 0.177023 | 0.192381 | 0.208851 | 0.226512 | 0.245451 | 0.265762 | 0.287548 | 0.310923 |
| 41 | 0.162934 | 0.177270 | 0.192646 | 0.209136 | 0.226817 | 0.245778 | 0.266113 | 0.287924 | 0.311327 |
| 42 | 0.163165 | 0.177518 | 0.192912 | 0.209420 | 0.227123 | 0.246106 | 0.266464 | 0.288301 | 0.311731 |
| 43 | 0.163396 | 0.177766 | 0.193178 | 0.209705 | 0.227428 | 0.246433 | 0.266815 | 0.288678 | 0.312136 |
| 44 | 0.163628 | 0.178014 | 0.193444 | 0.209991 | 0.227734 | 0.246761 | 0.267167 | 0.289056 | 0.312541 |
| 45 | 0.163859 | 0.178262 | 0.193710 | 0.210276 | 0.228041 | 0.247090 | 0.267520 | 0.289434 | 0.312947 |
| 46 | 0.164091 | 0.178511 | 0.193977 | 0.210562 | 0.228347 | 0.247419 | 0.267872 | 0.289812 | 0.313353 |
| 47 | 0.164323 | 0.178760 | 0.194244 | 0.210849 | 0.228654 | 0.247748 | 0.268225 | 0.290191 | 0.313759 |
| 48 | 0.164556 | 0.179009 | 0.194511 | 0.211136 | 0.228962 | 0.248078 | 0.268579 | 0.290570 | 0.314166 |
| 49 | 0.164788 | 0.179259 | 0.194779 | 0.211423 | 0.229270 | 0.248408 | 0.268933 | 0.290950 | 0.314574 |
| 50 | 0.165021 | 0.179509 | 0.195047 | 0.211710 | 0.229578 | 0.248738 | 0.269287 | 0.291330 | 0.314982 |
| 51 | 0.165254 | 0.179759 | 0.195315 | 0.211998 | 0.229886 | 0.249069 | 0.269642 | 0.291711 | 0.315391 |
| 52 | 0.165488 | 0.180009 | 0.195584 | 0.212286 | 0.230195 | 0.249400 | 0.269998 | 0.292092 | 0.315800 |
| 53 | 0.165722 | 0.180260 | 0.195853 | 0.212574 | 0.230504 | 0.249732 | 0.270353 | 0.292474 | 0.316209 |
| 54 | 0.165956 | 0.180511 | 0.196122 | 0.212863 | 0.230814 | 0.250064 | 0.270709 | 0.292856 | 0.316619 |
| 55 | 0.166190 | 0.180763 | 0.196392 | 0.213152 | 0.231124 | 0.250396 | 0.271066 | 0.293238 | 0.317029 |
| 56 | 0.166425 | 0.181014 | 0.196661 | 0.213441 | 0.231434 | 0.250729 | 0.271423 | 0.293621 | 0.337444 |
| 57 | 0.166660 | 0.181266 | 0.196932 | 0.213731 | 0.231745 | 0.251062 | 0.271780 | 0.294004 | 0.317852 |
| 58 | 0.166895 | 0.181518 | 0.197202 | 0.214021 | 0.232056 | 0.251396 | 0.272138 | 0.294388 | 0.318264 |
| 59 | 0.167130 | 0.181771 | 0.197473 | 0.214311 | 0.232367 | 0.251730 | 0.272496 | 0.294772 | 0.318676 |
| 60 | 0.167366 | 0.182024 | 0.197744 | 0.214602 | 0.232679 | 0.2 | 0.272855 | 0.295157 | 0.31908 |

## LOGARITHMS

Logarithms are used to facilitate and shorten calculations involving multiplication, division, the extraction of roots, and obtaining powers of numbers. The following properties of logarithms are useful in solving problems of this type:

$$
\begin{array}{lll}
\log _{c} c=1 & \log _{c} c^{p}=p & \log _{c} 1=0 \\
\log _{c}(a \times b)=\log _{c} a+\log _{c} b & \log _{c}(a \div b)=\log _{c} a-\log _{c} b \\
\log _{c}\left(a^{p}\right)=p \log _{c} a & & \log _{c}(\sqrt[p]{a})=1 / p \log _{c} a
\end{array}
$$

The logarithm of a number is defined as the exponent of a base number raised to a power. For example, $\log _{10} 3.162277=0.500$ means the logarithm of 3.162277 is equal to 0.500 . Another way of expressing the same relationship is $10^{0.500}=3.162277$, where 10 is the base number and the exponent 0.500 is the logarithm of 3.162277 . A common example of a logarithmic expression $10^{2}=100$ means that the base 10 logarithm of 100 is 2 , that is, $\log _{10}$ $100=2.00$. There are two standard systems of logarithms in use: the "common" system (base 10) and the so-called "natural" system (base $e=2.71828+$ ). Logarithms to base $e$ are frequently written using "ln" instead of " $\log _{e}$ " such as $\ln 6.1=1.808289$. Logarithms of a number can be converted between the natural- and common-based systems as follows: $\ln _{e}$ $\mathrm{A}=2.3026 \times \log _{10} A$ and $\log _{10} A=0.43430 \times \ln _{e} A$. Additional information on the use of "natural logarithms" is given at the end of this section.
A logarithm consists of two parts, a whole number and a decimal. The whole number, which may be positive, negative, or zero, is called the characteristic; the decimal is called the mantissa. As a rule, only the decimal or mantissa is given in tables of common logarithms; tables of natural logarithms give both the characteristic and mantissa. The tables given in this section are abbreviated, but very accurate results can be obtained by using the method of interpolation described in Interpolation from the Tables that follows. These tables are especially useful for finding logarithms and calculating powers and roots of numbers on calculators without these functions built in.

## Evaluating Logarithms

Common Logarithms.-For common logarithms, the characteristic is prefixed to the mantissa according to the following rules: For numbers greater than or equal to 1 , the characteristic is one less than the number of places to the left of the decimal point. For example, the characteristic of the logarithm of 237 is 2 , and of 2536.5 is 3 . For numbers smaller than 1 and greater than 0 , the characteristic is negative and its numerical value is one more than the number of zeros immediately to the right of the decimal point. For example, the characteristic of the logarithm of 0.036 is -2 , and the characteristic of the logarithm of 0.0006 is -4 . The minus sign is usually written over the figure, as in $\overline{2}$ to indicate that the minus sign refers only to the characteristic and not to the mantissa, which is never negative. The logarithm of 0 does not exist.
The table of common logarithms in this section gives the mantissas of the logarithms of numbers from 1 to 10 and from 1.00 to 1.01. When finding the mantissa, the decimal point in a number is disregarded. The mantissa of the logarithms of 2716, 271.6,27.16, 2.716, or 0.02716 , for example, is the same. The tables give directly the mantissas of logarithms of numbers with three figures or less; the logarithms for numbers with four or more figures can be found by interpolation, as described in Interpolation from the Tables and illustrated in the examples. All the mantissas in the common logarithmic tables are decimals and the decimal point has been omitted in the table. However, a decimal point should always be put before the mantissa as soon as it is taken from the table. Logarithmic tables are sufficient for many purposes, but electronic calculators and computers are faster, simpler, and more accurate than tables.

To find the common logarithm of a number from the tables, find the left-hand column of the table and follow down to locate the first two figures of the number. Then look at the top row of the table, on the same page, and follow across it to find the third figure of the number. Follow down the column containing this last figure until opposite the row on which the first two figures were found. The number at the intersection of the row and column is the mantissa of the logarithm. If the logarithm of a number with less than three figures is being obtained, add extra zeros to the right of the number so as to obtain three figures. For example, if the mantissa of the logarithm of 6 is required, find the mantissa of 600 .
Interpolation from the Tables.-If the logarithm of a number with more than three figures is needed, linear interpolation is a method of using two values from the table to estimate the value of the logarithm desired. To find the logarithm of a number not listed in the tables, find the mantissa corresponding to the first three digits of the given number (disregarding the decimal point and leading zeros) and find the mantissa of the first three digits of the given number plus one. For example, to find the logarithm of 601.2, 60.12, or 0.006012 , find the mantissa of 601 and find the mantissa of 602 from the tables. Then subtract the mantissa of the smaller number from the mantissa of the larger number and multiply the result by a decimal number made from the remaining (additional greater than 3 ) figures of the original number. Add the result to the mantissa of the smaller number. Find the characteristic as described previously.
Example: Find the logarithm of 4032. The characteristic portion of the logarithm found in the manner described before is 3 . Find the mantissa by locating 40 in the left-hand column of the logarithmic tables and then follow across the top row of the table to the column headed 3 . Follow down the 3 column to the intersection with the 40 row and read the mantissa. The mantissa of the logarithm of 4030 is 0.605305 . Because 4032 is between 4030 and 4040, the logarithm of 4032 is the logarithm of 4030 plus two tenths of the difference in the logarithms of 4030 and 4040 . Find the mantissa of 4040 and then subtract from it the mantissa of 4030 . Multiply the difference obtained by 0.2 and add the result to the mantissa of the logarithm of 4030 . Finally, add the characteristic portion of the logarithm. The result is $\log _{10} 4032=3+0.605305+0.2 \times(0.606381-0.605305)=3.60552$.
Finding a Number Whose Logarithm Is Given.-When a logarithm is given and it is required to find the corresponding number, find the number in the body of the table equal to the value of the mantissa. This value may appear in any column 0 to 9 . Follow the row on which the mantissa is found across to the left to read the first two digits of the number sought. Read the third digit of the number from the top row of the table by following up the column on which the mantissa is found to the top. If the characteristic of the logarithm is positive, the number of figures to the left of the decimal in the number is one greater than the value of the characteristic. For example, if the figures corresponding to a given mantissa are 376 and the characteristic is 5, then the number sought has six figures to the left of the decimal point and is 376,000 . If the characteristic had been $\overline{3}$, then the number sought would have been 0.00376 . If the mantissa is not exactly obtainable in the tables, find the mantissa in the table that is nearest to the one given and determine the corresponding number. This procedure usually gives sufficiently accurate results. If more accuracy is required, find the two mantissas in the tables nearest to the mantissa given, one smaller and the other larger. For each of the two mantissas, read the three corresponding digits from the left column and top row to obtain the first three figures of the number as described before. The exact number sought lies between the two numbers found in this manner.
Next: 1) subtract the smaller mantissa from the given mantissa and; and 2) subtract the smaller mantissa from the larger mantissa.
Divide the result of (1) by the result of (2) and add the quotient to the number corresponding to the smaller mantissa.
Example: Find the number whose logarithm is 2.70053 . First, find the number closest to the mantissa 70053 in the body of the tables. The closest mantissa listed in the tables is

700704, so read across the table to the left to find the first two digits of the number sought (50) and up the column to find the third digit of the number (2). The characteristic of the logarithm given is 2 , so the number sought has three digits to the left of the decimal point. Therefore, the number sought is slightly less than 502 and greater than 501. If greater accuracy is required, find the two mantissas in the table closest to the given mantissa (699838 and 700704). Subtract the smaller mantissa from the mantissa of the given logarithm and divide the result by the smaller mantissa subtracted from the larger mantissa. Add the result to the number corresponding to the smaller mantissa. The resulting answer is $501+$ $(700530-699838) \div(700704-699838)=501+0.79=501.79$.
Avoiding the Use of Negative Characteristics.-As previously explained, the logarithm of any number less than 1 has a negative characteristic and a positive mantissa. In many computations, the use of logarithms having negative characteristics is troublesome and frequently a source of error. A simple way to avoid this difficulty is to convert each logarithm having a negative characteristic into an equivalent logarithm having a positive characteristic. This is done according to the following method, which is based on the principle that any number can be simultaneously added to and subtracted from the characteristic of a logarithm without changing its value. Thus: $\log 1=0.000000=10.000000-10 ; \log$ $0.3=\overline{1} .47712=9.47712-10 ; \log 0.000478=\overline{4} .67943=6.67943-10$. Usually, 10 to 20 are added to and subtracted from the characteristic, but any convenient number may be so used.
Natural Logarithms.-In certain formulas and in some branches of mathematical analysis, use is made of logarithms (formerly also called Napierian or hyperbolic logarithms). As previously mentioned, the base of this system, $e=2.7182818284+$, is the limit of certain mathematical series. The logarithm of a number $A$ to the base $e$ is usually written $\log _{e}$ $A$ or $\ln A$. Tables of natural logarithms for numbers ranging from 1 to 10 and 1.00 to 1.01 are given in this Handbook after the table of common logarithms. To obtain natural logs of numbers less than 1 or greater than 10 , proceed as in the following examples: $\log _{e} 0.239=$ $\log _{e} 2.39-\log _{e} 10 ; \log _{e} 0.0239=\log _{e} 2.39-2 \log _{e} 10 ; \log _{e} 239=\log _{e} 2.39+2 \log _{e} 10 ; \log _{e}$ $2390=\log _{e} 2.39+3 \log _{e} 10$, etc.
Using Calculators to Find Logarithms.-Usually, using a scientific calculator is the quickest and most accurate method of finding logarithms and numbers corresponding to given logarithms. On most scientific calculators, the key labeled $\log$ is used to find common logarithms (base 10) and the key labeled $\mathbf{I n}$ is used for finding natural logarithms (base $e$ ). The keystrokes to find a logarithm will vary slightly from one calculator to another, so specific instructions are not given. To find the number corresponding to a given logarithm: use the key labeled $\mathbf{1 0}^{\mathbf{x}}$ if a common logarithm is given or use the key labeled $\mathbf{e}^{\mathbf{x}}$ if a natural logarithm is given; calculators without the $10^{\mathrm{x}}$ or $e^{\mathrm{x}}$ keys may have a key labeled $\mathbf{x}^{y}$ that can be used by substituting 10 or $e(2.718281 \ldots)$, as required, for $x$ and substituting the logarithm whose corresponding number is sought for $y$. On some other calculators, the $\log$ and $\mathbf{l n}$ keys are used to find common and natural logarithms, and the same keys in combination with the INV, or inverse, key are used to find the number corresponding to a given logarithm.
Multiplication by Logarithms.-If two or more numbers are to be multiplied together, find the logarithms of the numbers to be multiplied, and add these logarithms. The sum is the logarithm of the product, and the number corresponding to this logarithm, as found from the logarithmic tables, is the required product.
Example 1: Find the product of $2831 \times 2.692 \times 29.69 \times 19.4$

$$
\begin{aligned}
\log 2831=3.451786+0.1 \times(0.453318-0.451786) & =3.451939 \\
\log 2.692=0.429752+0.2 \times(0.431364-0.429752) & =0.430074 \\
\log 29.69=1.471292+0.9 \times(0.472756-0.471292) & =1.472610 \\
\log 19.4 & =\frac{1.287802}{6.642425}
\end{aligned}
$$

The closest number in the table corresponding to the mantissa is 439 . The characteristic indicates the number has seven digits to the left of the decimal point; therefore, the product is slightly less than $4,390,000$. If a more accurate result is required, interpolate from the table as follows: $438+(0.642425-0.641474) \div(0.642465-0.641474)=438.95963$. Therefore, the product sought is $4,389,596$.
In multiplication problems involving numbers less than 1 , the method of avoiding the use of negative characteristics simplifies the addition and tends to reduce the possibility of error.
Example: Find the product of $0.002656 \times 155.1 \times 0.5833 \times 7.968$

$$
\begin{aligned}
& \log 0.002656=\overline{3} .424228=7.424228-10 \\
& \log 155.1=2.190611=2.190611 \\
& \log 0.5853=\overline{1} .767379=9.767379-10 \\
& \log 7.968=0.901349=\underline{0.901349} \\
& 20.283567 \\
&-20=0.283567
\end{aligned}
$$

Therefore, the product is 1.92 . Interpolate for additional accuracy if required.
Division by Logarithms.-When dividing one number by another, subtract the logarithm of the divisor from the logarithm of the dividend; the remainder is the logarithm of the quotient.
Example: Find the quotient of $7658 \div 935.3$

$$
\begin{aligned}
\log 7658 . & =3.884115 \\
-\log 935.3 & =\frac{-2.970951}{0.913164}
\end{aligned}
$$

From the tables, $818+(0.913164-0.912753) \div(0.913284-0.912753)=818.8$. The answer has one digit to the left of the decimal; hence, $7658 \div 935.3=8.188$.
Instead of dividing 7658 by 935.3 , the same answer would be obtained if 7658 were multiplied by the reciprocal of 935.3 , or $1 \div 935.3$. To do this by logarithms, the $\log$ of 7658 and the $\log$ of the reciprocal of 935.3 would be added together.
To find the logarithm of the reciprocal of a number, subtract the log of the number from the $\log$ of 1 . To do this conveniently, some number, such as 10 , is first added to and then subtracted from the characteristic of the log of 1 .
Example: Find the $\log$ of the reciprocal of 935.3

$$
\begin{array}{rlr}
\log 1 & =0.000000 & =10.000000-10 \\
-\log 935.3 & =-2.970951 & =\frac{-2.970951}{7.029049}-10 \\
\log (1 \div 935.3) & =\overline{3} .029049 \\
\log (1 \div 935.3) & =0.001069
\end{array}
$$

The quotient of $7658 \div 935.3$ can be found by adding the $\log$ of 7658 and the $\log$ of the reciprocal of 935.3.

$$
\begin{aligned}
\log 7658 & =3.884115
\end{aligned}=3.884115=10.0 \frac{7.0299049-10}{\log (1 \div 935.3)=\overline{3} .029049}=\begin{aligned}
10.913164-10 & =0.91317
\end{aligned}
$$

Hence, $7658 \div 935.3=8.188$.
As is readily seen, this method is more cumbersome than the direct method where there is only one factor each in the dividend and divisor. However, it greatly facilitates the solution of problems in division involving several factors in the dividend and the divisor. In such a problem, the logarithm of each factor of the dividend is added to the logarithm of the reciprocal of each factor of the divisor.

Example: Find the quotient of

$$
\frac{0.0272 \times 27.1 \times 12.6}{2.371 \times 0.007}
$$

$$
\begin{aligned}
& \log 0.0272=\overline{2} .43457=8.434569-10 \\
& \log 27.1=1.432969=1.432969 \\
& \log 12.6=1.100371=1.100371 \\
& \log (1 \div 2.371) \quad=9.625069-10 \\
& \log (1 \div 0.007) \quad=\underline{2.154902} \\
& 22.74788-20=2.74788
\end{aligned}
$$

The quotient is $559+(0.74788-0.747412) \div(0.748188-0.747412)=559.6$.
In division problems where the divisor is larger than the dividend, the subtraction of logarithms is facilitated if some number is added to and subtracted from the $\log$ of the dividend. (The is the same method used to convert a logarithm with a negative characteristic to an equivalent logarithm with a positive characteristic except that it serves to convert a logarithm with a positive characteristic to one with a larger positive characteristic, but having the same value.)
Example: Find the quotient of $43.2 \div 971.4$

$$
\begin{aligned}
\log 43.2=1.63584= & 11.635484-10 \\
-\log 971.4=-2.987397= & \frac{-2.987397}{8.648087-10=\overline{2} .648087}
\end{aligned}
$$

Hence, the quotient of $43.2 \div 971.4$ is 0.044472 .
Obtaining the Powers of Numbers.-A number may be raised to any power by simply multiplying the logarithm of the number by the exponent of the number. The product gives the logarithm of the value of the power.
Example 1: Find the value of $6.51^{3}$

$$
\begin{aligned}
\log 6.51 & =0.81358 \\
3 \times 0.81358 & =2.44074
\end{aligned}
$$

The logarithm 2.44074 is the logarithm of $6.51^{3}$. Hence, $6.51^{3}$ equals the number corresponding to this logarithm, as found from the tables, or $6.51^{3}=275.9$.
Example 2: Find the value of $12^{1.29}$

$$
\begin{aligned}
\log 12 & =1.07918 \\
1.29 \times 1.07918 & =1.39214
\end{aligned}
$$

Hence, $12^{1.29}=24.67$.
Raising a decimal to a decimal power presents a somewhat more difficult problem because of the negative characteristic of the logarithm and the fact that the logarithm must be multiplied by a decimal exponent. The method previously outlined for avoiding the use of negative characteristics is helpful here.

Example 3: Find the value of $0.0813^{0.46}$

$$
\begin{aligned}
\log 0.0813 & =\overline{2} .91009=8.91009-10 \\
\log 0.0813^{0.46} & =0.46 \times(8.91009-10)=4.09864-4.6
\end{aligned}
$$

Subtract and add 0.6 to make the characteristic a whole number:

$$
\log 0.0813^{0.46}=\frac{\begin{array}{c}
4.09864-4.6 \\
-0.6+0.6 \\
3.49864-4
\end{array}}{=1.49864}
$$

Hence, $0.0813^{0.46}=0.3152$.
Extracting Roots by Logarithms.-Roots of numbers, for example, $\sqrt[5]{37}$, can be extracted easily by means of logarithms. The small $\left(^{5}\right)$ in the radical $(\sqrt{ })$ of the root sign is called the index of the root. Any root of a number may be found by dividing its logarithm by the index of the root; the quotient is the logarithm of the root.

Example 1: Find $\sqrt[3]{276}$

$$
\begin{aligned}
& \log 276=2.44091 \\
& 2.44091 \div 3=0.81364
\end{aligned}
$$

Hence, $\log \sqrt[3]{276}=0.81364 \quad$ and $\quad \sqrt[3]{276}=6.511$
Example 2: Find $\sqrt[3]{0.67}$

$$
\log 0.67=\overline{1} .82607
$$

Here it is not possible to divide directly, because there is a negative characteristic and a positive mantissa, another instance where the method of avoiding the use of negative characteristics, previously outlined, is helpful. The preferred procedure is to add and subtract some number to the characteristic that is evenly divisible by the index of the root. The root index is 3 , so 9 can be added to and subtracted from the characteristic, and the resulting logarithm divided by 3 .

$$
\begin{aligned}
& \log 0.67=\overline{1} .82607=8.82607-9 \\
& \log \sqrt[3]{0.67}=\frac{8.82607-9}{3}=2.94202-3 \\
& \log \sqrt[3]{0.67}=2.94202-3=\overline{1} .94202
\end{aligned}
$$

Hence, $\sqrt[3]{0.67}=0.875$
Example 3: Find $\sqrt[1.7]{0.2}$

$$
\begin{aligned}
& \log 0.2=\overline{1} .30103=16.30103-17 \\
& \log \sqrt[1.7]{0.2}=\frac{16.30103-17}{1.7}=9.58884-10=\overline{1} .58884
\end{aligned}
$$

Hence,

$$
\sqrt[1.7]{0.2}=0.388
$$

Table of Logarithms
Table of Common Logarithms

|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 10 | 000000 | 004321 | 008600 | 012837 | 017033 | 021189 | 025306 | 029384 | 033424 | 037426 |
| 11 | 041393 | 045323 | 049218 | 053078 | 056905 | 060698 | 064458 | 068186 | 071882 | 075547 |
| 12 | 079181 | 082785 | 086360 | 089905 | 093422 | 096910 | 100371 | 103804 | 107210 | 110590 |
| 13 | 113943 | 117271 | 120574 | 123852 | 127105 | 130334 | 133539 | 136721 | 139879 | 143015 |
| 14 | 146128 | 149219 | 152288 | 155336 | 158362 | 161368 | 164353 | 167317 | 170262 | 173186 |
| 15 | 176091 | 178977 | 181844 | 184691 | 187521 | 190332 | 193125 | 195900 | 198657 | 201397 |
| 16 | 204120 | 206826 | 209515 | 212188 | 214844 | 217484 | 220108 | 222716 | 225309 | 227887 |
| 17 | 230449 | 232996 | 235528 | 238046 | 240549 | 243038 | 245513 | 247973 | 250420 | 252853 |
| 18 | 255273 | 257679 | 260071 | 262451 | 264818 | 267172 | 269513 | 271842 | 274158 | 276462 |
| 19 | 278754 | 281033 | 283301 | 285557 | 287802 | 290035 | 292256 | 294466 | 296665 | 298853 |
| 20 | 301030 | 303196 | 305351 | 307496 | 309630 | 311754 | 313867 | 315970 | 318063 | 320146 |
| 21 | 322219 | 324282 | 326336 | 328380 | 330414 | 332438 | 334454 | 336460 | 338456 | 340444 |
| 22 | 342423 | 344392 | 346353 | 348305 | 350248 | 352183 | 354108 | 356026 | 357935 | 359835 |
| 23 | 361728 | 363612 | 365488 | 367356 | 369216 | 371068 | 372912 | 374748 | 376577 | 378398 |
| 24 | 380211 | 382017 | 383815 | 385606 | 387390 | 389166 | 390935 | 392697 | 394452 | 396199 |
| 25 | 397940 | 399674 | 401401 | 403121 | 404834 | 406540 | 408240 | 409933 | 411620 | 413300 |
| 26 | 414973 | 416641 | 418301 | 419956 | 421604 | 423246 | 424882 | 426511 | 428135 | 429752 |
| 27 | 431364 | 432969 | 434569 | 436163 | 437751 | 439333 | 440909 | 442480 | 444045 | 445604 |
| 28 | 447158 | 448706 | 450249 | 451786 | 453318 | 454845 | 456366 | 457882 | 459392 | 460898 |
| 29 | 462398 | 463893 | 465383 | 466868 | 468347 | 469822 | 471292 | 472756 | 474216 | 475671 |
| 30 | 477121 | 478566 | 480007 | 481443 | 482874 | 484300 | 485721 | 487138 | 488551 | 489958 |
| 31 | 491362 | 492760 | 494155 | 495544 | 496930 | 498311 | 499687 | 501059 | 502427 | 503791 |
| 32 | 505150 | 506505 | 507856 | 509203 | 510545 | 511883 | 513218 | 514548 | 515874 | 517196 |
| 33 | 518514 | 519828 | 521138 | 522444 | 523746 | 525045 | 526339 | 527630 | 528917 | 530200 |
| 34 | 531479 | 532754 | 534026 | 535294 | 536558 | 537819 | 539076 | 540329 | 541579 | 542825 |
| 35 | 544068 | 545307 | 546543 | 547775 | 549003 | 550228 | 551450 | 552668 | 553883 | 555094 |
| 36 | 556303 | 557507 | 558709 | 559907 | 561101 | 562293 | 563481 | 564666 | 565848 | 567026 |
| 37 | 568202 | 569374 | 570543 | 571709 | 572872 | 574031 | 575188 | 576341 | 577492 | 578639 |
| 38 | 579784 | 580925 | 582063 | 583199 | 584331 | 585461 | 586587 | 587711 | 588832 | 589950 |
| 39 | 591065 | 592177 | 593286 | 594393 | 595496 | 596597 | 597695 | 598791 | 599883 | 600973 |
| 40 | 602060 | 603144 | 604226 | 605305 | 606381 | 607455 | 608526 | 609594 | 610660 | 611723 |
| 41 | 612784 | 613842 | 614897 | 615950 | 617000 | 618048 | 619093 | 620136 | 621176 | 622214 |
| 42 | 623249 | 624282 | 625312 | 626340 | 627366 | 628389 | 629410 | 630428 | 631444 | 632457 |
| 43 | 633468 | 634477 | 635484 | 636488 | 637490 | 638489 | 639486 | 640481 | 641474 | 642465 |
| 44 | 643453 | 644439 | 645422 | 646404 | 647383 | 648360 | 649335 | 650308 | 651278 | 652246 |
| 45 | 653213 | 654177 | 655138 | 656098 | 657056 | 658011 | 658965 | 659916 | 660865 | 661813 |
| 46 | 662758 | 663701 | 664642 | 665581 | 666518 | 667453 | 668386 | 669317 | 670246 | 671173 |
| 47 | 672098 | 673021 | 673942 | 674861 | 675778 | 676694 | 677607 | 678518 | 679428 | 680336 |
| 48 | 681241 | 682145 | 683047 | 683947 | 684845 | 685742 | 686636 | 687529 | 688420 | 689309 |
| 49 | 690196 | 691081 | 691965 | 692847 | 693727 | 694605 | 695482 | 696356 | 697229 | 698101 |
| 50 | 698970 | 699838 | 700704 | 701568 | 702431 | 703291 | 704151 | 705008 | 705864 | 706718 |
| 51 | 707570 | 708421 | 709270 | 710117 | 710963 | 711807 | 712650 | 713491 | 714330 | 715167 |
| 52 | 716003 | 716838 | 717671 | 718502 | 719331 | 720159 | 720986 | 721811 | 722634 | 723456 |
| 53 | 724276 | 725095 | 725912 | 726727 | 727541 | 728354 | 729165 | 729974 | 730782 | 731589 |
| 54 | 732394 | 733197 | 733999 | 734800 | 735599 | 736397 | 737193 | 737987 | 738781 | 739572 |
| 55 | 740363 | 741152 | 741939 | 742725 | 743510 | 744293 | 745075 | 745855 | 746634 | 747412 |
| 56 | 748188 | 748963 | 749736 | 750508 | 751279 | 752048 | 752816 | 753583 | 754348 | 755112 |
| 57 | 755875 | 756636 | 757396 | 758155 | 758912 | 759668 | 760422 | 761176 | 761928 | 762679 |
| 58 | 763428 | 764176 | 764923 | 765669 | 766413 | 767156 | 767898 | 768638 | 769377 | 770115 |
| 59 | 770852 | 771587 | 772322 | 773055 | 773786 | 774517 | 775246 | 775974 | 776701 | 777427 |

Table of Common Logarithms

|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 60 | 778151 | 778874 | 779596 | 780317 | 781037 | 781755 | 782473 | 783189 | 783904 | 784617 |
| 61 | 785330 | 786041 | 786751 | 787460 | 788168 | 788875 | 789581 | 790285 | 790988 | 791691 |
| 62 | 792392 | 793092 | 793790 | 794488 | 795185 | 795880 | 796574 | 797268 | 797960 | 798651 |
| 63 | 799341 | 800029 | 800717 | 801404 | 802089 | 802774 | 803457 | 804139 | 804821 | 805501 |
| 64 | 806180 | 806858 | 807535 | 808211 | 808886 | 809560 | 810233 | 810904 | 811575 | 812245 |
| 65 | 812913 | 813581 | 814248 | 814913 | 815578 | 816241 | 816904 | 817565 | 818226 | 818885 |
| 66 | 819544 | 820201 | 820858 | 821514 | 822168 | 822822 | 823474 | 824126 | 824776 | 825426 |
| 67 | 826075 | 826723 | 827369 | 828015 | 828660 | 829304 | 829947 | 830589 | 831230 | 831870 |
| 68 | 832509 | 833147 | 833784 | 834421 | 835056 | 835691 | 836324 | 836957 | 837588 | 838219 |
| 69 | 838849 | 839478 | 840106 | 840733 | 841359 | 841985 | 842609 | 843233 | 843855 | 844477 |
| 70 | 845098 | 845718 | 846337 | 846955 | 847573 | 848189 | 848805 | 849419 | 850033 | 850646 |
| 71 | 851258 | 851870 | 852480 | 853090 | 853698 | 854306 | 854913 | 855519 | 856124 | 856729 |
| 72 | 857332 | 857935 | 858537 | 859138 | 859739 | 860338 | 860937 | 861534 | 862131 | 862728 |
| 73 | 863323 | 863917 | 864511 | 865104 | 865696 | 866287 | 866878 | 867467 | 868056 | 868644 |
| 74 | 869232 | 869818 | 870404 | 870989 | 871573 | 872156 | 872739 | 873321 | 873902 | 874482 |
| 75 | 875061 | 875640 | 876218 | 876795 | 877371 | 877947 | 878522 | 879096 | 879669 | 880242 |
| 76 | 880814 | 881385 | 881955 | 882525 | 883093 | 883661 | 884229 | 884795 | 885361 | 885926 |
| 77 | 886491 | 887054 | 887617 | 888179 | 888741 | 889302 | 889862 | 890421 | 890980 | 891537 |
| 78 | 892095 | 892651 | 893207 | 893762 | 894316 | 894870 | 895423 | 895975 | 896526 | 897077 |
| 79 | 897627 | 898176 | 898725 | 899273 | 899821 | 900367 | 900913 | 901458 | 902003 | 902547 |
| 80 | 903090 | 903633 | 904174 | 904716 | 905256 | 905796 | 906335 | 906874 | 907411 | 907949 |
| 81 | 908485 | 909021 | 909556 | 910091 | 910624 | 911158 | 911690 | 912222 | 912753 | 913284 |
| 82 | 913814 | 914343 | 914872 | 915400 | 915927 | 916454 | 916980 | 917506 | 918030 | 918555 |
| 83 | 919078 | 919601 | 920123 | 920645 | 921166 | 921686 | 922206 | 922725 | 923244 | 923762 |
| 84 | 924279 | 924796 | 925312 | 925828 | 926342 | 926857 | 927370 | 927883 | 928396 | 928908 |
| 85 | 929419 | 929930 | 930440 | 930949 | 931458 | 931966 | 932474 | 932981 | 933487 | 933993 |
| 86 | 934498 | 935003 | 935507 | 936011 | 936514 | 937016 | 937518 | 938019 | 938520 | 939020 |
| 87 | 939519 | 940018 | 940516 | 941014 | 941511 | 942008 | 942504 | 943000 | 943495 | 943989 |
| 88 | 944483 | 944976 | 945469 | 945961 | 946452 | 946943 | 947434 | 947924 | 948413 | 948902 |
| 89 | 949390 | 949878 | 950365 | 950851 | 951338 | 951823 | 952308 | 952792 | 953276 | 953760 |
| 90 | 954243 | 954725 | 955207 | 955688 | 956168 | 956649 | 957128 | 957607 | 958086 | 958564 |
| 91 | 959041 | 959518 | 959995 | 960471 | 960946 | 961421 | 961895 | 962369 | 962843 | 963316 |
| 92 | 963788 | 964260 | 964731 | 965202 | 965672 | 966142 | 966611 | 967080 | 967548 | 968016 |
| 93 | 968483 | 968950 | 969416 | 969882 | 970347 | 970812 | 971276 | 971740 | 972203 | 972666 |
| 94 | 973128 | 973590 | 974051 | 974512 | 974972 | 975432 | 975891 | 976350 | 976808 | 977266 |
| 95 | 977724 | 978181 | 978637 | 979093 | 979548 | 980003 | 980458 | 980912 | 981366 | 981819 |
| 96 | 982271 | 982723 | 983175 | 983626 | 984077 | 984527 | 984977 | 985426 | 985875 | 986324 |
| 97 | 986772 | 987219 | 987666 | 988113 | 988559 | 989005 | 989450 | 989895 | 990339 | 990783 |
| 98 | 991226 | 991669 | 992111 | 992554 | 992995 | 993436 | 993877 | 994317 | 994757 | 995196 |
| 99 | 995635 | 996074 | 996512 | 996949 | 997386 | 997823 | 998259 | 998695 | 999131 | 999565 |
| 100 | 000000 | 000434 | 000868 | 001301 | 001734 | 002166 | 002598 | 003029 | 003461 | 003891 |
| 101 | 004321 | 004751 | 005181 | 005609 | 006038 | 006466 | 006894 | 007321 | 007748 | 008174 |
| 102 | 008600 | 009026 | 009451 | 009876 | 010300 | 010724 | 011147 | 011570 | 011993 | 012415 |
| 103 | 012837 | 013259 | 013680 | 014100 | 014521 | 014940 | 015360 | 015779 | 016197 | 016616 |
| 104 | 017033 | 017451 | 017868 | 018284 | 018700 | 019116 | 019532 | 019947 | 020361 | 020775 |
| 105 | 021189 | 021603 | 022016 | 022428 | 022841 | 023252 | 023664 | 024075 | 024486 | 024896 |
| 106 | 025306 | 025715 | 026125 | 026533 | 026942 | 027350 | 027757 | 028164 | 028571 | 028978 |
| 107 | 029384 | 029789 | 030195 | 030600 | 031004 | 031408 | 031812 | 032216 | 032619 | 033021 |
| 108 | 033424 | 033826 | 034227 | 034628 | 035029 | 035430 | 035830 | 036230 | 036629 | 037028 |
| 109 | 037426 | 037825 | 038223 | 038620 | 039017 | 039414 | 039811 | 040207 | 040602 | 040998 |

Table of Natural Logarithms

|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1.0 | 0.00000 | 0.009950 | 0.019803 | 0.029559 | 0.039221 | 0.048790 | 0.058269 | 0.067659 | 0.076961 | 0.086178 |
| 1.1 | 0.09531 | 0.104360 | 0.113329 | 0.122218 | 0.131028 | 0.139762 | 0.148420 | 0.157004 | 0.16551 | 0.173953 |
| 1.2 | 0.18232 | 0.190620 | 0.198851 | 0.207014 | 0.215111 | 0.223144 | 0.231112 | 0.239017 | 0.246860 | 0.254642 |
| 1.3 | 0.26236 | 0.270027 | 0.277632 | 0.285179 | 0.292670 | 0.300105 | 0.307485 | 0.314811 | 0.322083 | 0.329304 |
| 1.4 | 0.33647 | 0.343590 | 0.350657 | 0.357674 | 0.364643 | 0.371564 | 0.378436 | 0.385262 | 0.392042 | 0.398776 |
| 1.5 | 0.40546 | 0.412110 | 0.418710 | 0.425268 | 0.431782 | 0.438255 | 0.444686 | 0.451076 | 0.457425 | 0.463734 |
| 1.6 | 0.47000 | 0.476234 | 0.482426 | 0.488580 | 0.494696 | 0.500775 | 0.506818 | 0.512824 | 0.518794 | 0.524729 |
| 1.7 | 0.53062 | 0.536493 | 0.542324 | 0.548121 | 0.553885 | 0.559616 | 0.565314 | 0.570980 | 0.576613 | 0.582216 |
| 1.8 | 0.58778 | 0.593327 | 0.598837 | 0.604316 | 0.609766 | 0.615186 | 0.620576 | 0.625938 | 0.631272 | 0.636577 |
| 1.9 | 0.64185 | 0.647103 | 0.652325 | 0.657520 | 0.662688 | 0.667829 | 0.672944 | 0.678034 | 0.683097 | 0.688135 |
| 2.0 | 0.69314 | 0.698135 | 0.703098 | 0.708036 | 0.712950 | 0.717840 | 0.722706 | 0.727549 | 0.732368 | 0.737164 |
| 2.1 | 0.74193 | 0.746688 | 0.751416 | 0.756122 | 0.760806 | 0.765468 | 0.770108 | 0.774727 | 0.779325 | 0.783902 |
| 2.2 | 0.78845 | 0.792993 | 0.797507 | 0.802002 | 0.806476 | 0.810930 | 0.815365 | 0.819780 | 0.824175 | 0.828552 |
| 2.3 | 0.83290 | 0.837248 | 0.841567 | 0.845868 | 0.850151 | 0.854415 | 0.858662 | 0.862890 | 0.867100 | 0.871293 |
| 2.4 | 0.87546 | 0.879627 | 0.883768 | 0.887891 | 0.891998 | 0.896088 | 0.900161 | 0.904218 | 0.908259 | 0.912283 |
| 2.5 | 0.91629 | 0.920283 | 0.924259 | 0.928219 | 0.932164 | 0.936093 | 0.940007 | 0.943906 | 0.947789 | 0.951658 |
| 2.6 | 0.95551 | 0.959350 | 0.963174 | 0.966984 | 0.970779 | 0.974560 | 0.978326 | 0.982078 | 0.985817 | 0.989541 |
| 2.7 | 0.99325 | 0.996949 | 1.000632 | 1.004302 | 1.007958 | 1.011601 | 1.015231 | 1.018847 | 1.022451 | 1.026042 |
| 2.8 | 1.02961 | 1.033184 | 1.036737 | 1.040277 | 1.043804 | 1.047319 | 1.050822 | 1.054312 | 1.057790 | 1.061257 |
| 2.9 | 1.06471 | 1.068153 | 1.071584 | 1.075002 | 1.078410 | 1.081805 | 1.085189 | 1.088562 | 1.091923 | 1.095273 |
| 3.0 | 1.09861 | 1.101940 | 1.10525 | 1.10856 | 1.111858 | 1.115142 | 1.118415 | 1.121678 | 1.124930 | 1.128171 |
| 3.1 | 1.13140 | 1.134623 | 1.137833 | 1.141033 | 1.144223 | 1.147402 | 1.150572 | 1.153732 | 1.156881 | 1.160021 |
| 3.2 | 1.16315 | 1.166271 | 1.16938 | 1.17 | 1.175573 | 1.178655 | 1.181727 | 1.184790 | 1.187843 | 1.190888 |
| 3.3 | 1.19392 | 1.196948 | 1.199965 | 1.202972 | 1.205971 | 1.208960 | 1.211941 | 1.214913 | 1.217876 | 1.220830 |
| 3.4 | 1.22377 | 1.226712 | 1.22964 | 1.23256 | 1.235471 | 1.238374 | 1.241269 | 1.244155 | 1.247032 | 1.249902 |
| 3.5 | 1.25276 | 1.255616 | 1.258461 | 1.261298 | 1.264127 | 1.266948 | 1.269761 | 1.272566 | 1.275363 | 1.278152 |
| 3.6 | 1.28093 | 1.283708 | 1.28647 | 1.289233 | 1.291984 | 1.294727 | 1.297463 | 1.300192 | 1.302913 | 1.305626 |
| 3.7 | 1.30833 | 1.311032 | 1.313724 | 1.316408 | 1.319086 | 1.321756 | 1.324419 | 1.327075 | 1.329724 | 1.332366 |
| 3.8 | 1.33500 | 1.337629 | 1.340250 | 1.342865 | 1.345472 | 1.348073 | 1.350667 | 1.353255 | 1.355835 | 1.358409 |
| 3.9 | 1.36097 | 1.363537 | 1.366092 | 1.368639 | 1.371181 | 1.373716 | 1.376244 | 1.378766 | 1.381282 | 1.383791 |
| 4.0 | 1.38629 | 1.388791 | 1.391282 | 1.393766 | 1.396245 | 1.398717 | 1.401183 | 1.403643 | 1.406097 | 1.408545 |
| 4.1 | 1.41098 | 1.413423 | 1.415853 | 1.418277 | 1.420696 | 1.423108 | 1.425515 | 1.427916 | 1.430311 | 1.432701 |
| 4.2 | 1.43508 | 1.437463 | 1.439835 | 1.442202 | 1.444563 | 1.446919 | 1.449269 | 1.451614 | 1.453953 | 1.456287 |
| 4.3 | 1.45861 | 1.460938 | 1.463255 | 1.465568 | 1.467874 | 1.470176 | 1.472472 | 1.474763 | 1.477049 | 1.479329 |
| 4.4 | 1.48160 | 1.483875 | 1.486140 | 1.488400 | 1.490654 | 1.492904 | 1.495149 | 1.497388 | 1.499623 | 1.501853 |
| 4.5 | 1.50407 | 1.506297 | 1.508512 | 1.510722 | 1.512927 | 1.515127 | 1.517323 | 1.519513 | 1.521699 | 1.523880 |
| 4.6 | 1.52605 | 1.528228 | 1.530395 | 1.532557 | 1.534714 | 1.536867 | 1.539015 | 1.541159 | 1.543298 | 1.545433 |
| 4.7 | 1.54756 | 1.549688 | 1.551809 | 1.553925 | 1.556037 | 1.558145 | 1.560248 | 1.562346 | 1.564441 | 1.566530 |
| 4.8 | 1.56861 | 1.570697 | 1.572774 | 1.574846 | 1.576915 | 1.578979 | 1.581038 | 1.583094 | 1.585145 | 1.587192 |
| 4.9 | 1.58923 | 1.591274 | 1.593309 | 1.595339 | 1.597365 | 1.599388 | 1.601406 | 1.603420 | 1.605430 | 1.607436 |
| 5.0 | 1.60943 | 1.611436 | 1.613430 | 1.615420 | 1.617406 | 1.619388 | 1.621366 | 1.623341 | 1.625311 | 1.627278 |
| 5.1 | 1.62924 | 1.631199 | 1.633154 | 1.635106 | 1.637053 | 1.638997 | 1.640937 | 1.642873 | 1.644805 | 1.646734 |
| 5.2 | 1.64865 | 1.650580 | 1.652497 | 1.654411 | 1.656321 | 1.658228 | 1.660131 | 1.662030 | 1.663926 | 1.665818 |
| 5.3 | 1.66770 | 1.669592 | 1.671473 | 1.673351 | 1.675226 | 1.677097 | 1.678964 | 1.680828 | 1.682688 | 1.684545 |
| 5.4 | 1.68639 | 1.688249 | 1.690096 | 1.691939 | 1.693779 | 1.695616 | 1.697449 | 1.699279 | 1.701105 | 1.702928 |
| 5.5 | 1.70474 | 1.706565 | 1.708378 | 1.710188 | 1.711995 | 1.713798 | 1.715598 | 1.717395 | 1.719189 | 1.720979 |
| 5.6 | 1.722767 | 1.724551 | 1.726332 | 1.728109 | 1.729884 | 1.731656 | 1.733424 | 1.735189 | 1.736951 | 1.738710 |
| 5.7 | 1.74046 | 1.742219 | 1.743969 | 1.745716 | 1.747459 | 1.749200 | 1.750937 | 1.752672 | 1.754404 | 1.756132 |
| 5.8 | 1.75785 | 1.759581 | 1.761300 | 1.763017 | 1.764731 | 1.766442 | 1.768150 | 1.769855 | 1.771557 | 1.773256 |
| 5.9 | 1.77495 | 1.776646 | 1.778336 | 1.780024 | 1.781709 | 1.783391 | 1.785070 | 1.786747 | 1.788421 | 1.790091 |

Table of Natural Logarithms

|  | 0 | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 6.0 | 1.791759 | 1.793425 | 1.795087 | 1.796747 | 1.798404 | 1.800058 | 1.801710 | 1.803359 | 1.805005 | 1.806648 |
| 6. | 1.808289 | 1.809927 | 1.811562 | 1.813195 | 1.814825 | 1.816452 | 1.818077 | 1.819699 | 1.821318 | 1.822935 |
| 6.2 | 1.824549 | 1.826161 | 1.827770 | 1.829376 | 1.830980 | 1.832581 | 1.834180 | 1.835776 | 1.837370 | 1.838961 |
| 6.3 | 1.840550 | 1.842136 | 1.843719 | 1.845300 | 1.846879 | 1.848455 | 1.850028 | 1.851599 | 1.853168 | 1.854734 |
| 6.4 | 1.856298 | 1.857859 | 1.859418 | 1.860975 | 1.862529 | 1.864080 | 1.865629 | 1.867176 | 1.868721 | 1.870263 |
| 6.5 | 1.871802 | 1.873339 | 1.874874 | 1.876407 | 1.877937 | 1.879465 | 1.880991 | 1.882514 | 1.884035 | 1.885553 |
| 6.6 | 1.887070 | 1.888584 | 1.890095 | 1.891605 | 1.89311 | 1.894617 | 1.896119 | 1.897620 | 1.899118 | 1.900614 |
| 6.7 | 1.902108 | 1.903599 | 1.905088 | 1.906575 | 1.908060 | 1.909543 | 1.911023 | 1.912501 | 1.913977 | 1.915451 |
| 6. | 1.916923 | 1.918392 | 1.919859 | 1.921325 | 1.922788 | 1.924249 | 1.925707 | 1.927164 | 1.928619 | 1.930071 |
| 6.9 | 1.931521 | 1.932970 | 1.934416 | 1.935860 | 1.937302 | 1.938742 | 1.940179 | 1.941615 | 1.943049 | 1.944481 |
| 7.0 | 1.945910 | 1.947338 | 1.948763 | 1.950187 | 1.951608 | 1.953028 | 1.954445 | 1.955860 | 1.957274 | 1.958685 |
| 7.1 | 1.960095 | 1.961502 | 1.962908 | 1.964311 | 1.965713 | 1.967112 | 1.968510 | 1.969906 | 1.971299 | 1.972691 |
| 7.2 | 1.974081 | 1.975469 | 1.976855 | 1.978239 | 1.97962 | 1.981001 | 1.982380 | 1.983756 | 1.985131 | 1.986504 |
| 7.3 | 1.987874 | 1.989243 | 1.990610 | 1.991976 | 1.993339 | 1.994700 | 1.996060 | 1.997418 | 1.998774 | 2.000128 |
| 7.4 | 2.001480 | 2.002830 | 2.004179 | 2.005526 | 2.0 | 2.0 | 2.009555 | 2.010895 | 2.012233 | 2.013569 |
| 7.5 | 2.014903 | 2.016235 | 2.017566 | 2.018895 | 2.020222 | 2.021548 | 2.022871 | 2.024193 | 2.025513 | 2.026832 |
| 7.6 | 2.028148 | 2.029463 | 2.0307 | 2.032088 | 2.03 | 2.034 | 2.036012 | 2.037317 | 2.038620 | 2.039921 |
| 7.7 | 2.041220 | 2.042518 | 2.043814 | 2.045109 | 2.046402 | 2.047693 | 2.048982 | 2.050270 | 2.051556 | 2.052841 |
| 7.8 | 2.054124 | 2.055405 | 2.056685 | 2.057963 | 2.05923 | 2.060514 | 2.061787 | 2.063058 | 2.064328 | 2.065596 |
| 7.9 | 2.066863 | 2.068128 | 2.069391 | 2.070653 | 2.071913 | 2.073172 | 2.074429 | 2.075684 | 2.076938 | 2.078191 |
| 8.0 | 2.079442 | 2.080691 | 2.081938 | 2.083185 | 2.08442 | 2.085672 | 2.086914 | 2.088153 | 2.089392 | 2.090629 |
| 8.1 | 2.09186 | 2.093098 | 2.094330 | 2.095561 | 2.096790 | 2.09801 | 2.099244 | 2.100469 | 2.101692 | 2.102914 |
| 8.2 | 2.104134 | 2.105353 | 2.106570 | 2.107786 | 2.109000 | 2.110213 | 2.111425 | 2.112635 | 2.113843 | 2.115050 |
| 8.3 | 2.116256 | 2.117460 | 2.118662 | 2.119863 | 2.1 | 2.1 | 2.123458 | 2.124654 | 2.125848 | 2.127041 |
| 8.4 | 2.128232 | 2.129421 | 2.130610 | 2.131797 | 2.132982 | 2.134166 | 2.135349 | 2.136531 | 2.137710 | 2.138889 |
| 8.5 | 2.140066 | 2.141242 | 2.142416 | 2.143589 | 2.14476 | 2.14593 | 2.147100 | 2.148268 | 2.149434 | 2.150599 |
| 8.6 | 2.151762 | 2.152924 | 2.154085 | 2.155245 | 2.156403 | 2.157559 | 2.158715 | 2.159869 | 2.161022 | 2.162173 |
| 8.7 | 2.163323 | 2.164472 | 2.165619 | 2.166765 | 2.167910 | 2.169054 | 2.170196 | 2.171337 | 2.172476 | 2.173615 |
| 8.8 | 2.174752 | 2.175887 | 2.177022 | 2.178155 | 2.179287 | 2.180417 | 2.181547 | 2.182675 | 2.183802 | 2.184927 |
| 8.9 | 2.186051 | 2.187174 | 2.188296 | 2.189416 | 2.190536 | 2.191654 | 2.192770 | 2.193886 | 2.195000 | 2.196113 |
| 9.0 | 2.197225 | 2.198335 | 2.199444 | 2.200552 | 2.201659 | 2.202765 | 2.203869 | 2.204972 | 2.206074 | 2.207175 |
| 9.1 | 2.208274 | 2.209373 | 2.210470 | 2.211566 | 2.212660 | 2.213754 | 2.214846 | 2.215937 | 2.217027 | 2.218116 |
| 9.2 | 2.219203 | 2.220290 | 2.221375 | 2.222459 | 2.223542 | 2.224624 | 2.225704 | 2.226783 | 2.227862 | 2.228939 |
| 9.3 | 2.230014 | 2.231089 | 2.232163 | 2.233235 | 2.234306 | 2.235376 | 2.236445 | 2.237513 | 2.238580 | 2.239645 |
| 9.4 | 2.240710 | 2.241773 | 2.242835 | 2.243896 | 2.244956 | 2.246015 | 2.247072 | 2.248129 | 2.249184 | 2.250239 |
| 9.5 | 2.251292 | 2.252344 | 2.253395 | 2.254445 | 2.255493 | 2.256541 | 2.257588 | 2.258633 | 2.259678 | 2.260721 |
| 9.6 | 2.261763 | 2.262804 | 2.263844 | 2.264883 | 2.265921 | 2.266958 | 2.267994 | 2.269028 | 2.270062 | 2.271094 |
| 9.7 | 2.272126 | 2.273156 | 2.274186 | 2.275214 | 2.276241 | 2.277267 | 2.278292 | 2.279316 | 2.280339 | 2.281361 |
| 9.8 | 2.282382 | 2.283402 | 2.284421 | 2.285439 | 2.286456 | 2.287471 | 2.288486 | 2.289500 | 2.290513 | 2.291524 |
| 9.9 | 2.292535 | 2.293544 | 2.294553 | 2.295560 | 2.296567 | 2.297573 | 2.298577 | 2.299581 | 2.300583 | 2.301585 |
| 1.00 | 0.000000 | 0.001000 | 0.001998 | 0.002996 | 0.003992 | 0.004988 | 0.005982 | 0.006976 | 0.007968 | 0.008960 |
| 1.01 | 0.009950 | 0.010940 | 0.011929 | 0.012916 | 0.013903 | 0.014889 | 0.015873 | 0.016857 | 0.017840 | 0.018822 |
| 1.02 | 0.019803 | 0.020783 | 0.021761 | 0.022739 | 0.023717 | 0.024693 | 0.025668 | 0.026642 | 0.027615 | 0.028587 |
| 1.03 | 0.029559 | 0.030529 | 0.031499 | 0.032467 | 0.033435 | 0.034401 | 0.035367 | 0.036332 | 0.037296 | 0.038259 |
| 1.04 | 0.039221 | 0.040182 | 0.041142 | 0.042101 | 0.043059 | 0.044017 | 0.044973 | 0.045929 | 0.046884 | 0.047837 |
| 1.05 | 0.048790 | 0.049742 | 0.050693 | 0.051643 | 0.052592 | 0.053541 | 0.054488 | 0.055435 | 0.056380 | 0.057325 |
| 1.06 | 0.058269 | 0.059212 | 0.060154 | 0.061095 | 0.062035 | 0.062975 | 0.063913 | 0.064851 | 0.065788 | 0.066724 |
| 1.07 | 0.067659 | 0.068593 | 0.069526 | 0.070458 | 0.071390 | 0.072321 | 0.073250 | 0.074179 | 0.075107 | 0.076035 |
| 1.08 | 0.076961 | 0.077887 | 0.078811 | 0.079735 | 0.080658 | 0.081580 | 0.082501 | 0.083422 | 0.084341 | 0.085260 |
| 1.09 | 0.086178 | 0.087095 | 0.088011 | 0.088926 | 0.089841 | 0.090754 | 0.091667 | 0.092579 | 0.093490 | 0.094401 |

